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PHILOSOPHICAL TRANSACTIONS.

VII. *Contributions to Terrestrial Magnetism.*—No. VI.

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§ 10. *Observations made on Board Her Majesty's Ships Erebus and Terror, from June 1841 to August 1842, in the Antarctic Expedition under the command of Captain Sir JAMES CLARK ROSS, R.N., F.R.S.*

I HAVE now to lay before the Royal Society the results of the Magnetic Observations made at sea by the Antarctic Expedition during the second year of its operations in the southern hemisphere. Leaving Hobarton early in July 1841, the ships proceeded in the first instance to Sydney in Australia, and from thence to the Bay of Islands in New Zealand, where they remained until the return of the season of navigation in the high latitudes. Quitting New Zealand in November, the ice was met with and entered in a somewhat lower latitude than in the preceding year, and in a longitude considerably to the east of the former track. The obstacles which the ice presented to their progress appear to have been greater than on the former occasion; they were however surmounted, and in February 1842 the ships again reached the ice barrier, or glacier, in latitude 78° , by which they had been stopped in the preceding year. After an unsuccessful endeavour to turn the eastern extremity of the glacier, the advance of the season compelled their return to the lower latitudes; they quitted the Antarctic Circle in March 1842, and keeping nearly in the 60th parallel, crossed the whole breadth of the southern Pacific Ocean to the Falkland Islands, where they arrived in April.

I proceed at once to the examination in detail of the magnetic observations made during this period.

Deductions of the Constants a and b in the Corrections for the Ship's attraction.

1. *In the Erebus.*—For the constants a and b to be employed in computing the corrections of the declination, we have the observations on each of the 32 principal points of the compass at Hobarton, in October 1840 and June 1841. We have also a similar series at Port Louis, in the Falkland Islands, in August 1842. The observations at Hobarton have been already discussed in No. V.* Those at Port Louis were as follows:—

August 19, 1842.

Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.
N.	+0 12·7	w.	−2 15·8	s.	+0 00·1	E.	+2 07·4
N. by w.	−0 04·1	w. by s.	−2 21·2	s. by E.	+0 43·9	E. by N.	+1 54·0
N.N.W.	−0 33·6	w.s.w.	−2 21·3	s.s.e.	+1 12·7	E.N.E.	+1 44·0
N.W. by N.	−0 50·1	s.w. by w.	−2 4·3	s.e. by s.	+1 41·4	N.E. by E.	+1 16·5
N.W.	−1 02·3	s.w.	−1 8·0	s.e.	+1 55·5	N.E.	+0 50·9
N.W. by w.	−1 00·6	s.w. by s.	−1 3·3	s.e. by E.	+2 06·9	N.E. by N.	+0 40·5
w.N.W.	−1 49·3	s.s.w.	−1 17·3	E.s.e.	+2 18·9	N.N.E.	+0 41·2
w. by N.	−2 09·6	s. by w.	−0 38·6	E. by s.	+2 16·4	N. by E.	+0 27·7

The values of the constants deduced from the observations at Hobarton were, $a=+0.0272$; $b=+0.986$. The values from the observations at the Falkland Islands are, $a=+0.0292$; $b=+0.984$.

The values of a at Hobarton were derived from two series, one in October 1840, when the ship had recently passed through the low magnetic latitudes, and the other in June 1841, on her return from the highest magnetic latitudes of the southern hemisphere; the two series separately considered give $a=+0.0235$ in 1840, and 0.0309 in 1841; we have therefore the following values:—

+0.0267 in the Thames, where the ship had been stationary for several years.

+0.0235 at Hobarton, on her first arrival from the low latitudes.

+0.0305 on her return to Hobarton from the very high southern magnetic latitudes.

+0.0292 at the Falkland Islands in 1842, on her second return from the very high southern latitudes.

The variations in these values is in accordance with the view expressed in the preceding Number of these Contributions†, that when a ship changes her magnetic latitude, the corresponding change in the induced portion of her magnetism may not be instantaneous; that some portions of her iron may be of a quality intermediate between perfectly soft iron, which would undergo instantaneous change, and iron permanently magnetic; and that when changing rapidly her geographical position, she may be liable to be more or less in arrear, in regard to her magnetic condition, of her actual locality at any particular time. In a ship in which this should be the case, a table computed with any one value of a would not apply equally to one portion

* Philosophical Transactions, 1843, Part II. pp. 152–154.

† Ibid. pp. 152, 153.

of her voyage in which she might be sailing from lower into higher inclinations, and to another portion in which she might be returning from higher into lower magnetic latitudes. The voyage under consideration comprised two such portions; and I have therefore employed two tables for the Erebus, one computed with $\cdot 0267$ for the period when the ship was increasing the dip, and the other with $\cdot 0288$ for the period when she was decreasing the dip. The differences are insignificant, except when the inclination is very high; the greater part of the declinations observed in the high dips were antecedent to the 1st of March 1842, when the ship commenced her return to the lower latitudes; for these the table computed with $a = \cdot 0267$ has been employed, and appears to answer better than the corrections computed either by the values resulting from the observations at Hobarton before the commencement, or by those at the Falkland Islands after the conclusion of the voyage.

2. *In the Terror*.—For the values of a and b in the Terror, we have observations on each of the thirty-two principal points of the compass at Hobarton in October 1840, and a second series in June 1841, as follows:—

Ship's head by compass.	Disturbance towards the west.			Ship's head by compass.	Disturbance towards the west.		
	1840.	1841.	Mean.		1840.	1841.	Mean.
N.	+0 42.4	—0 52	—0 05	S.	—0 11.6	—0 55	—0 33
N. by W.	—0 23.6	—0 52	—0 38	S. by E.	+0 52.4	—0 06	+0 23
N.N.W.	—1 20.6	—0 59	—1 10	S.S.E.	+1 56.4	+0 43	+1 20
N.W. by N.	—2 20.6	—0 03	—1 12	S.E. by S.	+2 38.4	+2 08	+2 23
N.W.	—3 25.6	—0 58	—2 12	S.E.	+3 19.4	+2 57	+3 08
N.W. by W.	—3 56.6	—2 12	—3 04	S.E. by E.	+4 00.4	+3 48	+3 54
W.N.W.	—4 01.6	—2 26	—3 14	E.S.E.	+4 43.4	+5 25	+4 54
W. by N.	—4 06.6	—2 51	—3 29	E. by S.	+4 28.4	+4 58	+4 43
W.	—4 36.6	—3 34	—4 06	E.	+4 24.4	+4 27	+4 26
W. by S.	—4 44.6	—3 43	—4 14	E. by N.	+4 11.4	+4 02	+4 07
W.S.W.	—4 52.6	—4 34	—4 43	E.N.E.	+4 07.4	+3 27	+3 47
S.W. by W.	—5 22.6	—4 01	—4 42	N.E. by E.	+3 27.4	+3 04	+3 16
S.W.	—4 23.6	—3 50	—4 07	N.E.	+3 02.4	+3 01	+3 02
S.W. by S.	—3 31.6	—4 22	—3 57	N.E. by N.	+2 37.4	+2 27	+2 32
S.S.W.	—2 03.6	—3 41	—2 52	N.N.E.	+2 11.4	+0 46	+1 29
S. by W.	—1 37.6	—2 44	—1 11	N. by E.	+1 26.4	—0 12	+0 37

We have also a series at Port Louis, in the Falkland Islands, in August 1842, as follows:—

Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.	Ship's head by compass.	Disturbance towards the west.
N.	+0 19	W.	—2 30	S.	—0 16	E.	+2 46
N. by W.	—0 02	W. by S.	—2 21	S. by E.	—0 08	E. by N.	+2 27
N.N.W.	—0 17	W.S.W.	—2 12	S.S.E.	0 00	E.N.E.	+1 58
N.W. by N.	—0 48	S.W. by W.	—2 21	S.E. by E.	+0 47	N.E. by E.	+1 39
N.W.	—1 19	S.W.	—1 33	S.E.	+1 35	N.E.	+1 13
N.W. by W.	—1 49	S.W. by S.	—1 05	S.E. by E.	+2 17	N.E. by N.	+1 11
W.N.W.	—1 47	S.S.W.	—0 47	E.S.E.	+3 04	N.N.E.	+0 34
W. by N.	—2 07	S. by W.	—0 45	E. by S.	+2 33	N. by E.	+0 27

From these observations we have the following values of the constants:—

Hobarton $a = +\cdot 0275$; $b = +\cdot 979$

Falkland Islands . . . $a = +\cdot 0293$; $b = +\cdot 994$.

These values are nearly the same as those derived from the observations in the Erebus at the same periods, and appear to require no special remark; the same tables have been employed in the declination corrections of both ships during the voyage under notice; the values of the constants in these tables were as follows:—

$a = \cdot 0267$ when the ships were sailing from the lower into the higher latitudes; $a = \cdot 0288$ when sailing from the higher into the lower latitudes; $b = +\cdot 984$ in both cases.

Deduction of the Corrections on account of the Ship's attraction for the Observations of Inclination.

1. *In the Erebus.*—The spot in the ship in which Mr. Fox's apparatus for the observations of inclination and intensity was employed, was a few feet in advance (towards the bow), and about two feet lower in height, than the position of the standard compass.

The values of a and b derived from the observations with the compass needle apply in strictness only to the spot in which that compass was stationed; it may be proper, therefore, before we employ them for the observations with Mr. Fox's apparatus, to show that nearly similar values for the constant a in particular (the more important constant) are deducible from the observations of inclination and intensity, independently of those made with the compass needle. For this purpose we may employ equation (1.), Phil. Trans., 1843, Part II. p. 147, viz.

$$\frac{\phi'}{A'\phi} \cos \theta' \cos \zeta' = \cos \theta \cos \zeta + a \sin \theta,$$

obtaining by its means the value of a from the observations of inclination and intensity made at Hobarton and Port Louis. As A' is known to differ very slightly, if at all, from unity, we have from equation (1.),

$$a \sin \theta = \frac{\phi'}{\phi} \cos \theta' \cos \zeta' - \cos \theta \cos \zeta.$$

ϕ and θ are furnished by the mean of the observations of inclination and intensity on the sixteen points of the compass, having approximate corrections applied to each of them; ϕ' and θ' by the (uncorrected) observations on the different points.

From the general aspect of the observations at both stations, we may conclude that the same symmetrical distribution of the iron existed in reference to the position of Mr. Fox's apparatus as in the case of the standard compass, and consequently that at the north and south points the value of ζ' and ζ coincided, being equal in the one case to 0° , and in the other to 180° . At Hobarton (in June 1841) we have $\phi = 1\cdot 83$, $\theta = -70^\circ 39'$; ϕ' at north $1\cdot 812$, at south $1\cdot 854$; θ' at north $-71^\circ 56'$, at south $-69^\circ 14'$:

Hence at north, $-.944a = +.307 - .331$ } ; whence $a = +.0275$.
 at south, $-.944a = -.359 + .331$ }

At Port Louis (August 1842) we have $\phi = 1.32$; $\theta = -52^\circ 05'$; ϕ' at north $= 1.279$, at south $= 1.346$; θ' at north $= -52^\circ 50'$, at south $= -51^\circ 33'$; hence

at north, $-.789a = +.5920 - .615$ } ; whence $a = +.0310$.
 at south, $-.788a = -.6367 + .615$ }

The accordance between these values and those deduced from the observations with the standard compass is fully sufficient to justify the inference that the effect of the ship's attraction was very nearly the same at the spot where Mr. Fox's apparatus was used, as at that at which the standard compass was fixed.

We may obtain c either by equation (11.), Phil. Trans., 1843, Part II. p. 148,

$$c \cos \zeta + d \tan \theta = \sqrt{(\cos \zeta + a \tan \theta)^2 + b^2 \sin^2 \zeta} \cdot \tan \theta';$$

or from the observations of inclination and intensity, independently of the values of a and b , by the equation

$$\frac{\phi'}{\phi} \sin \theta' = c \cos \theta \cos \zeta - d \sin \theta.$$

Confining ourselves to the north and south points, and to those points on either side of N. and S. from which c may be most advantageously derived, the observations at Hobarton give the following values to be employed in the equations:

$$\begin{aligned} & \text{N.}; \zeta' = 0; \quad \zeta = 0; \quad \theta' = -71^\circ 56'; \quad \phi' = 1.812. \\ & \left. \begin{array}{l} \text{N.N.E.} \\ \text{N.N.W.} \end{array} \right\}; \zeta' = 22^\circ 30'; \quad \zeta = 21^\circ 03'; \quad \theta' = -71^\circ 55'; \quad \phi' = 1.812. \\ & \left. \begin{array}{l} \text{N.E.} \\ \text{N.W.} \end{array} \right\}; \zeta' = 45^\circ 0'; \quad \zeta = 42^\circ 12'; \quad \theta' = -71^\circ 48'; \quad \phi' = 1.816. \\ & \left. \begin{array}{l} \text{S.E.} \\ \text{S.W.} \end{array} \right\}; \zeta' = 135^\circ 0'; \quad \zeta = 131^\circ 17'; \quad \theta' = -69^\circ 56'; \quad \phi' = 1.847. \\ & \left. \begin{array}{l} \text{S.S.E.} \\ \text{S.S.W.} \end{array} \right\}; \zeta' = 157^\circ 30'; \quad \zeta = 155^\circ 24'; \quad \theta' = -69^\circ 38'; \quad \phi' = 1.850. \\ & \text{S.}; \zeta' = 180^\circ 0'; \quad \zeta = 180^\circ 0'; \quad \theta' = -69^\circ 14'; \quad \phi' = 1.854. \\ & \quad \quad \quad \theta = -70^\circ 39'; \quad \phi = 1.83. \end{aligned}$$

Substituting these values in the first of the above equations (11.), we have at

$$\begin{aligned} & \text{N.} \quad 1.000c - 2.85d = -2.828; \\ & \left. \begin{array}{l} \text{N.N.E.} \\ \text{N.W.} \end{array} \right\} \quad .934c - 2.85d = -2.832; \\ & \left. \begin{array}{l} \text{N.E.} \\ \text{N.W.} \end{array} \right\} \quad .741c - 2.85d = -2.841; \\ & \left. \begin{array}{l} \text{S.E.} \\ \text{S.W.} \end{array} \right\} - .660c - 2.85d = -2.853; \end{aligned}$$

$$\begin{array}{l} \text{S.S.E.} \} - \cdot 909c - 2\cdot 85d = -2\cdot 876; \\ \text{S.S.W.} \} \\ \text{S.} \quad - 1\cdot 000c - 2\cdot 85d = -2\cdot 843. \end{array}$$

Changing the signs of the three last equations, and summing, we have

$$5\cdot 24c = +\cdot 071;$$

$$\text{whence} \quad c = +\cdot 014.$$

To obtain c from the observations of inclination and intensity alone, we have at

$$\begin{array}{l} \text{N.} \quad \cdot 331c - \cdot 94d = -\cdot 941; \\ \text{N.N.E.} \} \cdot 309c - \cdot 94d = -\cdot 942; \\ \text{N.N.W.} \} \\ \text{N.E.} \} \cdot 222c - \cdot 94d = -\cdot 943; \\ \text{N.W.} \} \\ \text{S.E.} \} -\cdot 218c - \cdot 94d = -\cdot 948; \\ \text{S.W.} \} \\ \text{S.S.E.} \} -\cdot 301c - \cdot 94d = -\cdot 948; \\ \text{S.S.W.} \} \\ \text{S.} \quad -\cdot 331c - \cdot 94d = -\cdot 947. \end{array}$$

Changing the signs of the three last equations, and summing, d is eliminated as before, and

$$c = \frac{+\cdot 017}{1\cdot 71} = +\cdot 010.$$

From the observations at Port Louis, we have the following values to be employed in the equations:

$$\begin{array}{l} \text{N.} \quad \zeta' = 0; \quad \zeta = 0; \quad \theta' = -52^\circ 50'; \quad \phi' = 1\cdot 279; \\ \text{N.N.E.} \} \zeta' = 22^\circ 30'; \quad \zeta = 22^\circ 01'; \quad \theta' = -52^\circ 42'; \quad \phi' = 1\cdot 290; \\ \text{N.N.W.} \} \\ \text{N.E.} \} \zeta' = 45^\circ 0'; \quad \zeta = 43^\circ 58'; \quad \theta' = -52^\circ 45'; \quad \phi' = 1\cdot 290; \\ \text{N.W.} \} \\ \text{S.E.} \} \zeta' = 135^\circ 0'; \quad \zeta = 133^\circ 03'; \quad \theta' = -51^\circ 59'; \quad \phi' = 1\cdot 323. \\ \text{S.W.} \} \\ \text{S.S.E.} \} \zeta' = 157^\circ 30'; \quad \zeta = 155^\circ 52'; \quad \theta' = -51^\circ 33'; \quad \phi' = 1\cdot 330. \\ \text{S.S.W.} \} \\ \text{S.} \quad \zeta' = 0; \quad \zeta = 0; \quad \theta' = -51^\circ 43'; \quad \phi' = 1\cdot 346. \\ \quad \quad \quad \theta = -52^\circ 05'; \quad \phi = 1\cdot 32. \end{array}$$

Substituting these values in equation (11.), we obtain

$$c = \frac{+\cdot 094}{5\cdot 24} = +\cdot 018;$$

or from the observations of inclination and intensity alone,

$$c = \frac{+\cdot 051}{3\cdot 22} = +\cdot 016.$$

The correspondence in the value of the constants obtained from the observations at Hobarton and Port Louis, being the commencing and concluding stations of the voyage now under consideration, is fully as good as could be desired; and a table formed from them has been employed for the correction of the observations made between Hobarton and the Bay of Islands, and during the return of the Expedition from the high latitudes to the Falkland Islands commencing with the 1st of March 1842. In those portions of the voyage the ship was passing from the higher to the lower magnetic latitudes, in which circumstance they corresponded with the observations at Hobarton and Port Louis, which were both made on the return from the vicinity of the magnetic pole. But if we attempt to apply the same table to the observations made under the reverse circumstances, namely, when the ship was passing from the lower to the higher latitudes (and such was the case with the greater part of the observations which we have to correct in the present voyage), we find that the tabular numbers, where the N. and S. points are approached, furnish a decided over compensation. On days when observations have been made at or near the N. and S. points, if we seek in the table for the corrections which should bring the results in accord with each other, we find that the corrections which will do so belong to a dip which is always some degrees less than the true terrestrial dip. It appeared desirable, therefore, if possible, to form a table for the correction of the observations of this portion of the voyage, derived from those observations themselves. Fortunately we have a better opportunity of doing this than might have been anticipated. The progress of the Expedition was so much impeded by ice in the early part of January 1842, that from the 6th to the 16th inclusive, the Erebus was the whole time between the latitudes of $-65^{\circ} 54'$ and $-66^{\circ} 14'$, and between the longitudes of $204^{\circ} 33'$ and $202^{\circ} 02'$; the weather and all other circumstances being favourable, the inclination was observed in the course of those eleven days with the ship's head on seventeen different points of the compass, sufficiently distributed, and particularly towards the north points and south points, where the effect of the ship's attraction is greatest, and is in opposite directions. From the observations at north and south it is not difficult to obtain an approximate value of a , which should bring the corrected results at those points into accord. The value thus obtained is about $+0.023$. I have collected the observations during the period referred to into the following table, taking, for the sake of simplicity, only those observations which were made by the *direct* method, which, however, comprises by far the greater part of the observations of that period. I have then computed the corrections, first, with the values of the constants, such as they are given by the observations made for their determination at Hobarton and the Falkland Islands (being the commencement and close of the voyage), viz. $a = +0.028$; $b = +0.984$; $c = +0.015$ and $d = 1$; and second, with $a = +0.023$, b , c and d , as before; and have placed the two series of corrected results in the table, with columns showing in both cases the difference of the corrected result, on each point, from the mean result. A comparison of those columns seems conclusive in favour of the application

of the smaller value of a to those observations which were made when the ship was in progress from the lower to the higher latitudes. If a be taken as it was found at Hobarton and the Falkland Islands, not only are the differences generally greater, but they are systematically so; evidencing an over compensation where the north and south points are approached; whilst with the smaller value of a the differences are greatly diminished in amount, and exhibit no appearance whatsoever of system. They are such as may well be supposed to have been occasioned partly by observation error, and partly by small differences of geographical position in which the observations themselves were made.

Ship's head by compass.	Number of observations.	Inclination observed.	Values of the Constants. $a = +\cdot 028$. $b = +\cdot 984$; $c = +\cdot 015$; $d = 1$.			Values of the Constants. $a = +\cdot 023$. $b = +\cdot 984$; $c = +\cdot 015$; $d = 1$.		
			Computed corrections.	Inclinations corrected.	$\alpha - \beta$.	Computed corrections.	Inclinations corrected.	$\alpha - \beta$.
				β .			β .	
N.	1	$-80^{\circ} 58'$	$+1^{\circ} 32'$	$-79^{\circ} 26'$	$-20'$	$+1^{\circ} 16'$	$-79^{\circ} 42'$	$-3'$
N.N.E.	2	$-81^{\circ} 00'$	$+1^{\circ} 27'$	$-79^{\circ} 33'$	$-13'$	$+1^{\circ} 12'$	$-79^{\circ} 48'$	$+3'$
N.E.	2	$-80^{\circ} 42'$	$+1^{\circ} 12'$	$-79^{\circ} 30'$	$-26'$	$+1^{\circ} 00'$	$-79^{\circ} 42'$	$-3'$
N.W.	3	$-80^{\circ} 35'$	$+1^{\circ} 12'$	$-79^{\circ} 23'$	$-23'$	$+1^{\circ} 00'$	$-79^{\circ} 35'$	$-10'$
N.E. by E.	2	$-80^{\circ} 50'$	$+1^{\circ} 01'$	$-79^{\circ} 49'$	$+3'$	$+0^{\circ} 55'$	$-79^{\circ} 55'$	$+10'$
W.	1	$-79^{\circ} 58'$	$+0^{\circ} 17'$	$-79^{\circ} 41'$	$-5'$	$+0^{\circ} 14'$	$-79^{\circ} 44'$	$-1'$
E.	3	$-79^{\circ} 50'$	$+0^{\circ} 17'$	$-79^{\circ} 33'$	$-13'$	$+0^{\circ} 14'$	$-79^{\circ} 36'$	$-9'$
E. by S.	1	$-79^{\circ} 45'$	$-0^{\circ} 01'$	$-79^{\circ} 46'$	$-00'$	$-0^{\circ} 01'$	$-79^{\circ} 46'$	$+1'$
S.W. by W.	3	$-79^{\circ} 19'$	$-0^{\circ} 38'$	$-79^{\circ} 57'$	$+11'$	$-0^{\circ} 31'$	$-79^{\circ} 50'$	$+5'$
S.W. $\frac{3}{4}$ W.	1	$-79^{\circ} 30'$	$-0^{\circ} 42'$	$-80^{\circ} 12'$	$+26'$	$-0^{\circ} 34'$	$-80^{\circ} 04'$	$+19'$
S.W. $\frac{1}{2}$ W.	1	$-79^{\circ} 10'$	$-0^{\circ} 46'$	$-79^{\circ} 56'$	$+10'$	$-0^{\circ} 38'$	$-79^{\circ} 48'$	$+3'$
S.E.	1	$-79^{\circ} 08'$	$-0^{\circ} 55'$	$-80^{\circ} 03'$	$+17'$	$-0^{\circ} 45'$	$-79^{\circ} 53'$	$+8'$
S.W.	3	$-78^{\circ} 52'$	$-0^{\circ} 55'$	$-79^{\circ} 47'$	$+1'$	$-0^{\circ} 45'$	$-79^{\circ} 37'$	$-8'$
S.W. $\frac{1}{2}$ S.	1	$-78^{\circ} 48'$	$-1^{\circ} 02'$	$-79^{\circ} 50'$	$+4'$	$-0^{\circ} 50'$	$-79^{\circ} 38'$	$-7'$
S.S.E.	3	$-78^{\circ} 28'$	$-1^{\circ} 13'$	$-79^{\circ} 41'$	$-5'$	$-1^{\circ} 05'$	$-79^{\circ} 33'$	$-12'$
S. by W.	3	$-78^{\circ} 28'$	$-1^{\circ} 29'$	$-79^{\circ} 57'$	$+11'$	$-1^{\circ} 13'$	$-79^{\circ} 41'$	$-2'$
S.	5	$-78^{\circ} 32'$	$-1^{\circ} 31'$	$-80^{\circ} 03'$	$+17'$	$-1^{\circ} 14'$	$-79^{\circ} 46'$	$+1'$
Means	36	$-79^{\circ} 46' = \alpha$		$-79^{\circ} 45' = \alpha$	

The mean of the observations in the table thus corrected is $-79^{\circ} 45'$; the corresponding geographical position is $-66^{\circ} 04'$, and $203^{\circ} 17'.5$, if we take as such the middle point of the geographical space in which the ship was detained from the 6th to the 16th of January. The inclination observed on the ice on the 16th of January, in lat. $-65^{\circ} 49'$, long. $202^{\circ} 02'$, with needles whose poles were reversed, was $-79^{\circ} 39'.5$. We can derive no *precise* conclusion in regard to the value of d , from observations which are not identical in locality; but the accordance of the results obtained on board and on the ice, in geographical positions so little different, is quite sufficient to show that the error involved by assuming d as unity must be, at the utmost, very inconsiderable.

The tables for the correction of the inclination in the Erebus have therefore been computed with the following values for the constants, viz. from New Zealand to the end of February 1842, being the portion of the voyage in which the ship was in pro-

gress from the lower into the higher inclinations, $a = +\cdot023$, $b = +\cdot984$, $c = +\cdot015$ and $d = 1$: and for the remainder of the voyage $a = +\cdot028$, b , c and d , as before.

In the Terror.—The place in which Mr. Fox's apparatus was used in the *Terror* was about the same distance from the position of the standard compass, and in the same direction, as in the *Erebus*. A series of observations were made with it for the purpose of furnishing materials for the determination of the constants, at Hobarton in June 1841, and at the Falkland Islands in August 1842; and the inclination was also observed with the ship's head on several points of the compass during the detention of the ships by the ice between the 6th and 16th of January 1842. In the case of the *Erebus*, we have found these latter observations of principal use in furnishing the values of the constants which apply to the greater part of the observations of the voyage; it may, therefore, be advisable to commence with the discussion of the corresponding series in the *Terror*.

Inclinations observed on board Her Majesty's ship *Terror* with needle F.C.B. used direct, during her detention by the ice from the 6th to the 16th of January 1842, between the latitudes of $-65^{\circ} 45'$ and $-66^{\circ} 20'$, and longitudes of $201^{\circ} 46'$ and $204^{\circ} 04'$.

Ship's head by compass.	Number of observations.	Inclination observed.	Ship's head by compass.	Number of observations.	Inclination observed.
N.	4	$-81^{\circ} 19\cdot5$	S.	6	$-78^{\circ} 30$
N. $\frac{1}{2}$ E.	2	$-81 14$	S. $\frac{3}{4}$ W.	1	$-78 21$
N. $\frac{3}{4}$ E.	1	$-80 50$	S. by W.	1	$-78 48$
N.N.E.	3	$-80 57$	S.W. by W. $\frac{1}{2}$ W.	1	$-78 50$
N.E.	2	$-80 48$	S.W. by S.	3	$-79 00$
N.E. by E.	1	$-80 26$	S.W.	3	$-79 08$
E. $\frac{1}{2}$ N.	1	$-79 57$	S.W. $\frac{1}{2}$ W.	1	$-79 08$
E.	6	$-79 55$	S.W. by W.	5	$-79 21$
E. $\frac{1}{2}$ S.	1	$-79 45$	W.S.W.	2	$-79 37$
E. by S.	1	$-79 33$	W. by S.	1	$-80 05$
E.S.E.	2	$-79 21$	W. $\frac{1}{4}$ S.	2	$-80 07$
S.E. by E. $\frac{1}{2}$ E.	1	$-79 04$	N.W.	2	$-81 09$
S.S.E.	1	$-78 42$	N. by W.	1	$-81 15$
S. by E.	4	$-78 37$			

These observations manifest the general systematic character of the disturbance occasioned by the ship's attraction; they furnish indeed a remarkable example of the success with which the effect of the ship's iron on the inclination may be investigated by observations made at sea. The disturbance appears to have not been strictly symmetrical, inasmuch as the inclinations observed on the western points somewhat exceed in amount those observed on the corresponding eastern points; the same circumstance took place in the observations at Hobarton; but at the Falkland Islands, on the contrary, the inclinations observed on the eastern points were generally somewhat the higher. A similar occasional departure from strict symmetry has before been noticed in the effect of the ship's iron on the compass needle*; in that case also

* Philosophical Transactions, 1843, Part II. p. 152.

the disturbance in the same ship was sometimes greater on the eastern, and sometimes on the western points; these small irregularities, having no uniform character, are regarded as included amongst those varying accidents which are classed generally under the name of observation error. It is proper, however, in consequence of this occasional irregularity, that the data from which constants are to be derived for general corrections should consist of the mean of observations on corresponding points on the east and west sides of the compass; in this view we have as available observations in the preceding table those on the following points of the compass.

North	—81 19·5
N.W.	} —80 58·5
N.E.	
W. $\frac{1}{4}$ S.	} —79 58·5
E. $\frac{1}{4}$ S. (from E. and E. $\frac{1}{2}$ S.)	
W. by S.	} —79 49
E. by S.	
W.S.W.	} —79 29
E.S.E.	
S.W.	} —79 04·5
S.E. (from E.S.E. and S.S.E.)	
South	—78 30

We have here $2^{\circ} 49' \cdot 5$ for the difference between the inclinations observed with the ship's head north and south; the value of a which will give that amount for the sum of the corrections at north and south when the dip is between -79° and -80° , (neglecting c as too small in such case to require consideration), is about $+0\cdot026$. The observations at north were four in number,—those at south six, and on different days,—they were as follows:—

North.		South.	
January	8, —81 19	January	7, —78 28
	8, —81 20		8, —78 31
	8, —81 18		11, —78 28
	13, —81 21		13, —78 25
	<hr/>		13, —78 33
Mean	81 19·5		14, —78 34
			<hr/>
		Mean	78 30

From the accord which these observations respectively exhibit, it is clear that we should not be justified in taking a value of a which should differ much from $+0\cdot026$.

If we now refer to the observations which were made in the *Terror* soon after her arrival at the Falkland Islands, when the ship's head was placed on the principal points of the compass for the purpose of determining the values of the constants, we shall

find that a value of a taken near $+.026$ will by no means bring the results on the N. and S. points, or on those approaching the N. and S. points, into accord; and that as we have already found in the dip corrections of the Erebus, and in the declination corrections of both ships, a considerably higher value of a is required for the observations on the return from the high latitudes, than for those when the ship was in progress from the lower to the higher dips.

We have no observations at the Falkland Islands (made at the spot in the ship where Mr. Fox's apparatus was used) either of the direction of the compass needle, or of the force acting on the horizontal needle: we must therefore obtain a and b directly from the observations of Inclination and Intensity. The observations gave as follows:—

Ship's head.	Inclination observed. $\theta = -51^{\circ} 56'.$		Intensity observed. $\phi = 1.336.$	
	θ'		ϕ'	
N.	$-52^{\circ} 46.5$	$-52^{\circ} 46.5$	1.320	1.320
N.N.E.	$-52^{\circ} 51$	$-52^{\circ} 47$	1.315	1.314
N.N.W.	$-52^{\circ} 43$		1.313	
N.E.	$-52^{\circ} 47$	$-52^{\circ} 46$	1.314	1.313
N.W.	$-52^{\circ} 45$		1.312	
E.N.E.	$-52^{\circ} 52$	$-52^{\circ} 45$	1.336	1.322
W.N.W.	$-52^{\circ} 38$		1.308	
E.	$-52^{\circ} 31$	$-52^{\circ} 22$	1.336	1.330
W.	$-52^{\circ} 13$		1.324	
E.S.E.	$-52^{\circ} 16$	$-52^{\circ} 01$	1.355	1.350
W.S.W.	$-51^{\circ} 46$		1.345	
S.E.	$-51^{\circ} 32$	$-51^{\circ} 32$	1.370	1.364
S.W.	$-51^{\circ} 32$		1.359	
S.S.E.	$-51^{\circ} 09$	$-51^{\circ} 15$	1.368	1.367
S.S.W.	$-51^{\circ} 21$		1.366	
S.	$-50^{\circ} 53$	$-50^{\circ} 53$	1.370	1.370

For a , we have from equation (1.),

$$a \sin \theta = \frac{\phi'}{\phi} \cos \theta' \cos \zeta' - \cos \theta \cos \zeta,$$

whence we obtain, from the observations on the N. and S. points, $a = +.0311$, and from those on the N.N.E. and N.N.W., S.S.E. and S.S.W. points, a also $= +.0311$.

In the Erebus we have found a for the spot in the ship where Mr. Fox's apparatus was used $= +.023$, from the observations made when the ship was in progress to the southward; and $= +.029$ at Hobarton and the Falkland Islands. The corresponding values in the Terror are $+.026$ and $+.031$.

In the case of the Terror, therefore, I have employed separate tables for the corrections for the ship's attraction, viz. a taken as $+.028$ in the passage from Hobarton to New Zealand; as $+.026$ in the passage to the higher latitudes; and as $+.031$ during the return from the high latitudes to the Falkland Islands.

For b and c , we obtain from the observations at the Falkland Islands as follows:—

In the case of b , we have from equation (2.),

$$b \cos \theta = \frac{\phi'}{\phi} \cos \theta' \sin \zeta' \operatorname{cosec} \zeta;$$

the observations at N.E., N.W., S.E. and S.W. give $b=+^{\circ}984$; those at E.N.E., W.N.W., E.S.E. and W.S.W., $b=^{\circ}984$; and those at E. and W. $b=^{\circ}982$.

In the case of c , we have from equation (3.),

$$\frac{\phi'}{\phi} \sin \theta' = c \cos \theta \cos \zeta + d \sin \theta;$$

from the observations at N. to N.E. and N.W. inclusive, and from S. to S.E. and S.W. inclusive, eliminating d , we have

$$c=+^{\circ}009.$$

The constant d is perhaps the most difficult of the constants to ascertain satisfactorily, as its value derivable from the observations depends on a knowledge of the true geographical dip at the place of observation, free from what is now known as *station error*. Experience has fully shown the general fact, that inclinations observed on land cannot safely be assumed as free from local disturbance. The discrepancies of gravitation at the Falkland Islands are well known from the experiments with the pendulum; and from the geological character of these islands, we might be prepared to expect the existence of magnetic discrepancies also. By the needles in both ships, the inclination was found a third of a degree higher at the magnetic observatory on shore than when observed on board in the harbour; if the observatory dip were to be assumed as an undisturbed one, we should obtain d in both ships considerably less than unity, whereas from the comparison of the observations in both ships in the preceding December and January, with the inclination observed at the same time on the ice over a deep sea, where no local attraction can be imagined to exist, we have d (as far as the small differences of geographical position will permit us to judge) differing scarcely, if at all, from unity in either ship. The preference is certainly due to the deduction from the results obtained on the ice. Taking therefore $d=1$, $c=+^{\circ}01$, $b=^{\circ}984$ and $a=+^{\circ}026$, we have the corrections, and the corrected inclination, of the observations in the *Terror* between the 6th and 16th of January as follows:

Ship's head.	No. of observations.	Inclination observed.	Correction.	Corrected Inclination.
N.	4	$-81^{\circ} 19.5$	$+1^{\circ} 26$	$-79^{\circ} 53.5$
N.W.	4	$-80^{\circ} 58.5$	$+1^{\circ} 09$	$-79^{\circ} 49.5$
N.E.	9	$-79^{\circ} 58.5$	$+0^{\circ} 12$	$-79^{\circ} 46.5$
W. $\frac{1}{4}$ S.				
E. $\frac{1}{4}$ S.				
W. by S.				
E. by S.	4	$-79^{\circ} 49.0$	$-0^{\circ} 01$	$-79^{\circ} 50.0$
W.S.W.		$-79^{\circ} 29.0$	$-0^{\circ} 17.5$	$-79^{\circ} 56.5$
E.S.E.	6	$-79^{\circ} 04.5$	$-0^{\circ} 51.5$	$-79^{\circ} 56.0$
S.W.		$-78^{\circ} 30.0$	$-1^{\circ} 24.5$	$-79^{\circ} 54.5$
S.E.	6			
S.				

Slight differences in the corrected results must be looked for, as the observations were not all taken precisely at the same geographical spot: those which appear in the table are, however, very slight; the accord produced by the corrections seems as

satisfactory as could be wished or expected ; and I have accordingly taken the above stated values of *b*, *c*, and *d*, for the whole period under notice.

On a general review of the examination to which the observations in the *Erebus* and *Terror* in this and the preceding voyage have been subjected, in reference to the magnetic influence of their iron, we find reason to conclude from the consistent experience of both voyages, that the disturbance in them was altogether such as would be occasioned by the magnetism induced in the soft iron of the ship by the magnetism of the earth,—if we permit ourselves to include as possessing the quality of softness, certain portions of iron which, though not permanently magnetic, do still retain polarity, and require some time to conform to the changes in magnetical relations induced by changes of geographical position. It is not improbable that this may be a general case in sailing vessels similar to the *Erebus* and *Terror* ; but we should by no means be warranted in deriving a corresponding inference in regard to ships which contain steam machinery, and still less in the case of iron vessels. These may possibly possess permanent magnetism strictly so called ; in addition to induced magnetism, and temporarily-abiding polarity. It is very desirable that we should have some means of judging of what may be expected in vessels of these two classes. The knowledge would be valuable were it only for the compass corrections necessary for the ordinary purposes of navigation ; and it appears indispensable before a correct judgment can be formed of the confidence to which methods may be entitled, which have been already, or may hereafter be devised, to supersede these corrections by the employment of compensating forces. It is not necessary that steam or iron-built ships should perform voyages like those of the *Erebus* and *Terror* to procure this knowledge ; a voyage from the British Channel to the Tropics would be sufficient ; the ship should be swung before her departure from these islands, and immediately on her arrival in the Tropics, and at intervals of three or six months during her continuance there ; the experiment should also be repeated on her return to England before any material alteration is made in the distribution of her iron.

Index Correction.

Index Correction of R. F. 5 for the Observations of the Inclination in the Erebus.—The observations at sea with this needle having been made in the one position of the instrument only, viz. with the face of the circle towards the east, and the marked side of the needle towards the observer,—we have to obtain the index correction, by comparing the inclinations observed in the same manner on shore, or on the ice, with the results given at the same places by needles of which the poles were reversed and the needle and circle used in the eight ordinary positions.

The stations which furnish this comparison are Hobarton, Sydney, New Zealand, the Falkland Islands, and two stations on the ice in the latitudes of $-63^{\circ} 23'$ and $-65^{\circ} 49'$. The results of the observations at Hobarton with needles with which the complete process for determining the inclination was gone through, were given in No. V. of these Contributions*. Those at the other five stations are as follows :—

* Philosophical Transactions, 1843, Part II. p. 165.

Observations of the Inclination, with Needles whose Poles were reversed, made at
Garden Island, Sydney, July 1841.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1841. July 20.	h m 9 20 A.M.	R 4	$\alpha -62^{\circ} 52.5$ $\beta -62^{\circ} 46.5$	$-62^{\circ} 49.5$	Needles belonging to H.M.S. Erebus.
20.	10 45 A.M.	R 10	$\alpha -62^{\circ} 57.5$ $\beta -62^{\circ} 33.7$	$-62^{\circ} 45.6$	
20.	1 00 P.M.	R 6	$\alpha -62^{\circ} 50.1$ $\beta -62^{\circ} 58.5$	$-62^{\circ} 54.3$	
20.	2 15 P.M.	R 7	$\alpha -62^{\circ} 53.9$ $\beta -62^{\circ} 51.9$	$-62^{\circ} 52.9$	
20.	9 00 A.M.	C 1	$\alpha -62^{\circ} 48.2$ $\beta -62^{\circ} 45.6$	$-62^{\circ} 46.9$	Needles belonging to H.M.S. Terror.
		C 2	$\alpha -62^{\circ} 49.6$ $\beta -62^{\circ} 40.5$	$-62^{\circ} 45.1$	
				$-62^{\circ} 49.1$	General Mean.

Observations of the Inclination, with Needles whose Poles were reversed, made at the
Bay of Islands, New Zealand, August to November 1841.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1841. August 23.	h m 2 10 P.M.	R 10	$\alpha -59^{\circ} 46.1$ $\beta -59^{\circ} 16.9$	$-59^{\circ} 31.5$	Needles belonging to H.M.S. Erebus.
23.	3 10 P.M.	R 4	$\alpha -59^{\circ} 38.5$ $\beta -59^{\circ} 27.5$	$-59^{\circ} 33.0$	
24.	8 40 A.M.	R 4	$\alpha -59^{\circ} 38.4$ $\beta -59^{\circ} 25.8$	$-59^{\circ} 32.1$	
24.	9 45 A.M.	R 10	$\alpha -59^{\circ} 53.9$ $\beta -59^{\circ} 21.3$	$-59^{\circ} 37.4$	
24.	11 00 A.M.	R 6	$\alpha -59^{\circ} 28.8$ $\beta -59^{\circ} 34.0$	$-59^{\circ} 31.4$	
24.	1 10 P.M.	R 7	$\alpha -59^{\circ} 30.3$ $\beta -59^{\circ} 30.6$	$-59^{\circ} 30.4$	
October 5.	4 00 P.M.	R 4	$\alpha -59^{\circ} 39.7$ $\beta -59^{\circ} 27.3$	$-59^{\circ} 33.5$	
12.	7 00 A.M.	R 4	$\alpha -59^{\circ} 35.2$ $\beta -59^{\circ} 27.9$	$-59^{\circ} 31.8$	
26.	6 35 A.M.	R 4	$\alpha -59^{\circ} 35.7$ $\beta -59^{\circ} 28.1$	$-59^{\circ} 31.9$	
26.	9 35 A.M.	R 10	$\alpha -59^{\circ} 50.5$ $\beta -59^{\circ} 26.6$	$-59^{\circ} 38.5$	
26.	10 35 A.M.	R 6	$\alpha -59^{\circ} 30.1$ $\beta -59^{\circ} 31.4$	$-59^{\circ} 30.8$	
26.	1 30 P.M.	R 7	$\alpha -59^{\circ} 32.4$ $\beta -59^{\circ} 36.2$	$-59^{\circ} 34.3$	
August 23.	9 00 A.M.	C 1	$\alpha -59^{\circ} 30.0$ $\beta -59^{\circ} 27.8$	$-59^{\circ} 28.9$	Needles belonging to H.M.S. Terror.
23.	11 30 A.M.	C 2	$\alpha -59^{\circ} 31.4$ $\beta -59^{\circ} 22.7$	$-59^{\circ} 27.0$	
November 6.	9 00 A.M.	C 1	$\alpha -59^{\circ} 32.5$ $\beta -59^{\circ} 28.1$	$-59^{\circ} 30.3$	
6.	10 30 A.M.	C 2	$\alpha -59^{\circ} 32.8$ $\beta -59^{\circ} 20.8$	$-59^{\circ} 26.8$	
				$-59^{\circ} 31.9$	General Mean.

Observations of the Inclination with Needles whose Poles were reversed, made on the ice.

Date.	Lat.	Long.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1841. December 19.	$-63^{\circ} 23'$	$210^{\circ} 02'$	R 4	$\alpha -77^{\circ} 23.1$ $\beta -77^{\circ} 23.4$	$-77^{\circ} 23.3$ $-77^{\circ} 23.3$	Needles belonging to H.M.S. Erebus.
23.	$-65^{\circ} 59'$	$204^{\circ} 14'$	R 4	$\alpha -79^{\circ} 32.0$ $\beta -79^{\circ} 24.7$	$-79^{\circ} 28.4$	
23.	$-65^{\circ} 59'$	$204^{\circ} 14'$	R 6	$\alpha -79^{\circ} 35.6$ $\beta -79^{\circ} 31.5$	$-79^{\circ} 33.6$	
1842. January 16.	$-65^{\circ} 49'$	$202^{\circ} 02'$	R 4	$\alpha -79^{\circ} 40.5$ $\beta -79^{\circ} 34.4$	$-79^{\circ} 37.4$	
16.	$-65^{\circ} 49'$	$202^{\circ} 02'$	R 6	$\alpha -79^{\circ} 36.2$ $\beta -79^{\circ} 42.9$	$-79^{\circ} 39.6$	
16.	$-65^{\circ} 49'$	$202^{\circ} 02'$	R 7	$\alpha -79^{\circ} 41.8$ $\beta -79^{\circ} 41.0$	$-79^{\circ} 41.4$	

Observations of the Inclination, with Needles whose Poles were reversed, made at the Magnetic Observatory at Port Louis, in the Falkland Islands, April to August 1842.

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1842. April 12.	h m 1 30 P.M.	R 4	$\alpha -52^{\circ} 33.5$ $\beta -52^{\circ} 16.7$	$-52^{\circ} 25.1$	Needles belonging to H.M.S. Erebus.
12.	3 30 P.M.	R 6	$\alpha -52^{\circ} 26.0$ $\beta -52^{\circ} 32.0$	$-52^{\circ} 29.0$	
12.	3 30 P.M.	R 7	$\alpha -52^{\circ} 30.8$ $\beta -52^{\circ} 30.9$	$-52^{\circ} 30.8$	
15.	8 20 A.M.	R 4	$\alpha -52^{\circ} 36.8$ $\beta -52^{\circ} 16.3$	$-52^{\circ} 26.6$	
15.	3 10 P.M.	R 4	$\alpha -52^{\circ} 39.9$ $\beta -52^{\circ} 12.4$	$-52^{\circ} 26.2$	
19.	8 00 A.M.	R 4	$\alpha -52^{\circ} 36.9$ $\beta -52^{\circ} 17.8$	$-52^{\circ} 27.3$	
19.	3 30 P.M.	R 4	$\alpha -52^{\circ} 35.8$ $\beta -52^{\circ} 16.2$	$-52^{\circ} 26.3$	
22.	8 00 A.M.	R 4	$\alpha -52^{\circ} 36.3$ $\beta -52^{\circ} 16.8$	$-52^{\circ} 26.5$	
22.	3 30 P.M.	R 4	$\alpha -52^{\circ} 36.8$ $\beta -52^{\circ} 15.3$	$-52^{\circ} 26.1$	
26.	8 00 A.M.	R 4	$\alpha -52^{\circ} 35.9$ $\beta -52^{\circ} 10.3$	$-52^{\circ} 23.1$	
26.	3 30 P.M.	R 4	$\alpha -52^{\circ} 36.0$ $\beta -52^{\circ} 08.7$	$-52^{\circ} 22.3$	
29.	8 00 A.M.	R 4	$\alpha -52^{\circ} 38.3$ $\beta -52^{\circ} 18.8$	$-52^{\circ} 28.6$	
May 3.	8 00 A.M.	R 4	$\alpha -52^{\circ} 35.8$ $\beta -52^{\circ} 06.4$	$-52^{\circ} 21.1$	
3.	3 30 P.M.	R 4	$\alpha -52^{\circ} 36.8$ $\beta -52^{\circ} 16.9$	$-52^{\circ} 26.8$	
6.	8 00 A.M.	R 4	$\alpha -52^{\circ} 36.3$ $\beta -52^{\circ} 17.1$	$-52^{\circ} 26.7$	
6.	3 30 P.M.	R 4	$\alpha -52^{\circ} 37.3$ $\beta -52^{\circ} 14.9$	$-52^{\circ} 26.1$	

Observations of Inclination. (Continued.)

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1842. May 10.	^h ^m 10 30 A.M.	R 4	$\alpha - 52^{\circ} 31.2'$ $\beta - 52^{\circ} 25.2'$	$-52^{\circ} 28.2'$	Needles belonging to H.M.S. Erebus.
10.	3 00 P.M.	R 4	$\alpha - 52^{\circ} 24.3'$ $\beta - 52^{\circ} 30.6'$	$-52^{\circ} 27.5'$	
13.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 36.7'$ $\beta - 52^{\circ} 14.5'$	$-52^{\circ} 25.6'$	
13.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 37.0'$ $\beta - 52^{\circ} 13.5'$	$-52^{\circ} 25.3'$	
17.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 35.6'$ $\beta - 52^{\circ} 15.3'$	$-52^{\circ} 25.5'$	
17.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 33.4'$ $\beta - 52^{\circ} 17.7'$	$-52^{\circ} 25.5'$	
20.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 36.8'$ $\beta - 52^{\circ} 13.2'$	$-52^{\circ} 25.0'$	
20.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 34.3'$ $\beta - 52^{\circ} 13.0'$	$-52^{\circ} 23.7'$	
24.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 36.5'$ $\beta - 52^{\circ} 18.6'$	$-52^{\circ} 27.7'$	
24.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 37.6'$ $\beta - 52^{\circ} 17.7'$	$-52^{\circ} 27.7'$	
27.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 23.5'$ $\beta - 52^{\circ} 12.5'$	$-52^{\circ} 23.0'$	
27.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 32.8'$ $\beta - 52^{\circ} 14.0'$	$-52^{\circ} 23.4'$	
June 1.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 37.1'$ $\beta - 52^{\circ} 16.0'$	$-52^{\circ} 26.5'$	
1.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 35.3'$ $\beta - 52^{\circ} 16.2'$	$-52^{\circ} 25.7'$	
4.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 35.4'$ $\beta - 52^{\circ} 17.7'$	$-52^{\circ} 26.5'$	
4.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 36.3'$ $\beta - 52^{\circ} 16.9'$	$-52^{\circ} 26.6'$	
7.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 36.4'$ $\beta - 52^{\circ} 15.4'$	$-52^{\circ} 25.9'$	
7.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 29.0'$ $\beta - 52^{\circ} 13.7'$	$-52^{\circ} 26.4'$	
10.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 38.4'$ $\beta - 52^{\circ} 16.4'$	$-52^{\circ} 27.4'$	
10.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 35.9'$ $\beta - 52^{\circ} 17.6'$	$-52^{\circ} 26.8'$	
14.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 35.8'$ $\beta - 52^{\circ} 16.2'$	$-52^{\circ} 26.0'$	
14.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 41.3'$ $\beta - 52^{\circ} 13.2'$	$-52^{\circ} 27.3'$	
17.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 34.8'$ $\beta - 52^{\circ} 14.7'$	$-52^{\circ} 24.8'$	
17.	10 00 A.M.	R 6	$\alpha - 52^{\circ} 20.4'$ $\beta - 52^{\circ} 28.0'$	$-52^{\circ} 24.2'$	
17.	11 00 A.M.	R 7	$\alpha - 52^{\circ} 32.1'$ $\beta - 52^{\circ} 23.4'$	$-52^{\circ} 27.8'$	
17.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 34.0'$ $\beta - 52^{\circ} 13.6'$	$-52^{\circ} 23.8'$	
21.	8 00 A.M.	R 4	$\alpha - 52^{\circ} 29.9'$ $\beta - 52^{\circ} 18.6'$	$-52^{\circ} 24.2'$	
21.	3 30 P.M.	R 4	$\alpha - 52^{\circ} 29.7'$ $\beta - 52^{\circ} 19.9'$	$-52^{\circ} 24.8'$	

Observations of Inclination. (Continued.)

Date.	Hour.	Needle.	Poles. α direct. β reversed.	Mean.	Remarks.
1842.	h m				
June 28.	8 00 A.M.	R 4	$\alpha -52^{\circ} 28.8$ $\beta -52 14.1$	$-52^{\circ} 21.5$	Needles belonging to H.M.S. Erebus.
July 1.	3 30 P.M.	R 4	$\alpha -52 37.7$ $\beta -52 03.6$	$-52 20.7$	
5.	8 00 A.M.	R 4	$\alpha -52 28.7$ $\beta -52 14.3$	$-52 21.5$	
8.	3 30 P.M.	R 4	$\alpha -52 35.4$ $\beta -52 11.5$	$-52 23.5$	
12.	8 00 A.M.	R 4	$\alpha -52 34.1$ $\beta -52 11.9$	$-52 23.0$	
15.	3 30 P.M.	R 4	$\alpha -52 35.6$ $\beta -52 09.7$	$-52 22.7$	
19.	8 00 A.M.	R 4	$\alpha -52 32.8$ $\beta -52 11.6$	$-52 22.2$	
22.	3 30 P.M.	R 4	$\alpha -52 31.8$ $\beta -52 14.8$	$-52 23.3$	
August 2.	8 00 A.M.	R 4	$\alpha -52 32.6$ $\beta -52 16.1$	$-52 24.3$	
9.	8 00 A.M.	R 4	$\alpha -52 33.4$ $\beta -52 11.9$	$-52 22.6$	
12.	3 30 P.M.	R 4	$\alpha -52 32.7$ $\beta -52 13.8$	$-52 23.2$	
16.	8 00 A.M.	R 4	$\alpha -52 29.9$ $\beta -52 10.1$	$-52 20.0$	
19.	3 30 P.M.	R 4	$\alpha -52 38.4$ $\beta -52 11.9$	$-52 25.2$	
23.	8 00 A.M.	R 4	$\alpha -52 10.0$ $\beta -52 34.0$	$-52 22.0$	
23.	9 00 A.M.	R 6	$\alpha -52 25.7$ $\beta -52 19.3$	$-52 22.5$	
23.	10 00 A.M.	R 7	$\alpha -52 30.9$ $\beta -52 17.5$	$-52 24.2$	
April 15.	8 00 A.M.	C 1	$\alpha -52 47.0$ $\beta -52 21.7$	$-52 34.3$	Needles belonging to H.M.S. Terror.
15.	3 00 P.M.	C 1	$\alpha -52 46.1$ $\beta -52 24.9$	$-52 35.5$	
19.	8 45 A.M.	C 1	$\alpha -52 43.3$ $\beta -52 20.2$	$-52 31.8$	
19.	3 45 P.M.	C 1	$\alpha -52 42.8$ $\beta -52 21.6$	$-52 32.2$	
June 15.	8 00 A.M.	C 1	$\alpha -52 40.4$ $\beta -52 24.4$	$-52 32.4$	
15.	9 00 A.M.	C 2	$\alpha -52 37.8$ $\beta -52 20.9$	$-52 29.4$	
15.	3 00 A.M.	C 1	$\alpha -52 39.9$ $\beta -52 23.4$	$-52 31.7$	
15.	3 40 A.M.	C 2	$\alpha -52 35.4$ $\beta -52 23.2$	$-52 29.3$	
July 26.	8 40 A.M.	C 1	$\alpha -52 44.9$ $\beta -52 23.5$	$-52 34.2$	
26.	10 30 A.M.	C 2	$\alpha -52 38.6$ $\beta -52 15.3$	$-52 26.9$	
August 17.	10 00 A.M.	C 1	$\alpha -52 50.4$ $\beta -52 21.0$	$-52 35.7$	
17.	10 30 A.M.	C 2	$\alpha -52 36.2$ $\beta -52 14.1$	$-52 25.1$	
23.	9 30 A.M.	C 1	$\alpha -52 39.9$ $\beta -52 24.9$	$-52 32.4$	
23.	11 00 A.M.	C 2	$\alpha -52 33.8$ $\beta -52 19.2$	$-52 26.5$	
23.	11 40 A.M.			$-52 26.2$	General Mean.

From these observations we have the true inclination at these six stations as follows :—

On ice, lat.—65° 49'. Long. 202° 02'	. . .	79° 39' 5
On ice, lat.—63° 23'. Long. 210° 02'	. . .	77° 23' 3
Hobarton		70° 40' 7
Sydney		62° 49' 1
New Zealand		59° 31' 9
Falkland Islands		52° 26' 2

The observations with R. F. 5, at the same stations, and at the same spots on shore, or on the ice, gave as follows :—

	On Ice. Lat. —65° 49'. Long. 202° 02'.	On Ice. Lat. —63° 23'. Long. 210° 02'.	Hobarton.	Sydney.	New Zealand.	Falkland Islands.
Face East	—79° 35' 6	—77° 15' 5	—70° 26' 4	—62° 46' 3	—59° 29' 8	—52° 32' 9
Face West	—80° 39' 2	—78° 20' 3	—71° 20' 3	—63° 44' 3	—60° 27' 9	—53° 34' 7
Mean	<u>—80° 07' 4</u>	<u>—77° 47' 9</u>	<u>—70° 53' 4</u>	<u>—63° 15' 3</u>	<u>—59° 58' 8</u>	<u>—53° 03' 8</u>

We have thus the following index corrections :—

Face East	— 3' 8	— 7' 8	—14' 3	— 2' 8	— 2' 1	+ 6' 7
Face West	+59' 7	+57' 0	+39' 6	+55' 2	+56' 0	+68' 5
Mean correction	<u>+27' 9</u>	<u>+24' 6</u>	<u>+12' 7</u>	<u>+26' 2</u>	<u>+26' 9</u>	<u>+37' 6</u>

and the difference of the results with the face east and face west as follows :—

63' 6	64' 8	53' 9	58' 0	58' 1	61' 8
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From the signs and numerical values of the corrections of the *mean results* with R. F. 5, we may infer that the axis of rotation in this needle deviated from the centre of gravity in the longitudinal direction, so as to cause the south end of the needle slightly to preponderate. From the differences of the results with the face east and face west, it appears that there was also a small deviation in the axis of rotation from the centre of gravity in the perpendicular direction. In the results with the face east, these two sources of error partially counteracted each other, so that the index correction with the face east amounted at no time to more than a very few minutes.

The corrections which have been applied to the observations have been taken from the following table, in which the correction for -70° has been taken as $-5' 8$, and the change in the correction, corresponding to an increase of one degree in the south dip, as $-0' 5$. In forming this table the determinations on land have been allowed a greater weight than the determinations upon the ice, the latter consisting of fewer observations, and being made probably under circumstances less favourable for this particular purpose.

Table of Index corrections for R. F. 5, face East, between -52° and -85° .

Inclination.	Correction.	Inclination.	Correction.
-52°	$+3.2$	-69°	-5.3
-53	$+2.7$	-70	-5.8
-54	$+2.2$	-71	-6.3
-55	$+1.7$	-72	-6.8
-56	$+1.2$	-73	-7.3
-57	$+0.7$	-74	-7.8
-58	$+0.2$	-75	-8.3
-59	-0.3	-76	-8.8
-60	-0.8	-77	-9.3
-61	-1.3	-78	-9.8
-62	-1.8	-79	-10.3
-63	-2.3	-80	-10.8
-64	-2.8	-81	-11.3
-65	-3.3	-82	-11.8
-66	-3.8	-83	-12.3
-67	-4.3	-84	-12.8
-68	-4.8	-85	-13.3

Index Correction of F. C. B. for the Observations of Inclination in the Terror.—The observations of inclination at sea in this ship were all made with the face of the instrument towards the east, and with the marked face of the needle towards the observer. We may examine the index corrections consequently in the same manner, and by comparison with the same complete determinations as in the case of the needle of the Erebus; confining the comparison however to the land stations, because F. C. B. was not observed with at either of the ice stations.

The inclinations taken with this needle were observed both direct and with the aid of deflectors; the deflectors employed were a spare needle as “deflector N” and “deflector S”; and the magnets of the apparatus, either used separately as “magnet N,” or “magnet S,” or conjointly as “magnets N S.” From some instrumental accident, the inclinations observed with “deflector N” were always considerably in defect of the others when the face of the circle was east; with a corresponding excess with the face west, on the few occasions on shore when the observations were made in both positions. As the observations at sea were exclusively with the face east, it has been necessary on this account to consider separately those amongst them which were taken with “deflector N,” and to obtain a distinct index correction for them. We will first examine the index corrections required for the direct observations, and for those with the other deflectors.

The observations with F. C. B. on shore at the four land stations, where the com-

plete process for determining the true inclination was gone through with other needles, were as follows:—

		Hobarton.	Sydney.	New Zealand.	Falkland Islands.
Observed . . .	{ Face East	$-70^{\circ} 17'3$	$-62^{\circ} 22'4$	$-58^{\circ} 50'6$	$-51^{\circ} 38'4$
	{ Face West	$-70 44'8$	$-62 56'5$	$-60 02'8$	$-52 57'2$
Mean		$-70 31'1$	$-62 39'5$	$-59 26'7$	$-52 17'8$
True inclination		$-70 40'7$	$-62 49'1$	$-59 31'9$	$-52 26'3$
Index correction	{ Face East	$-23'4$	$-26'7$	$-41'3$	$-47'9$
	{ Face West	$+ 4'1$	$+ 7'4$	$+ 30'9$	$+ 30'9$
	{ Mean . . .	$- 9'7$	$- 9'6$	$- 5'2$	$- 8'5$
Differences face East and West		$27'5$	$34'1$	$72'2$	$78'8$

The corrections of the *mean results* with F. C. B. at the four stations accord well within the limits of observation error. On examining the differences in the results with the face east and face west, and the corrections severally required in the two positions at the four stations, it appears probable that a very slight derangement of some part of the instrument took place between the observations at Sydney and those at the Bay of Islands, which caused the partial results with the face east and face west to diverge more from each other than they had done previously, but without affecting the mean results. A note which accompanied the observations to England shows that Captain CROZIER considered that some slight change had taken place in the amount of the index correction with the face east, but was unable to assign its date or its cause. In the absence of any distinct evidence in these respects,—and in consideration of the insufficiency of the means of assigning the precise amount of the change,—I have preferred the employment of an arithmetical mean of the index corrections observed at the four stations ($-35'$) during the whole course of the voyage. The uncertainty arising from this source cannot amount to more than a very few minutes in any portion of the voyage.

For the index correction with deflector N we have,

	Hobarton.	Sydney.	New Zealand.	Falkland Islands.
Face East . . .	$-69 33'5$	$-61 36'7$	$-57 58'0$	$-50 54'4$
Face West . . .	$-71 25'9$	$-63 00'7$	$-60 12'3$	$-53 31'3$
Mean	$-70 29'7$	$-62 18'7$	$-59 05'1$	$-52 12'8$
True inclination	$-70 40'7$	$-62 49'1$	$-59 31'9$	$-52 26'3$
Index correction, face East . .	$-67'2$	$-72'4$	$-93'9$	$-91'9$
Mean index correction, face East		$-81'$		

Elements of Calculation of the Intensity Observations.

1. *With Weights.*—The observations of the intensity of the magnetic force, during the period now under consideration, were made in both ships with Mr. Fox's apparatus; those in the Erebus with the same circle which had been used in the previous voyage, and those in the Terror with a circle of the same size as that of the Erebus, being the property of Captain CROZIER, and received by him at Van Diemen Island. The needle employed to show the angles of deflection in the Erebus, marked R. F. 5, was not the same which had been used for that purpose in the voyage of 1840–1841, namely, R. F. 4, which now in its turn was used as a deflector. The weights employed in deflecting the intensity needle were 1, 2, 3, 4, 5 and 6 grains: the angles of deflection obtained with one grain were however too small to yield results of the same satisfactory nature as those derived from the weights from two to six grains, and I have not therefore taken them into the account. The mounted needle in the Terror was marked F. C. B., a spare needle C being used as a deflector, in addition to the deflecting magnets belonging to the apparatus. The weights were 1, $1\frac{1}{2}$, 2, $2\frac{1}{2}$, 3 and $3\frac{1}{2}$ grains.

At Hobarton we have the deflections occasioned by the constant weights on the needle of the Erebus, April 1841, as follows:—

Deflection. Therm.					Deflection. Therm.				
grs.					grs.				
Face East.	2	13	02·8	60	Face West.	2	13	14·5	60
	3	19	37·2	60		3	19	55·5	60
	4	26	47·7	60		4	27	02·7	58
	5	34	23·5	60		5	34	51·5	58
	6	42	55·7	61		6	43	07·3	58

and in the needle of the Terror as follows:—

Deflection. Therm.					Deflection. Therm.				
Face East.	grs.				Face West.	grs.			
	1	12	11·9	60		1	11	42·0	60
	1½	18	29·4	60		1½	17	52·6	60
	2	25	13·7	60		2	24	15·6	60
	2½	31	43·0	60		2½	31	00·7	60
	3	39	02·3	60		3	38	42·3	60
	3½	46	51·3	60		3½	46	06·3	60

At Sydney, in July 1841, the deflections with the same weights were—

EREBUS.								TERROR.															
Deflection.				Ther.	Deflection.				Ther.	Deflection.				Ther.									
grs.					grs.					grs.													
Face East.	{	2	13	57·4	56	Face West.	{	2	14	32·6	64	Face East.	{	1	13	08·8	60	Face West.	{	1	12	44·1	60
		3	21	13·7	55			3	21	51·4	63			1½	20	02·0	60			1½	19	03·3	60
		4	29	09·2	55			4	29	32·1	64			2	27	00·7	60			2	26	01·2	60
		5	37	43·3	55			5	37	38·9	63			2½	34	25·2	60			2½	33	17·7	60
		6	46	51·7	55			6	47	32·4	63			3	42	06·9	60			3	41	35·2	60
						</																	

Taking 1·82 as the provisional value of the intensity at Hobarton (Phil. Trans. 1843, Part II. p. 186)*, we have its value at Sydney, by the needles of the two ships, as follows :—

EREBUS.			TERROR.		
grs.	Face East.	Face West.	grs.	Face East.	Face West.
2	1·703	1·662	1	1·691	1·674
3	1·687	1·667	1½	1·685	1·712
4	1·683	1·680	2	1·708	1·705
5	1·680	1·704	2½	1·692	1·709
6	1·698	1·688	3	1·709	1·715
	<u>1·690</u>	<u>1·680</u>	3½	1·703	1·687
	<u>1·685</u>			<u>1·698</u>	<u>1·700</u>
				<u>1·699</u>	

At the Bay of Islands in New Zealand, in August and October 1841, the deflections were as follows :—

EREBUS.											
August.						October.					
Face East.			Face West.			Face East.			Face West.		
grs.	Deflection.	Ther.	grs.	Deflection.	Ther.	grs.	Deflection.	Ther.	grs.	Deflection.	Ther.
2	14 59·3	59	15	23·3	60	14	43·2	68	15	11·1	64
3	22 47·5	59	23	17·9	59	22	45·0	70	23	17·2	64
4	30 55·0	59	30	26·9	59	30	30·6	70	31	29·2	65
5	40 10·5	58	40	52·0	60	39	59·3	70	40	51·0	65
6	50 38·1	58	51	26·0	61	50	35·0	71	51	38·7	65

TERROR.											
August.						October.					
Face East.			Face West.			Face East.			Face West.		
grs.	Deflection.	Ther.	grs.	Deflection.	Ther.	grs.	Deflection.	Ther.	grs.	Deflection.	Ther.
1	14 03·2	59	13	24·3	59	13	51·7	64	13	26·8	64
1½	21 17·9	59	20	30·5	59	20	53·0	64	20	16·4	64
2	28 22·1	59	27	46·9	59	28	22·4	64	27	38·8	64
2½	36 50·7	59	35	43·0	59	37	05·6	64	35	45·1	64
3	44 58·3	59	44	38·7	59	45	02·2	64	44	47·7	64
3½	55 09·9	59	55	23·7	59	55	19·1	64	55	26·4	64

whence we have the intensity at the Bay of Islands, by the needles of the two ships, as follows :—

* $1·82 + e$ being the true value, in which e is a small correction to be determined hereafter, applicable to the whole series of observations depending on Hobarton as a primary station.

EREBUS.				TERROR.			
August.		October.		August.		October.	
grs.	Face East.	Face West.	Face East.	Face West.	grs.	Face East.	Face West.
2	1.590	1.571	1.620	1.593	1	1.584	1.592
3	1.578	1.568	1.583	1.570	1½	1.601	1.595
4	1.597	1.633	1.619	1.586	2	1.633	1.605
5	1.594	1.590	1.603	1.591	2½	1.596	1.607
6	1.604	1.591	1.608	1.588	3	1.622	1.619
	<u>1.593</u>	<u>1.591</u>	<u>1.607</u>	<u>1.586</u>	3½	1.618	1.594
	<u>1.592</u>		<u>1.596</u>			<u>1.609</u>	<u>1.602</u>
		<u>1.594</u>				<u>1.605</u>	<u>1.614</u>
							<u>1.609</u>
						<u>1.607</u>	

At Port Louis in the Falkland Islands, in July and August 1842, the deflections were—

EREBUS.									
April.					August.				
	Deflection.	Ther.	Deflection.	Ther.	Deflection.	Ther.	Deflection.	Ther.	
Face East.	2	18 31.1	45	Face West.	18 50.4	42	Face East.	17 57.1	37
	3	27 42.7	45		28 30.0	42		27 43.3	37
	4	37 58.5	43		38 51.0	41		37 40.4	37
	5	48 55.9	43		51 27.9	41		49 31.4	38
	6	66 49.8	43		68 40.3	41		67 23.4	38
Face East.	18 32.9	39	Face West.	28 26.6	40	Face East.	39 05.3	40	
	28 26.6	40		51 19.2	40		69 35.7	40	
	39 05.3	40							
	51 19.2	40							
	69 35.7	40							

TERROR.												
April.				July.				August.				
	Deflection.	Ther.	Deflection.	Ther.	Deflection.	Ther.	Deflection.	Ther.	Deflection.	Ther.		
Face East.	1	16 56.5	43	Face West.	16 14.1	43	Face East.	16 51.2	41	Face West.	16 26.1	41
	1 1/2	25 36.6	43		24 36.9	43		25 34.3	41		24 27.9	41
	2	34 47.2	43		33 44.9	43		34 47.8	41		33 49.5	41
	2 1/2	45 34.1	43		44 31.3	43		45 29.7	41		44 17.1	41
	3	57 39.1	43		58 17.8	43		57 48.7	41		58 19.5	41
Face East.	17 00.4	38	Face West.	25 37.3	38	Face East.	34 24.4	38	Face West.	16 15.4	38	
	25 37.3	38		34 24.4	38		33 57.8	38				
	34 24.4	38		45 20.1	38		44 32.3	38				
	45 20.1	38		57 43.6	38		57 35.7	38				
	57 43.6	38										

whence we have the intensity at Port Louis, by the needles of the two ships, as follows:—

EREBUS.				TERROR.			
April.		August.		April.		July.	
grs.	Face East.	Face West.	Face East.	Face West.	grs.	Face East.	Face West.
2	1.291	1.288	1.330	1.306	1	1.316	1.316
3	1.311	1.296	1.310	1.299	1½	1.331	1.338
4	1.331	1.315	1.339	1.309	2	1.356	1.342
5	1.361	1.326	1.347	1.329	2½	1.336	1.334
6	1.345	1.332	1.339	1.324	3	1.353	1.333
	<u>1.328</u>	<u>1.311</u>	<u>1.333</u>	<u>1.313</u>		<u>1.338</u>	<u>1.332</u>
	<u>1.320</u>		<u>1.323</u>			<u>1.340</u>	<u>1.331</u>
		<u>1.322</u>				<u>1.336</u>	<u>1.341</u>
						<u>1.336</u>	<u>1.334</u>

Besides the four land stations at which the intensities shown by the needles of the two ships have been thus compared, we have also one ice station in lat. $-65^{\circ} 47'$, long. $202^{\circ} 08'$, at which similar comparisons may be instituted. The deflections and intensities were as follows:—

EREBUS.					TERROR.				
		Deflection.	Ther.	Intensity.			Deflection.	Ther.	Intensity.
Face East.	grs. 2	12 13.0	50	1.940	Face East.	grs. 1	11 25.4	53	1.940
	3	18 32.4	54	1.921		1½	17 08.3	53	1.957
	4	24 49.3	54	1.952		2	23 02.9	53	1.979
	5	32 02.4	54	1.936		2½	29 16.2	53	1.955
	6	39 31.4	55	1.946		3	36 17.4	53	1.935
				<u>1.939</u>					<u>1.932</u>
									<u>1.950</u>

Collecting these several results in one view, we have as follows:—

	EREBUS.	TERROR.	DIFFERENCE.
Intensity at Hobarton	1.82	1.82	(Erebus in defect.)
Intensity at Sydney	1.685	1.699	.014 or 8 parts in 1000
Intensity at the Bay of Islands	1.594	1.607	.013 or 8 parts in 1000
Intensity on ice, lat. $-65^{\circ} 49'$, long. $202^{\circ} 02'$	1.939	1.950	.011 or 7 parts in 1000
Intensity at Port Louis, Falkland Islands .	1.322	1.336	.014 or 10 parts in 1000

The difference between the results given by the needles of the two ships, though small, is so consistently shown at all the stations during the voyage, that we cannot hesitate to attribute it to the occurrence of a change of corresponding amount in the magnetism of one needle or the other, between the observations at Hobarton in April 1841, and those at Sydney in July of the same year. If we further compare the intensities observed at sea by the two ships on the passage from Hobarton to Sydney, we find that a similar difference prevails in them; and we are therefore led to the conclusion, either that the needle of the Terror gained, or that the needle of the Erebus lost, a very small portion of magnetism, in the period between the observations at Hobarton in April 1841, and the departure of the Expedition from that port in the following July. Now experience has shown that a loss of magnetism is no unfrequent occurrence, whilst a gain is extremely rare, happening only, as far as we know, from such an accident as the contact of a needle with a more powerful magnet than itself. We may therefore conclude with great probability that the needle of the Erebus sustained a small loss of magnetism between April and July 1841, antecedent to all the observations of the voyage, causing the intensities derived with it, *when computed in reference to the angles of deflection observed at Hobarton in April 1841*, to require to be increased about one hundredth part, or more precisely 8 parts in 1000, in order

to bring them into strict relation with 1·82, taken as the value of the force at Hobarton. This correction being applied, all the intensities observed throughout the voyage by the two ships are in accordance (subject only to errors of observation), forming a consistent series of relative determinations, resting on 1·82 and 1·336, assumed provisionally as the values of the intensity at Hobarton and Port Louis, the commencing and concluding stations of the series. The correction is made in the Table which exhibits the intensities observed on board the two ships, and the geographical positions to which they belong; it is also made in the results inserted in the Map. The correctness of the values assumed at the base stations, 1·82 at Hobarton and 1·336 at Port Louis, remains to be proved by absolute determinations which have yet to be made at those two stations. The absolute intensities observed by the Expedition itself, with the instruments and according to the method prescribed in the instructions of the Royal Society, certainly have not the necessary precision. In the preceding Number of these Contributions are stated the results of five determinations which were obtained by Captain Ross at Hobarton in 1840 and 1841, with the 15-inch magnets of his observatory magnetometers; and of twenty-two determinations obtained by Lieut. KAY at the magnetic observatory at that station, with similar instruments, in 1841 and 1842. Captain Ross's mean result was 4·573, the partial results varying from 4·491 to 4·626. Lieut. KAY's mean result in 1841 was 4·553, the partial results (ten in number) varying from 4·509 to 4·601; and in 1842 4·513, the partial results (twelve in number) varying from 4·443 to 4·568. In 1843 Lieut. KAY received the *auxiliary apparatus* supplied in compliance with the *revised instructions* of the Royal Society, published in 1842. The magnets of this apparatus were 12 inches in length. The following Table exhibits the results obtained with this instrument in thirteen determinations made with it, between June 23rd and July 1st, 1843. Each determination is deduced from two series of observations of deflection; in the first six instances the distances were 4·505 and 6·005 feet; in the remainder, 4·0 and 5·3 feet. The moment of inertia of the deflecting magnet was computed from the length, breadth and mass of the bar.

June 23.	4·509	June 27.	4·557
24.	4·515	28.	4·505
24.	4·528	28.	4·504
26.	4·510	29.	4·549
26.	4·523	29.	4·527
27.	4·583	30.	4·466
		July 1.	4·479

Mean of the 13 determinations 4·520

Here also it is obvious, from the discrepancy of the partial results, that the angles of deflection afforded by these magnets at the prescribed distances, viz. the least distance being not less than four times the length of the bar, were still too small; and that before any final conclusion be arrived at, it is desirable that we should await the

results which will be obtained with the smaller apparatus described by Lieut. RIDDELL in his "Magnetical Instructions for the use of Portable Instruments," &c. In this apparatus the suspended and deflecting magnets are respectively 3·0 and 3·67 inches in length. Meanwhile we may derive, as a provisional value, the arithmetical mean of the four mean results already stated; allowing to each an equal weight, we have,

ROSS, in 1840-1841, 15-inch magnets, 4·573	} Mean <u>4·54</u>
KAY, in 1841, do. do. 4·553	
KAY, in 1842, do. do. 4·513	
KAY, in 1843, 12-inch magnets, 4·520	

which, with the other necessary data stated in the preceding Number of these Contributions, would give the value of the total intensity at Hobarton 1·81 to 1·372 in London*.

* Since these pages were written I have received the details of the observations of ten distinct determinations of the absolute horizontal intensity at the magnetic observatory at Hobarton, made in August 1843 with deflecting and suspended magnets respectively of 9·18 inches and 7·50 inches in length. The deflecting distances were the same throughout, being 3·2893 and 4·3393 feet. The calculation of these observations not having been yet received from Lieut. KAY, the results have been computed by Lieut. RIDDELL, R.A., F.R.S., so far as the materials hitherto furnished permit. They give the value of X' ;—being the absolute horizontal intensity (X), uncorrected for the difference in the magnetic moment of the deflecting bar produced by the earth's inducing action in the different positions in which the bar is placed in the experiments of deflection and in those of vibration; viz. 1° perpendicular to the magnetic meridian, and 2° in the plane of the meridian. We owe the suggestion of a correction due to this cause to Dr. LAMONT: but the necessary data for computing it, for the particular bars employed by Lieut. KAY on this, or on the former occasions, have not yet been received. Observations made at the Cape of Good Hope and at Woolwich, with similar bars, have given results which show that the correction may possibly prove to be of nearly the same amount for the larger and smaller bars, in which case the relative values will be but little affected, and we may estimate that the value of X at Hobarton will be about 0·02 less than X' . In the expression which has been employed in these Contributions for the absolute horizontal intensity ($1·82 + e$ at Hobarton and $3·72 + e$ at London, e being a small quantity to be supplied hereafter), the correction here referred to will form a portion of e . The following Table exhibits the abstract of the observations made in August 1843 with 9·18 and 7·50 inch bars.

Gottingen Mean Time.	Deflecting Magnet.			Values of X' .	Bifilar Magnetometer. $k=000229$. $g=000224$.	
	No.	Value of m' .	Temperature during deflection.		Reading.	Temp.
1843. Aug. 20 19·0	9·18 inch.	6·256	54·6	4·5052	165·1	52·0
21 11·5	9·18 inch.	·259	49·6	·5034	168·6	49·1
21 16·5	9·18 inch.	·251	51·9	·5043	165·3	49·1
21 19·5	9·18 inch.	·261	53·7	·4993	168·3	50·0
22 11·0	9·18 inch.	·227	48·0	·5177	165·4	49·3
22 19·5	9·18 inch.	·243	54·5	·5025	164·6	50·7
23 10·8	9·18 inch.	·259	50·7	·4884	161·0	51·2
23 18·1	9·18 inch.	·244	52·4	·5005	162·2	51·0
23 19·1	9·18 inch.	·240	52·0	·4982	163·9	51·3
25 11·4	9·18 inch.	·252	49·4	·4953	165·3	51·5
		6·249	51·7	4·5015	165·0	50·5

The mean value of the results, 4·501, is considerably different from the mean deduced in the text from all

At the Falkland Islands there were two determinations of the absolute horizontal intensity made by Captain Ross at the Magnetic Observatory at Port Louis, one in September 1842, being 6·87, and a second in November of the same year, being 6·32. They were both made with 15-inch magnets; the angles of deflection were observed at four distances, but amounted only to 56'·8, 31'·9, 21'·4, and 12'·9 in the first experiment, and to 1° 49'·9, 1° 01'·6, 41'·5, and 25'·1 in the second experiment.

These values of the horizontal intensity would give that of the total intensity at Port Louis respectively 1·609 and 1·367. It is obvious that we can draw no conclusion whatsoever from these numbers, and that we must wait for the confirmation or correction of the value given by the needles of Mr. Fox's instrument, until absolute determinations can be procured with instruments capable of affording more satisfactory results. Steps have been taken to obtain such determinations at the Falkland Islands from Captain SULLIVAN, R.N., and at Sydney and New Zealand from the Surveying Expedition under Captain BLACKWOOD, R.N.; when these arrive, we may learn whether any and what final correction will require to be applied to the intensities now provisionally deduced from the observations with Mr. Fox's needles, in the Erebus and Terror. We may expect to receive these determinations before the time when the results now presented to the Royal Society will have to be combined with those of the preceding and succeeding years, in a general calculation of the magnetic lines in the southern hemisphere.

2. *With Deflectors.*—In the Erebus, the spare needle R. F. 4 was employed,—as “deflector S,” with its south pole opposite to the division of the circle which the south pole of the mounted needle had previously indicated as the dip;—and as “deflector N,” with its north pole similarly applied to the opposite division of the circle. The angles of deflection varied in different localities during the voyage, in round numbers as follows:—Deflect. S from 52° to 71°; and deflect. N from 49° to 67°. For obtaining the equivalent weights to the deflecting force of the deflectors at these angles, we have the comparative observations with deflectors and weights at Hobarton, Sydney, New Zealand, the Falkland Islands, and on the ice in lat. —65° 47', long. 202° 08'. The angles of deflection caused by the weights have been already stated;

the preceding observations; yet from the improvement which it is natural to suppose practice must have made in the observers, and from the reduced discrepancies of the partial results with the smaller bars, the mean of the ten results in August 1843 would seem entitled to a preference over the earlier and more numerous results. Judging by what has been done at Woolwich with the 2·45 and 3 inch magnets, and at the Cape of Good Hope with 3·0 and 3·67 inch, we may expect with them a still further and considerable reduction in the discrepancies of the partial results; but it would not be safe, with the comparisons which we have now before us, to feel full confidence that there will be no apparently constant or systematic difference between the results of the larger and smaller bars. Reviewing the whole subject, we can as yet, therefore, only consider ourselves as being in progress towards such accuracy in determining the ratio of the intensity at different places by the absolute method, as shall be superior to that with which it was previously obtained by the employment of well-selected needles in relative determinations.

those by the deflectors, with the equivalent weights deduced from the comparison, are collected in the following Table.

Station.	Date.	Intensity deduced by weights.	Angles of deflection by		Equivalent weights.	
			Def. S.	Def. N.	Def. S.	Def. N.
Hobarton	April 1841	1·82	56 28·6	53 02·6	grs. 7·39	grs. 7·08
Sydney	July 1841	1·685	59 10·2	55 37·0	7·05	6·77
New Zealand....	Aug. and Oct. 1841	1·594	61 46·9	57 59·0	6·84	6·58
On ice	January 1842	1·939	54 03·1	50 35·0	7·65	7·30
Falkland Islands .	April and Aug. 1842	1·322	71 11·8	67 10·3	6·10	5·93

By projecting these angles and weights, and proceeding in the manner described in the Third Number of these Contributions*, the values of w' in the following Table were obtained for each deflector, corresponding to each angle of deflection v' ; and employing these values of w' , the intensities I' entered in the general table of observations have been computed by the formula

$$I' = \frac{1·82 \sin 56 28·6}{7·39} \cdot w' \operatorname{cosec} v' = 2·053 w' \operatorname{cosec} v'.$$

Besides the observations with the spare needle R. F. 4, employed as a deflector, angles of deflection were occasionally observed with the magnets N and S, belonging to the apparatus of the Erebus, used conjointly; their magnetism, however, was so much inferior to that of R. F. 4, that, even when both were used together, their joint effect was less than the half of either pole of R. F. 4; their results would consequently be much inferior in precision to those of R. F. 4, and I have not therefore employed them.

Def. S.						Def. N.					
v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .
52	grs. 7·87	59	7·11	66	6·47	49	7·49	56	6·76	63	6·19
53	7·76	60	7·01	67	6·39	50	7·38	57	6·67	64	6·13
54	7·65	61	6·91	68	6·31	51	7·27	58	6·57	65	6·06
55	7·54	62	6·82	69	6·24	52	7·17	59	6·48	66	6·00
56	7·43	63	6·73	70	6·17	53	7·07	60	6·40	67	5·94
57	7·32	64	6·64	71	6·10	54	6·97	61	6·33		
58	7·21	65	6·55	72	6·03	55	6·86	62	6·26		

In the Terror, the spare needle marked C was employed both as “deflector N” and “deflector S.” The magnets belonging to the apparatus were also used, N separately, and N and S conjointly. Observations were also occasionally made with magnet S, but its magnetism was so feeble, and the deflections obtained with it consequently so small in comparison with the others, that the results are not entitled to the same confidence, and have not therefore been taken into the account. The equivalent weights have been obtained, as in the Erebus, from the comparative observations with weights and deflectors at Hobarton, Sydney, New Zealand, the Falkland

* Philosophical Transactions, 1842, Art. II.

Islands, and on the ice in lat. $-65^{\circ} 47'$, long. $202^{\circ} 08'$. I have also, in the case of the Terror, availed myself of a comparison of the weights and deflectors made on the 3rd, 4th and 5th of December 1841, at sea, when the weather was extremely favourable, and the ship did not materially change her position. From the observations on these days we have as follows:—

December 1841.	Intensity deduced by weights.	Angles of deflection by			
		Def. N.	Def. S.	Mag. N.	Mag. N S.
3 A.M.	1.783	36 55.9	34 06.7	30 44.1	40 52.8
3 P.M.	1.778	36 51.6	34 06.3	30 46.1	40 45.8
4	1.773	36 { 41.8 44.7	34 22.0	30 48.7	40 56.3
5	1.779	36 18.3	34 29.4	30 46.1	40 54.9
Mean ..	1.778	36 42.5	34 16.0	30 46.2	40 52.5

The several comparisons from which the equivalent weights are derived, together with the weights so derived, are collected in the following Table.

Station.	Date.	Intensity deduced by weights.	Angles of deflections by				Equivalent weights.			
			Deflector N.	Deflector S.	Magnet N.	Magnets N S.	Deflector N.	Deflector S.	Magnet N.	Magnets N S.
Hobarton	April 1841 ..	1.820	36 00.6	33 23.0	30 14.0	40 05.5	grs. 2.793	grs. 2.613	grs. 2.391	grs. 3.059
Sydney	July 1841 ..	1.699	38 05.9	35 15.7	31 47.2	41 45.3	2.736	2.560	2.336	2.953
New Zealand ..	Aug. and Oct. 1841	1.608	39 36.8	36 57.8	32 50.8	42 58.4	2.675	2.525	2.276	2.861
At Sea	Dec. 3, 4 and 5, 1841	1.778	36 42.5	34 16.0	30 46.2	40 52.5	2.773	2.613	2.374	3.036
On Ice	Jan. 16, 1842	1.949	33 47.6	31 16.1	28 52.7	38 45.7	2.829	2.640	2.456	3.184
Falkland Islands	April, July and Aug. 1842	1.336	44 38.2	41 57.1	35 59.0	46 14.0	2.442	2.324	2.042	2.510

The equivalent weights for each deflector, and for each half degree of deflection, have been obtained in the manner already described, for the angles of deflection and equivalent weights in the preceding Table, and are subjoined; by their aid the intensities I' entered in the general table of observations have been computed by the formula

$$I' = .3832w' \operatorname{cosec} v'.$$

Def. N.				Def. S.				Magnet N.				Magnets N S.			
v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .	v' .	w' .
33 00	grs. 2.840	39 30	grs. 2.682	31 00	grs. 2.644	37 30	grs. 2.504	28 00	grs. 2.482	34 30	grs. 2.166	37 00	grs. 3.268	43 30	grs. 2.816
33 30	2.834	40 00	2.660	31 30	2.639	38 00	2.485	28 30	2.464	35 00	2.126	37 30	3.240	44 00	2.766
34 00	2.826	40 30	2.638	32 00	2.634	38 30	2.464	29 00	2.446	35 30	2.085	38 00	3.210	44 30	2.714
34 30	2.817	41 00	2.615	32 30	2.627	39 00	2.444	29 30	2.426	36 00	2.040	38 30	3.180	45 00	2.660
35 00	2.809	41 30	2.593	33 00	2.619	39 30	2.423	30 00	2.406			39 00	3.148	45 30	2.604
35 30	2.800	42 00	2.571	33 30	2.611	40 00	2.403	30 30	2.387			39 30	3.114	46 00	2.544
36 00	2.790	42 30	2.548	34 00	2.602	40 30	2.382	31 00	2.367			40 00	3.081	46 30	2.460
36 30	2.777	43 00	2.524	34 30	2.591	41 00	2.361	31 30	2.346			40 30	3.049		
37 00	2.765	43 30	2.488	35 00	2.580	41 30	2.341	32 00	2.323			41 00	3.016		
37 30	2.753	44 00	2.473	35 30	2.567	42 00	2.321	32 30	2.297			41 30	2.981		
38 00	2.738	44 30	2.448	36 00	2.554			33 00	2.268			42 00	2.944		
38 30	2.721	45 00	2.423	36 30	2.538			33 30	2.236			42 30	2.905		
39 00	2.702			37 00	2.523			34 00	2.203			43 00	2.863		

General Remarks.—If we take a general view of the magnetic DECLINATION in the southern hemisphere, particularly in the best-known portion of it, comprised between the tropics and the Antarctic Circle, we find that the phenomena present the same obvious and decided features of a duplicate system as do those of the northern hemisphere. If, following any of the geographical parallels, we carry our attention round the hemisphere, we find it divided into four spaces, in which opposite characteristics in regard to the direction of the needle alternately present themselves. In two of the spaces the change in the pointing of the needle, as the space is traversed in the direction of the parallel, is continuous and progressive towards the west, and in the other two continuous and progressive towards the east. If, for example, commencing with the meridian of 30° E. or thereabouts, we trace the parallel of -45° round the hemisphere, always proceeding in an easterly direction till we return to the meridian at which we began, we shall find that we first pass through a space in which the direction of the north end of the needle becomes progressively more and more *easterly*, either by the decrease of westerly or increase of easterly declination; we next pass into a second space, on entering which the continuity is broken, the progressive movement of the north end of the needle towards the east is arrested, and its direction becomes now more and more *westerly* as we advance; thence we pass, successively, into a third space which has the same characteristic as the first, and into a fourth which has the same as the second.

The spaces here spoken of must be distinguished from those which are characterized by the exclusive prevalence of either east or west declination: they have a more simple and pure magnetical relation, implying the predominance within each space of one or the other of the two systems of magnetic forces which govern the direction of the needle. It may happen, or it may not happen, that in one of these spaces the direction of the needle may coincide in some point or points with the *geographical* meridian; when this occurs, the space will comprise both east and west declination; when it does not happen, the declination throughout the space will be exclusively east or exclusively west as the instance may be: but in either case, the change in the direction of the needle is always continuous and uniform in character throughout the space. It is well known that if the magnetic declination be computed on the supposition of a single central magnetic axis, there will be found two, and only two such spaces in each hemisphere. The systematic discordance which the declinations in the *northern* hemisphere presented when compared with the declinations so computed, and their agreement with the phenomena deducible from a double system of forces, led HALLEY to embrace the latter hypothesis. The declinations in the southern hemisphere present an arrangement strictly analogous to that in the northern, and conduct to the same conclusion, be that conclusion what it may.

If, with HALLEY, we view the declinations in the Southern Pacific as principally influenced by the weaker system of forces, or by that to which is also to be ascribed the high intensity of the magnetic force in the same quarter, we should be prepared

to expect that if the geographical limits of the adjacent spaces, having the characteristics referred to, were determined at different epochs, the alteration in the position of the spaces, if any, would show the existence of a secular change in the system itself; that it would indicate the direction of such change; and, if the intervals were sufficiently long in reference to the precision with which the determinations were made, the average rate of the movement of translation might also be inferred.

In this view a knowledge of the geographical position of the limiting lines, or of lines drawn so as to separate one of these spaces from the next, may have a particular value. In the part of the Pacific Ocean which is now referred to, the *separating lines*, as for distinction they may be called, coincide nearly in direction with geographical meridians, and are therefore crossed nearly at right angles by vessels pursuing a course from east to west, or from west to east. Prior to our own times, the epoch of Captain Cook's voyages is perhaps that in which the observations of the declination in the Southern Pacific may be regarded with the most confidence. The determinations of that period have been collected by M. HANSTEEN into a map, of which he assigns the year 1770 as the mean epoch. It is one of those published in the Atlas of the Magnetismus der Erde, and comprehends the results obtained by BYRON, CARTERET, WALLIS, COOK in three voyages, EKEBERG also in three voyages, and ABERCROMBIE. If in this map we draw lines separating the spaces which have the opposite magnetic characteristics referred to, and compare them with the corresponding lines which we may draw in ERMAN's map of the Declination in 1827-1830, published in the Magnetic Instructions of the Royal Society, we find an effect of secular change very distinctly shown in the altered position of the separating lines. These lines, A and B, are drawn in the accompanying Plate*, where the two epochs, 1770, and 1827-1830, are brought into comparison. In the map of 1827-1830, the separating lines occupy a considerably more westerly position than in the earlier map, the difference amounting to about 10° of longitude. Hence we are led to the conclusion, that the spaces in the Southern Pacific, distinguished by certain magnetic characteristics, undergo a movement of translation, of which the general direction is from east to west. This direction is the opposite to that in which the change is known to take place in the corresponding quarter in the northern hemisphere (viz. in the Siberian quarter), where the secular movement is from west to east.

We are not without earlier, though possibly it may be supposed less precise, evidence of the effect of secular change in the Southern Pacific. From HALLEY's chart of the variation lines for 1700, we are enabled to draw the separating line B for that epoch, when we find it to have been between the longitudes of 305° and 310° . In a still earlier map drawn by HANSTEEN for the year 1600 (Magnetismus der Erde, Atlas, No. 1), representing the observations of the very able and scientific navigators of that period, we find the position of the same line to have been about 333° of east longitude.

In the observations of Captain Ross's voyage, we have the most recent evidence of the progressive westerly movement of the magnetic phenomena in the Southern

Pacific. The separating lines A and B, deducible from the observations in 1842, are seen in the Plate to be in both cases considerably to the west of those derived from the observations of 1827–1830.

The whole body of evidence therefore, from the earliest observations to the latest, is consistent in showing a progressive movement to the westward of the spaces in the Southern Pacific, characterized by certain magnetic peculiarities, which in HALLEY'S view indicated the proximity and predominance of the weaker system of forces. It is worthy of notice that the rate of progression, deduced from the changes of position shown at the several epochs, differs much less from a uniform rate than might have been anticipated from the nature of the evidence we possess, even supposing the actual rate to have been uniform in nature; whilst the magnitude of the whole change which appears to have taken place since the phenomenon became the subject of observation, in round numbers 50° of longitude in two centuries and a half, can scarcely fail to fix the attention. These are facts which, when the true physical causes of the magnetism of the globe shall occupy the earnest attention of philosophers, will probably attain an importance which at present perhaps we scarcely sufficiently estimate. But an endeavour to place distinctly before our minds facts of which the explanation must be deemed an essential condition of a satisfactory solution of this great problem, may not be without its use even at the present time. It may be also useful to call the attention of navigators to the value which may hereafter attach to determinations which may be made with instruments which are on board every ship, and in constant employ for the ordinary purposes of navigation. The position of the lines separating the spaces which have been the subject of discussion, has the advantage of being even more easily determined by observations on board ship than that of any particular declination line; in crossing them, the declination, if previously decreasing, will then begin to increase, and if previously increasing will begin to decrease; the determination is therefore independent of compass error, which is a much more prevalent source of error than is generally supposed; and if the ship's course be steady for some days together, which in the latitudes in question is very frequently the case, it is also in a great measure independent of the disturbance occasioned by the ship's iron. A very cursory inspection of the general table of the declinations observed by the Erebus and Terror suffices to show that they must have crossed the separating line (A) about the 15th of March 1842, when their latitude was about -59° and longitude 221° ; and the line (B) about the 27th or 28th of the same month in latitude about -59° , and longitude 275° *.

Should the circumstance occur that one of the separating lines in the course of its progressive change of place should pass over a magnetic observatory, the epoch of its passage would be precisely determined. There is some reason for believing that

* The line A passes through the culminating points of the southerly inflexion of the declination lines, of which the present position is shown in the Declination Map at the close of this paper to be about 220° east longitude. The line B passes through the culminating points of the northerly inflexion of the declination lines about the longitude of 276° .

such an event is now taking place at the Cape of Good Hope. If we examine ERMAN's map of the Declination in 1827–1830, published in the magnetic instructions of the Royal Society, we find one of the separating lines in the neighbourhood of the Cape of Good Hope, and if we compare this map with those of earlier epochs, we find the position of that line progressively more and more to the east as we ascend in the order of time. Hence we should be led to expect that about this period it might be found to pass over the meridian of the Cape. The observations which have been made daily at the magnetic observatory at the Cape, since its establishment in 1841, give reason to believe that the westerly declination which had been increasing for above two centuries, attained its maximum in the year 1842 or 1843. In April 1841 the declination was $29^{\circ} 05'$ west, in and April 1844 $29^{\circ} 06'$ west*. The earliest observations at the Cape with which I am acquainted, are those of DAVIS in 1605, and KEELING in 1609. (Purchas, Book iv. ch. 6. § 1. and Book iii. ch. 6. § 4.) According to these observations the declination in 1605 was $0^{\circ} 30'$ east, and in 1609 $0^{\circ} 12'$ west†. The line of no declination probably therefore passed over the Cape about the year 1607, and in 235 years the westerly declination has increased from 0° to 29° , (omitting the odd minutes,) or at an annual average rate of $7'4$. Observations at several intermediate epochs show that the progression of this change was at least not very far from being an uniform one. If we divide the whole period into four equal parts, we should have

In the year 1607	$0^{\circ} 0'$
In the year 1666	$7^{\circ} 15' W.$
In the year 1725	$14^{\circ} 30' W.$
In the year 1784	$21^{\circ} 45' W.$
In the year 1843	$29^{\circ} 0' W.$

In the appendix of HANSTEEN's *Magnetismus der Erde*, p. 24, we have the record of actual observations as follows :—

In the year 1667	$7^{\circ} 15' W.$
In the year 1724	$\left\{ \begin{array}{l} 16^{\circ} 27' W. \\ 16^{\circ} 18' W. \end{array} \right.$
In the year 1780	$22^{\circ} 16' W.$

We may therefore conclude that the westerly declination at the Cape, which for above 200 years had increased at an average rate of about $7'4$ a year, or a degree in about eight years, has been for the last three years nearly stationary, having arrived at a maximum of 29° and a few minutes about the year 1843; and that a decreasing progression may now be expected‡. Ships passing the Cape, on a voyage to the

* The observations at the magnetic observatory at the Cape of Good Hope, preparing for the press, will show the mean declination in each month of the years referred to.

† See also, for the latter observation, HANSTEEN's *Magnet. der Erde*. Anhang. S. 146.

‡ Captain FITZROY observed $28^{\circ} 30'$ in 1836; at that epoch, consequently, the maximum had not been reached. Sir EDWARD BELCHER, in 1842, observed $29^{\circ} 13'$.

east, will find that the westerly variation, which increases the whole way from the Brazils to about the meridian of the Cape, begins there to diminish, and continues to diminish, passing into easterly variation increasing, for above 100 degrees of longitude east of the Cape. The separating line which now passes through the Cape divides spaces distinguished by opposite magnetic characteristics; on the west side of the Cape the north end of the needle moves to the west, and on the east side to the east, as east longitude increases.

The maps which exhibit the results of the observations in the two ships, of the Declination, Inclination and Intensity, in the voyage of 1841–1842, and the isogonic, isoclinal, and isodynamic lines traced approximately in conformity with them, are a continuation of the maps published in No. V., which embodied in a similar manner the results of the preceding voyage. The results in the Erebus are distinguished from those in the Terror by a different character, for the purpose of permitting the degree of accordance in the two series of independent determinations to be readily judged of by the eye. These maps afford the best reply to those who have expressed doubts of the success of observations of the inclination and intensity made at sea.

Magnetic lines, drawn from observations made in parts of the globe to which observation had not previously extended, are the proper test by which we may judge of the degree of approximation with which the values of the numerical elements have been obtained in a general mathematical theory of terrestrial magnetism, such as M. GAUSS's. The portion of the observations of the Antarctic Expedition which has been placed before the Royal Society in No. V. and in the present number of these Contributions, permits us already to form some conclusion on this point. Plate XIII. exhibits the lines of one of the magnetic elements, i. e. the intensity, computed by M. GAUSS's theory, and drawn in Plates XVIII. and XIX. of the *Atlas des Erdmagnetismus*, compared with the lines which are the direct results of observation.

The very imperfect resemblance between the two systems of lines is of course no impeachment of the sufficiency of the theory, with corrected numerical elements, to represent the natural phenomena in parts of the globe which observation may not have reached. The degree of approximation to which it will do this must depend upon the extent and correctness of the observation-basis from whence the numerical elements are derived, and upon the order of the magnitudes comprehended in the calculation.

The evidence which the plate affords, that the calculations in the elaborate work referred to differ so widely from the facts in the southern latitudes, shows how much observations were wanting in those latitudes for the purpose of perfecting the theory; and is an ample justification (if indeed any justification were necessary) of the exertions which the last few years have witnessed to obtain them.

Since these pages were written I have received from Mr. ARCHIBALD SMITH the following note. Regarding it as a continuation of the memorandum with which he

was so obliging as to favour me, printed in the last number of these Contributions, I avail myself of this opportunity of giving it an early circulation.

“The apparent changes in the values of the constants a , b , c and d , in the Erebus and Terror (Contributions, No. V., p. 153), seem to show that those vessels had an appreciable quantity of magnetism, which was so far permanent, as to retain for a considerable time traces of the inductive force to which they had been exposed, and perhaps some strictly permanent magnetism. It seems, therefore, desirable to introduce into the expressions in the memorandum printed at p. 147 of Contribution No. V., terms which will represent such forces.

“Suppose, then, as in the memorandum, that ϕ represents the total magnetic force of the earth at the place of observation, θ the inclination, ζ the azimuth of the ship's head, reckoning from N. to W., and that ϕ' , θ' , ζ' represent the values of the same quantities shown by an instrument at a fixed position in the vessel, and affected by the attraction of the iron in the vessel; and let P, Q, R represent the attraction of the permanent magnetism in the vessel to the bow, to the starboard side, and vertically downwards. The fundamental equations of the former memorandum become by the introduction of these terms,

$$\begin{aligned}\phi' \cos \theta' \cos \zeta' &= \phi [A' \cos \theta \cos \zeta + B \cos \theta \sin \zeta + C \sin \theta] + P \\ \phi' \cos \theta' \sin \zeta' &= \phi [D \cos \theta \cos \zeta + E' \cos \theta \sin \zeta + F \sin \theta] + Q \\ \phi' \sin \theta' &= \phi [G \cos \theta \cos \zeta + H \cos \theta \sin \zeta + K' \sin \theta] + R.\end{aligned}$$

“In these equations A' , B , C , D , E' , F , G , H and K' are constants depending on the distribution of the soft iron in the ship, and perhaps on the temperature and other circumstances.

“If we suppose, as before, that the soft iron is symmetrically disposed, the equations (1.) (2.) and (3.) of the former memorandum become,

$$\frac{\phi' \cos \theta' \cos \zeta'}{A' \phi \cos \theta} = \cos \zeta + a \tan \theta + \frac{P}{A' \phi \cos \theta} \quad \dots \quad (1.)$$

$$\frac{\phi' \cos \theta' \sin \zeta'}{A' \phi \cos \theta} = b \sin \zeta + \frac{Q}{A' \phi \cos \theta} \quad \dots \quad (2.)$$

$$\frac{\phi' \sin \theta'}{A' \phi \cos \theta} = c \cos \zeta + d \tan \theta + \frac{R}{A' \phi \cos \theta} \quad \dots \quad (3.)$$

“Let H represent the horizontal force $= \phi \cos \theta$, H' the affected horizontal force $= \phi' \cos \theta'$, and let $a \tan \theta + \frac{P}{A'H} = L$, $\frac{Q}{A'H} = M$, and $d \tan \theta + \frac{R}{A'H} = N$. The last equations become

$$\frac{H'}{A'H} \cos \zeta' = \cos \zeta + L \quad \dots \quad (1 a.)$$

$$\frac{H'}{A'H} \sin \zeta' = b \sin \zeta + M \quad \dots \quad (2 a.)$$

$$\frac{H' \tan \theta'}{A'H} = c \cos \zeta + N \quad \dots \quad (3 a.)$$

“ By the introduction of the same quantities, the equations numbered from (4.) to (14.) in the former memorandum become

$$\frac{H'}{A'H} = \cos \zeta \cos \zeta' + b \sin \zeta \sin \zeta' + L \cos \zeta' + M \sin \zeta' \quad . \quad . \quad . \quad (4.)$$

$$(\cos \zeta + L) \sin \zeta' = (b \sin \zeta + M) \cos \zeta'; \quad . \quad . \quad . \quad . \quad . \quad . \quad (5.)$$

and representing $\zeta - \zeta'$, or the deviation, by δ ,

$$\sin \delta = L \sin \zeta' - M \cos \zeta' + (1 - b) \sin \zeta \cos \zeta' \quad . \quad . \quad . \quad . \quad . \quad . \quad (6.)$$

$$= \frac{2}{1+b} L \sin \zeta' - \frac{2}{1+b} M \cos \zeta' + \frac{1-b}{1+b} \sin (\zeta + \zeta') \quad . \quad . \quad . \quad . \quad (7.)$$

$$\tan \zeta' = \frac{b \sin \zeta + M}{\cos \zeta + L} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (8.)$$

$$c \cos \zeta + N = (b \sin \zeta + M) \operatorname{cosec} \zeta' \tan \theta' \quad . \quad . \quad . \quad . \quad . \quad . \quad (9.)$$

$$= (\cos \zeta + L) \sec \zeta' \tan \theta' \quad . \quad . \quad . \quad . \quad . \quad . \quad (10.)$$

$$= \sqrt{(\cos \zeta + L)^2 + (b \sin \zeta + M)^2} \tan \theta' \quad . \quad . \quad . \quad . \quad . \quad . \quad (11.)$$

$$\tan \theta' = \frac{c}{b} \cdot \frac{\cos \zeta + \frac{1}{c} N}{\sin \zeta + \frac{1}{b} M} \sin \zeta' \quad . \quad . \quad . \quad . \quad . \quad . \quad (12.)$$

$$= c \frac{\cos \zeta + \frac{1}{c} N}{\cos \zeta + L} \cos \zeta' \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (13.)$$

$$= \frac{c \cos \zeta + N}{\sqrt{(\cos \zeta + L)^2 + (b \sin \zeta + M)^2}} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (14.)$$

“ Equation (7.) may also be put under the form

$$\sin \delta = \frac{2}{1+b} \sqrt{L^2 + M^2} \sin (\zeta' - \mu) + \frac{1-b}{1+b} \sin (\zeta + \zeta'),$$

where

$$= \frac{2}{1+b} L \sec \mu \sin (\zeta' - \mu) + \frac{1-b}{1+b} \sin (\zeta + \zeta'),$$

in which $\tan \mu = \frac{M}{L}$, and μ represents the displacement of the line of no deviation towards the starboard side.

“ By means of these equations we can determine A' , L , b , M , c , N , from observations made at sea alone. The first four of these quantities furnish the corrections for the horizontal force and the declination. There is greater difficulty in obtaining the correction for the inclination. It will be observed that θ only occurs in these equations involved in the quantities L and N . If there were no permanent magnetism in the vessel, it would be necessary, in order to determine the correcting factors a and d , that observations of the inclination on shore, and corresponding observations on board, should be made in at least one magnetic latitude. If there is any appreciable permanent magnetism, observations of the inclination on shore and on board, and of the horizontal force, should be made in at least two magnetic latitudes. This would be sufficient if a , P , d , R remained absolutely constant. As that appears not to be

the case, as many observations as possible should be made of the inclination on shore and on board, with corresponding observations of the horizontal force. Such observations should be made with great care when the vessel is on or near the magnetic equator and before and after any rapid change of magnetic latitude, and whenever the vessel returns to a place where the observations have been made before on board the same vessel, under the same circumstances as to the distribution of her iron.

“When the permanent magnetism is symmetrically distributed, $Q=0$ and $M=0$, and the other constants may be easily, and probably with great accuracy, determined from the following equations. The small letter suffixed to the symbol of a function indicating the affected value observed with the vessel's head on the N., W., S., E. (affected) points,

$$A' = \frac{H_n + H_s}{2H} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (15.)$$

$$a \tan \theta + \frac{P}{A'H} = L = \frac{H_n - H_s}{H_n + H_s} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (16.)$$

$$b = \frac{H_w + H_e}{2\sqrt{H_n H_s}} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (17.)$$

$$d \tan \theta + \frac{R}{A'H} = N = \frac{H_n \tan \theta_n + H_s \tan \theta_s}{H_n + H_s} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (18.)$$

$$c = \frac{H_n \tan \theta_n - H_s \tan \theta_s}{H_n + H_s} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (19.)$$

“The values of H_n, H_s, H_e, H_w , are given by the square of the number of vibrations of a horizontal needle made in a given time, and beginning to vibrate in a given arc, and require no correction except for temperature.

“If n, s , represent the number of vibrations made by such a needle in the same time, with the ship's head successively on the north and south points, and if Δ represent the value of δ when $\zeta' = \pm 90$, the values of L and Δ are given by the following simple expressions:—

$$\text{“ If } \tan \lambda = \frac{n}{s},$$

$$L = \cos 2\lambda \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (20.)$$

$$\Delta = 90^\circ - 2\lambda \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (21.)$$

The equations (18.) and (19.) may be put under the form

$$d \tan \theta + \frac{R}{A'H} = N = \frac{\phi_n \sin \theta_n + \phi_s \sin \theta_s}{\phi_n \cos \theta_n + \phi_s \cos \theta_s} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (22.)$$

$$c = \frac{\phi_n \sin \theta_n - \phi_s \sin \theta_s}{\phi_n \cos \theta_n + \phi_s \cos \theta_s} \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad . \quad (23.)$$

and the values of N and c obtained, but probably with less accuracy, from observations of the total intensity and inclinations made with a Fox's instrument.

“*Note.*—The last equation in the former memorandum is erroneous. The value of ψ cannot be obtained from two observations of the true azimuth of the ship's head, when $\zeta'_1 + \zeta'_2 = 180$, independently of a .”

General Table of the Declinations observed on board Her Majesty's Ships Erebus and Terror, between May 1841 and August 1842.

Lat.	Long.	Ship.	No. of observations.	Declination.	Lat.	Long.	Ship.	No. of observations.	Declination.
° ' "	° ' "			° ' "	° ' "				° ' "
-42 52	147 24	{ On shore at Hobarton. }	-10 24	-56 19	211 53	Erebus.	18	-14 47
-43 30	147 20	Terror.	4	-12 35	-56 54	212 23	Erebus.	8	-13 32
-42 40	148 45	Erebus.	2	-10 06	-57 03	212 15	Terror.	10	-15 14
-42 17	149 30	Terror.	5	-11 49	-57 16	212 45	Erebus.	13	-13 54
-40 40	149 23	Erebus.	2	-9 51	-58 21	213 00	Terror.	9	-17 34
-40 51	149 21	Terror.	5	-11 11	-58 20	213 13	Erebus.	12	-14 37
-37 48	150 21	Erebus.	10	-11 01	-62 49	212 13	Erebus.	12	-20 14
-37 54	150 20	Terror.	8	-10 38	-62 46	212 13	Terror.	15	-20 03
-37 14	151 34	Erebus.	13	-9 31	-63 19	210 22	Erebus.	6	-20 39
-37 10	151 32	Terror.	10	-11 32	-63 23	210 05	On ice.	5	-19 59
-33 51	151 17	{ On shore at Sydney. }	-9 51	-63 23	209 43	Erebus.	14	-20 44
-33 56	151 00	Terror.	4	-11 18	-63 21	209 48	Terror.	17	-20 56
-33 54	153 50	Erebus.	2	-10 07	-64 29	206 55	Erebus.	11	-22 00
-33 35	162 47	Terror.	10	-14 26	-64 48	206 10	Terror.	9	-22 55
-33 33	162 01	Erebus.	8	-12 02	-64 54	206 05	Erebus.	8	-22 51
-33 41	166 26	Erebus.	8	-13 34	-65 14	205 56	Erebus.	8	-21 51
-33 48	166 29	Terror.	16	-13 40	-65 30	205 57	Erebus.	8	-22 46
-33 32	167 35	Erebus.	7	-13 27	-66 04	203 51	Erebus.	4	-24 13
-33 37	168 04	Terror.	12	-15 02	-65 32	204 57	Terror.	7	-24 27
-33 42	169 44	Erebus.	11	-12 54	-66 22	203 40	Erebus.	11	-25 36
-34 15	172 33	Terror.	9	-13 45	-66 04	203 16	Erebus.	8	-26 59
-34 31	173 28	Erebus.	11	-13 56	-66 10	203 37	Terror.	7	-27 24
-34 32	173 47	Terror.	5	-13 42	-66 16	204 39	Erebus.	6	-26 36
-35 16	174 00	{ On shore, Bay of Islands. }	-13 36	-66 15	204 23	Erebus.	10	-25 55
-36 39	177 58	Erebus.	11	-14 24	-66 04	204 14	Erebus.	16	-25 48
-38 03	179 32	Terror.	10	-14 55	-66 02	204 00	Terror.	18	-26 48
-38 02	179 51	Erebus.	13	-14 44	-66 00	204 11	Erebus.	11	-25 26
-39 29	182 42	Terror.	11	-16 55	-65 58	203 54	Terror.	11	-25 00
-39 10	182 43	Erebus.	13	-14 43	-65 57	204 14	Erebus.	13	-25 24
-40 51	183 16	Erebus.	11	-12 57	-65 58	203 54	Terror.	11	-25 59
-41 59	183 28	Terror.	19	-15 13	-65 55	203 28	Erebus.	17	-24 58
-42 02	183 31	Erebus.	11	-14 24	-65 47	202 13	On ice.	6	-25 15
-46 09	183 59	Erebus.	13	-16 35	-65 59	203 07	Terror.	15	-26 24
-47 05	184 30	Terror.	11	-15 17	-67 38	204 20	Erebus.	9	-27 46
-47 32	184 52	Erebus.	11	-15 45	-67 40	204 10	Terror.	9	-28 19
-48 53	186 48	Erebus.	15	-16 23	-67 20	202 02	Erebus.	8	-27 36
-49 21	188 32	Terror.	7	-16 52	-67 19	202 35	Terror.	11	-28 37
-49 28	189 00	Erebus.	8	-17 51	-67 19	201 56	Erebus.	8	-28 12
-49 57	191 10	Terror.	7	-16 36	-67 20	201 40	Terror.	11	-28 33
-50 03	191 27	Erebus.	12	-18 23	-68 32	200 07	Erebus.	14	-30 25
-50 54	192 33	Erebus.	6	-18 18	-68 24	199 57	Terror.	13	-32 43
-50 53	192 30	Terror.	8	-16 37	-68 47	199 45	Erebus.	13	-32 33
-51 39	194 53	Erebus.	18	-15 16	-68 52	199 40	Terror.	7	-30 47
-51 50	195 06	Terror.	8	-15 14	-70 10	186 15	Erebus.	9	-35 42
-52 43	202 14	Erebus.	10	-13 58	-70 25	185 38	Terror.	11	-38 55
-53 05	204 33	Terror.	11	-14 54	-70 33	185 22	Erebus.	11	-38 21
-53 10	205 28	Erebus.	12	-13 06	-70 32	185 13	Terror.	12	-38 17
-54 54	209 24	Erebus.	8	-14 26	-70 23	184 31	Erebus.	10	-37 35
-56 20	211 40	Terror.	14	-15 14	-70 14	184 00	Terror.	17	-37 19
					-70 14	183 52	Erebus.	11	-36 28
					-71 04	180 46	Terror.	5	-40 45
					-72 10	180 58	Erebus.	1	-45 37
					-73 14	181 08	Terror.	2	-51 48
					-75 06	173 14	Erebus.	3	-77 17

Observations of Declination. (Continued.)

Lat.	Long.	Ship.	No. of observations.	Declination.	Lat.	Long.	Ship.	No. of observations.	Declination.
—75 40	174 56	Terror.	5	—76 03	—58 50	222 00	Terror.	4	—16 03
—76 48	182 33	Erebus.	6	—86 23	—58 58	227 00	Terror.	1	—17 01
—76 54	182 17	Terror.	3	—82 28	—59 04	229 00	Erebus.	4	—17 49
—76 12	191 40	Terror.	2	—70 22	—60 18	236 30	Terror.	3	—20 57
—76 42	194 37	Erebus.	10	—79 57	—60 14	236 32	Erebus.	3	—20 56
—76 46	194 40	Terror.	8	—81 23	—60 02	240 31	Terror.	1	—20 48
—78 03	197 31	Erebus.	10	—87 31	—59 17	245 40	Erebus.	1	—20 14
—77 57	197 54	Terror.	8	—88 01	—58 28	251 40	Terror.	4	—22 46
—77 44	198 07	Erebus.	10	—88 08	—58 40	251 52	Erebus.	3	—21 47
—75 17	195 06	Terror.	5	—64 33	—58 40	254 59	Erebus.	4	—23 28
—74 49	193 56	Erebus.	6	—62 17	—58 36	255 20	Terror.	7	—24 46
—71 56	186 36	Erebus.	2	—45 11	—58 46	257 50	Terror.	3	—26 13
—71 08	184 54	Erebus.	5	—39 20	—58 46	258 07	Erebus.	3	—25 25
—70 58	184 03	Terror.	3	—38 26	—59 00	267 56	Terror.	8	—26 25
—70 10	180 20	Terror.	3	—31 26	—59 01	268 34	Erebus.	9	—26 17
—69 50	180 16	Erebus.	12	—30 50	—59 02	272 04	Erebus.	1	—26 51
—68 17	183 27	Erebus.	12	—27 32	—59 04	272 20	Terror.	4	—27 08
—68 02	183 35	Terror.	4	—28 50	—58 51	276 04	Erebus.	5	—26 18
—67 30	185 00	Terror.	7	—29 46	—58 55	276 26	Terror.	7	—28 25
—67 25	186 42	Erebus.	4	—27 32	—58 21	279 48	Terror.	10	—27 13
—65 51	190 25	Terror.	6	—25 02	—58 20	280 27	Erebus.	5	—25 04
—65 07	192 24	Erebus.	7	—23 40	—58 30	282 00	Terror.	10	—26 49
—63 33	194 53	Erebus.	1	—21 57	—58 30	282 05	Erebus.	8	—26 14
—62 26	195 40	Terror.	4	—19 41	—58 32	283 40	Erebus.	7	—26 18
—62 20	196 15	Erebus.	5	—19 51	—58 29	283 33	Terror.	8	—26 13
—61 00	199 00	Terror.	4	—19 49	—57 35	288 54	Terror.	1	—25 16
—61 02	199 25	Erebus.	8	—18 42	—56 46	294 30	Terror.	2	—20 26
—60 20	205 12	Terror.	4	—18 20	—52 14	301 09	Terror.	4	—18 25
—60 26	203 26	Erebus.	4	—17 31	—52 16	301 06	Erebus.	6	—16 29
—60 16	212 59	Erebus.	4	—17 01	—17 01				
—60 05	213 51	Terror.	6	—17 19	—51 32	301 53	{ On shore at Port Louis* }	—17 36
—58 59	220 30	Erebus.	6	—15 30					

* The mean monthly results with the magnetometers of the Expedition at the observatory at Port Louis at the Falkland Islands were as follows:—

April . . . 1 to 23.	—17 50·3	} Mean corresponding to August 15, 1842. —17 36·2.
May . . . 1 to 31.	—17 43·7	
June . . . 1 to 30.	—17 38·1	
July . . . 1 to 31.	—17 35·6	
August . . 1 to 31.	—17 33·0	
September 1 to 30.	—17 32·3	
October . . 1 to 31.	—17 30·2	
November 1 to 26.	—17 26·7	

The easterly declination appears to be decreasing very rapidly at the Falkland Islands.

General Table of the Inclinations observed on board Her Majesty's Ships Erebus
and Terror, between May 1841 and August 1842.

Lat.	Long.	Ship.	No. of ob- servations.	Inclination.	Lat.	Long.	Ship.	No. of ob- servations.	Inclination.
-43 00	148 28	Erebus.	5	-70 25	-40 47	183 03	Erebus.	5	-62 21
-42 43	148 55	Terror.	8	-70 44	-40 42	183 05	Terror.	15	-61 56
-42 13	149 25	Erebus.	5	-69 37	-41 34	183 40	Terror.	7	-62 57
-40 51	149 28	Terror.	4	-69 05	-41 49	183 41	Erebus.	5	-63 28
-40 55	149 12	Erebus.	4	-68 41	-42 40	183 46	Terror.	7	-63 46
-38 17	150 22	Terror.	4	-66 57	-43 32	183 03	Erebus.	5	-64 44
-37 50	150 22	Erebus.	4	-66 36	-43 56	183 04	Terror.	15	-65 22
-37 28	151 30	Terror.	4	-66 22	-45 40	183 20	Erebus.	5	-66 35
-37 21	151 33	Erebus.	5	-66 01	-45 39	183 18	Terror.	14	-66 43
-36 21	151 39	Terror.	3	-66 11	-47 19	184 40	Erebus.	5	-67 56
-36 01	151 48	Erebus.	4	-65 04	-47 26	184 42	Terror.	14	-67 32
-34 06	151 19	Terror.	4	-62 58	-48 42	186 25	Terror.	15	-68 40
-33 51	151 20	Erebus.	19	-62 47	-48 43	186 30	Erebus.	6	-69 05
-33 51	151 17	Terror.	7	-62 59*	-49 24	187 23	Terror.	15	-68 59
-33 51	151 17	Erebus.	8	-62 48*	-49 23	188 29	Erebus.	9	-69 41
-33 51	151 17	Terror.	11	-62 52	-49 30	189 19	Terror.	14	-68 55
-33 51	151 17	Erebus.	7	-62 42	-50 03	191 20	Terror.	14	-68 43
-33 58	153 35	Terror.	8	-62 30	-50 24	191 40	Erebus.	10	-69 43
-33 52	154 07	Erebus.	5	-62 47	-50 38	192 05	Terror.	14	-69 25
-33 56	156 38	Terror.	4	-61 46	-51 48	194 25	Terror.	15	-69 51
-33 51	157 18	Erebus.	5	-62 07	-51 48	196 20	Erebus.	10	-70 21
-33 31	160 20	Terror.	4	-61 04	-52 28	199 05	Terror.	11	-70 10
-33 27	160 43	Erebus.	5	-61 30	-52 51	203 56	Terror.	8	-70 01
-33 42	164 05	Terror.	4	-60 52	-52 54	203 00	Erebus.	11	-70 44
-33 38	163 42	Erebus.	5	-60 48	-53 01	205 08	Erebus.	6	-70 10
-33 38	166 28	Erebus.	5	-60 07	-53 12	205 40	Terror.	15	-69 52
-33 44	166 37	Terror.	10	-59 55	-54 31	208 46	Terror.	11	-70 10
-33 33	167 38	Terror.	9	-59 58	-54 53	209 24	Terror.	12	-70 21
-33 22	167 40	Erebus.	5	-59 39	-55 01	209 47	Erebus.	10	-70 58
-33 00	169 00	Terror.	9	-58 43	-55 50	211 10	Erebus.	10	-71 28
-32 58	169 20	Erebus.	5	-59 04	-56 14	211 43	Terror.	14	-71 41
-32 12	170 27	Erebus.	4	-58 33	-56 39	212 10	Erebus.	10	-72 18
-32 11	171 01	Terror.	11	-57 28	-56 06	212 20	Erebus.	6	-72 08
-33 57	171 58	Erebus.	8	-58 24	-56 40	211 57	Terror.	12	-72 00
-33 55	171 59	Terror.	5	-58 24	-57 06	212 12	Terror.	12	-72 14
-34 29	173 36	Erebus.	6	-58 26	-57 57	213 02	Terror.	10	-73 09
-33 58	172 06	Terror.	7	-58 14	-58 38	213 10	Terror.	11	-73 45
-34 15	172 50	Terror.	10	-58 48	-58 39	213 17	Erebus.	11	-73 45
-34 24	173 43	Terror.	7	-59 00	-61 12	213 52	Terror.	14	-75 32
-35 16	174 00	Terror.	3	-59 36	-61 18	213 57	Erebus.	11	-75 32
-35 16	174 00	Erebus.	10	-59 31†	-62 36	212 36	Terror.	8	-76 37
-35 16	174 00	Terror.	14	-59 25†	-62 40	212 53	Erebus.	7	-76 36
-35 16	174 23	Erebus.	10	-59 28	-63 11	210 18	Terror.	12	-77 37
-36 05	176 17	Terror.	12	-59 20	-63 23	210 02	Erebus.	5	-77 26
-36 27	177 34	Erebus.	5	-59 54	-63 23	210 02	Erebus.	4	-77 25§
-38 17	179 51	Erebus.	6	-60 34	-63 23	210 02	Erebus.	3	-77 30
-38 16	179 58	Terror.	15	-60 37	-63 36	208 20	Terror.	10	-77 53
-38 54	182 17	Terror.	17	-61 21	-63 49	208 29	Terror.	10	-77 56
-39 08	182 30	Erebus.	11	-61 34	-63 47	208 26	Erebus.	5	-77 57
-39 21	182 57	Terror.	16	-61 15	-64 25	206 29	Terror.	14	-78 30

* On shore at Garden Island, Sydney; inclination by needles whose poles were reversed, $-62^{\circ} 49' 1$.

† Correct; in page 174 it is printed by mistake $-59^{\circ} 29'$.

‡ On shore at the Bay of Islands, New Zealand; inclination by needles whose poles are reversed, $-59^{\circ} 31' 9$.

§ On ice; the inclination observed with needles whose poles were reversed, was $-77^{\circ} 23' 3$.

General Table of Inclination. (Continued.)

Lat.	Long.	Ship.	No. of observations.	Inclination.	Lat.	Long.	Ship.	No. of observations.	Inclination.
-64 42	206 47	Erebus.	8	-78 20	-69 53	182 51	Terror.	7	-84 09
-65 13	206 03	Erebus.	11	-78 57	-70 37	181 09	Erebus.	9	-84 06
-65 26	205 04	Terror.	15	-79 16	-71 03	180 57	Terror.	8	-84 20
-65 47	204 19	Terror.	13	-79 26	-72 46	181 46	Erebus.	6	-85 04
-65 47	204 19	Terror.	13	-79 28	-72 07	181 50	Terror.	9	-84 59
-65 50	204 08	Terror.	11	-79 30	-73 08	181 03	Terror.	9	-85 22
-65 58	204 03	Erebus.	22	-79 31*	-73 53	180 06	Erebus.	2	-86 02
-65 59	204 03	Terror.	8	-79 39	-74 56	173 36	Erebus.	6	-86 52
-66 08	203 50	Terror.	10	-79 39	-74 59	173 40	Terror.	13	-87 05
-66 06	203 41	Erebus.	12	-79 53	-75 10	173 08	Erebus.	5	-86 59
-66 19	203 09	Terror.	14	-80 01	-75 59	175 13	Erebus.	6	-86 44
-66 26	203 25	Erebus.	13	-79 57	-76 05	174 58	Terror.	8	-87 03
-66 21	203 34	Terror.	6	-80 03	-76 58	181 03	Erebus.	5	-86 46
-66 20	203 59	Terror.	9	-79 52	-77 03	181 35	Terror.	8	-86 56
-66 34	203 34	Erebus.	42	-79 55	-76 43	184 30	Erebus.	6	-86 07
-66 05	204 02	Terror.	12	-79 51	-76 48	184 58	Terror.	8	-86 30
-66 01	204 04	Terror.	12	-79 50	-76 15	191 10	Terror.	9	-85 59
-66 11	204 21	Erebus.	14	-79 44	-76 03	193 43	Erebus.	2	-85 18
-66 13	204 33	Erebus.	11	-79 34	-76 42	194 42	Erebus.	6	-85 25
-65 59	204 01	Erebus.	14	-79 38	-76 48	194 21	Terror.	15	-85 12
-65 57	203 56	Terror.	14	-79 47	-77 05	194 38	Erebus.	5	-85 24
-65 53	203 29	Terror.	10	-79 51	-77 47	197 25	Terror.	9	-84 49
-66 11	202 12	Terror.	13	-79 48	-77 45	197 48	Erebus.	5	-84 49
-66 12	203 04	Erebus.	8	-79 35	-77 12	199 24	Terror.	8	-85 35
-66 08	201 46	Terror.	11	-79 35	-74 50	193 45	Erebus.	6	-84 49
-65 49	202 02	Erebus.	4	-79 47†	-75 20	194 36	Terror.	9	-85 46
-65 50	202 14	Terror.	13	-79 38	-72 46	189 59	Erebus.	5	-84 38
-66 09	202 56	Erebus.	9	-79 33	-73 10	189 41	Terror.	7	-85 08
-67 02	201 00	Terror.	12	-80 22	-72 01	187 35	Erebus.	5	-84 10
-66 39	202 14	Erebus.	6	-80 01	-71 01	187 37	Terror.	9	-84 56
-67 12	202 12	Terror.	10	-80 06	-71 08	184 59	Erebus.	6	-84 04
-67 36	204 00	Erebus.	9	-80 22	-71 12	184 20	Terror.	10	-84 37
-67 46	204 17	Terror.	15	-80 43	-69 54	179 55	Terror.	8	-84 30
-67 47	204 17	Terror.	15	-80 48	-69 52	180 04	Erebus.	5	-83 34
-67 16	203 20	Terror.	16	-80 44	-69 44	179 53	Erebus.	5	-83 31
-67 19	202 52	Erebus.	11	-80 26	-68 09	183 10	Terror.	7	-82 26
-67 14	201 34	Terror.	18	-80 35	-68 04	183 25	Erebus.	10	-82 13
-67 57	200 00	Erebus.	7	-80 46	-67 37	186 06	Terror.	15	-81 33
-68 38	199 57	Terror.	14	-81 18	-67 31	185 13	Erebus.	6	-81 51
-68 33	199 52	Erebus.	11	-81 14	-67 09	188 02	Terror.	7	-81 03
-68 46	199 38	Terror.	11	-81 33	-67 19	188 10	Erebus.	5	-81 02
-68 59	195 54	Erebus.	6	-81 54	-65 18	191 39	Terror.	10	-79 42
-68 52	198 24	Terror.	7	-82 30	-65 21	191 43	Erebus.	5	-79 19
-69 48	192 25	Erebus.	5	-82 35	-63 30	194 15	Terror.	7	-78 30
-69 55	192 17	Terror.	10	-83 00	-63 30	194 22	Erebus.	6	-78 11
-70 05	191 03	Terror.	9	-83 20	-62 17	195 55	Terror.	7	-77 30
-70 07	191 11	Erebus.	6	-82 51	-62 16	196 10	Erebus.	5	-77 17
-70 26	189 00	Erebus.	5	-83 07	-61 06	198 08	Terror.	9	-76 32
-70 18	186 01	Erebus.	5	-83 18	-61 11	198 45	Erebus.	5	-76 34
-70 12	186 23	Terror.	17	-83 23	-60 50	200 11	Erebus.	5	-75 33
-70 39	185 31	Erebus.	6	-83 35	-60 57	199 03	Terror.	7	-75 08
-70 32	185 38	Terror.	10	-83 30	-60 18	204 46	Erebus.	7	-75 08
-70 11	183 50	Erebus.	5	-83 33	-60 15	208 06	Terror.	7	-74 21
-69 56	184 43	Terror.	8	-84 03	-60 13	211 44	Erebus.	6	-74 21

* The inclination observed in Lat. -65° 59', Long. 204° 14', with needles whose poles were reversed, was -79° 31' 0.

† Observed on ice; inclination with needles whose poles were reversed, -79° 39' 5.

General Table of Inclination. (Continued.)

Lat.	Long.	Ship.	No. of observations.	Inclination.	Lat.	Long.	Ship.	No. of observations.	Inclination.
—60 16	211 52	Terror.	8	—74 14	—59 00	267 18	Erebus.	6	—67 39
—59 58	216 28	Terror.	7	—73 36	—59 02	271 58	Erebus.	5	—67 01
—59 24	218 55	Erebus.	11	—73 30	—59 01	272 06	Terror.	8	—66 53
—59 07	219 12	Terror.	17	—73 48	—58 54	276 18	Terror.	7	—66 10
—58 53	222 27	Erebus.	7	—73 38	—58 51	277 05	Erebus.	6	—65 27
—59 04	228 09	Terror.	9	—73 25	—58 25	279 44	Terror.	8	—64 44
—59 03	228 33	Erebus.	7	—72 57	—58 23	280 03	Erebus.	5	—64 49
—59 39	232 48	Erebus.	5	—72 54	—58 31	281 38	Terror.	9	—63 48
—59 45	233 55	Erebus.	4	—72 51	—58 29	282 10	Erebus.	5	—63 41
—60 09	236 11	Terror.	11	—73 01	—58 36	285 33	Terror.	7	—63 00
—60 16	236 11	Erebus.	5	—73 00	—58 31	285 56	Erebus.	5	—63 05
—60 21	237 02	Erebus.	5	—72 45	—57 21	289 36	Terror.	7	—61 36
—60 22	237 14	Terror.	10	—73 08	—57 22	289 50	Erebus.	5	—61 15
—60 20	237 54	Erebus.	9	—72 44	—57 26	291 36	Terror.	8	—59 52
—60 01	241 31	Erebus.	5	—72 40	—57 11	292 14	Erebus.	6	—58 51
—59 17	245 40	Erebus.	5	—71 29	—56 37	294 34	Terror.	7	—59 02
—59 11	246 37	Terror.	10	—71 24	—56 40	294 46	Erebus.	5	—59 01
—59 15	248 12	Erebus.	5	—71 26	—54 48	297 21	Terror.	7	—56 48
—58 59	249 18	Erebus.	6	—71 04	—54 50	298 08	Erebus.	4	—56 10
—58 26	251 42	Terror.	7	—70 55	—52 54	300 27	Erebus.	5	—53 52
—58 29	252 18	Erebus.	5	—70 50	—52 34	300 10	Terror.	15	—53 25
—58 33	254 45	Terror.	7	—70 16	—52 03	301 56	Erebus.	3	—52 34
—58 35	255 10	Erebus.	5	—70 11	—51 42	301 36	Terror.	7	—52 04
—58 42	257 44	Terror.	10	—69 50	—51 32	301 53	Erebus.	8	—52 36*
—58 45	257 58	Erebus.	5	—69 47	—51 32	301 53	Terror.	25	—52 15*
—58 58	267 18	Terror.	8	—68 00					

* Observed on shore at the Falkland Islands; the Inclination with needles whose poles were reversed, was 52° 26'2.

General Table of the Intensity of the Magnetic Force, from the observations made on board Her Majesty's Ships Erebus and Terror, between April 1841 and August 1842.

Lat.	Long.	Ship.	No. of observations.	Intensity.	Lat.	Long.	Ship.	No. of observations.	Intensity.
				London = 1.372.					London = 1.372.
—43 00	148 28	Erebus.	2	1.853	—43 54	183 06	Terror.	8	1.707
—43 03	148 20	Terror.	2	1.849	—45 39	183 18	Terror.	8	1.733
—42 13	149 29	Erebus.	2	1.823	—46 29	184 00	Erebus.	4	1.744
—42 24	149 30	Terror.	2	1.822	—47 26	184 37	Terror.	8	1.753
—40 54	149 13	Erebus.	2	1.818	—48 18	185 54	Terror.	10	1.772
—40 51	149 28	Terror.	2	1.814	—49 04	187 11	Erebus.	7	1.767
—38 17	150 22	Terror.	2	1.795	—49 05	186 54	Terror.	10	1.772
—37 31	151 09	Erebus.	3	1.769	—49 27	189 13	Erebus.	5	1.773
—37 28	151 30	Terror.	2	1.758	—49 24	187 23	Terror.	11	1.772
—34 35	151 30	Erebus.	3	1.734	—49 27	189 51	Terror.	14	1.775
—34 51	151 25	Terror.	3	1.738	—49 50	190 46	Terror.	10	1.766
—33 51	151 17	Erebus.	14	1.698*	—50 14	191 06	Erebus.	7	1.780
—33 51	151 17	Terror.	16	1.699*	—50 08	191 39	Terror.	6	1.771
—33 51	151 17	Erebus.	6	1.719	—50 42	192 11	Terror.	14	1.777
—33 51	151 17	Terror.	4	1.719	—51 34	194 29	Erebus.	5	1.806
—32 52	154 07	Erebus.	2	1.708	—51 37	194 00	Terror.	10	1.794
—33 57	153 35	Terror.	4	1.703	—52 13	197 03	Terror.	9	1.799
—33 51	157 18	Erebus.	2	1.680	—52 43	201 40	Erebus.	7	1.822
—33 56	156 38	Terror.	2	1.679	—52 52	204 31	Terror.	20	1.820
—33 27	160 43	Erebus.	2	1.668	—53 01	205 08	Erebus.	5	1.825
—33 31	160 20	Terror.	2	1.671	—53 31	206 14	Terror.	10	1.834
—33 38	163 42	Erebus.	2	1.655	—54 54	209 16	Terror.	13	1.814
—33 42	163 50	Terror.	4	1.658	—55 08	210 00	Erebus.	6	1.846
—33 41	166 23	Erebus.	2	1.638	—56 14	211 43	Terror.	8	1.836
—33 44	166 37	Terror.	5	1.627	—56 38	211 30	Erebus.	8	1.851
—33 22	167 40	Erebus.	2	1.630	—56 30	211 50	Terror.	10	1.841
—33 34	167 37	Terror.	5	1.600	—57 04	212 06	Terror.	8	1.843
—32 58	169 20	Erebus.	2	1.620	—58 08	212 40	Erebus.	4	1.866
—32 58	169 20	Terror.	4	1.604	—57 44	212 59	Terror.	8	1.863
—32 11	171 02	Terror.	6	1.589	—58 32	213 09	Terror.	14	1.878
—33 32	171 59	Erebus.	6	1.596	—58 45	213 19	Erebus.	7	1.888
—33 57	172 04	Terror.	6	1.601	—61 02	213 52	Terror.	14	1.892
—34 15	172 50	Terror.	5	1.597	—61 20	213 57	Erebus.	4	1.923
—34 24	173 43	Terror.	4	1.619	—62 34	212 34	Terror.	10	1.916
—35 16	174 00	Erebus.	26	1.607†	—62 40	212 53	Erebus.	2	1.937
—35 16	174 00	Terror.	24	1.608†	—63 21	209 37	Terror.	8	1.910
—35 16	174 00	Terror.	2	1.610	—63 23	210 02	Erebus.	2	1.952
—36 20	177 27	Terror.	4	1.616	—63 23	210 02	Erebus.	2	1.938†
—35 15	173 39	Erebus.	2	1.624	—64 02	207 33	Terror.	8	1.927
—36 27	177 34	Erebus.	2	1.625	—63 47	208 26	Erebus.	6	1.945
—38 13	179 46	Terror.	8	1.634	—64 49	206 36	Erebus.	8	1.948
—38 17	179 31	Erebus.	2	1.627	—64 51	206 19	Terror.	8	1.943
—38 54	182 05	Terror.	10	1.640	—65 26	205 04	Terror.	8	1.931
—39 10	182 58	Erebus.	4	1.628	—66 00	204 09	Erebus.	15	1.971
—40 02	183 02	Terror.	16	1.652	—65 50	204 12	Terror.	8	1.950
—40 47	183 03	Erebus.	2	1.672	—66 33	203 28	Erebus.	4	1.981
—41 34	183 40	Terror.	10	1.666	—66 09	203 51	Terror.	5	1.949
—41 49	183 41	Erebus.	2	1.684	—66 09	204 26	Erebus.	11	1.970
—42 40	183 46	Terror.	4	1.682	—66 07	204 00	Terror.	18	1.944
—43 32	183 03	Erebus.	2	1.714	—66 10	203 58	Erebus.	12	1.973
					—65 57	203 56	Terror.	14	1.949

* On shore at Garden Island, Sydney.

† On shore at the Bay of Islands, New Zealand.

‡ Observed on ice.

General Table of the Intensity of the Magnetic Force. (Continued.)

Lat.	Long.	Ship.	No. of observations.	Intensity.	Lat.	Long.	Ship.	No. of observations.	Intensity.
				London = 1.372.					London = 1.372.
-66 03	202 29	Terror.	12	1.945	-67 35	185 18	Terror.	10	1.978
-65 49	202 02	Erebus.	6	1.959 *	-67 24	187 51	Terror.	8	1.981
-65 47	202 08	Terror.	10	1.948 *	-66 56	189 36	Erebus.	4	1.980
-67 16	203 40	Erebus.	8	1.976	-65 17	191 58	Terror.	10	1.955
-67 46	204 17	Terror.	10	1.960	-63 30	194 15	Terror.	4	1.942
-67 37	204 12	Terror.	10	1.965	-63 05	195 18	Erebus.	6	1.941
-67 21	202 15	Erebus.	6	1.967	-61 57	196 33	Terror.	14	1.916
-67 12	202 24	Terror.	6	1.946	-61 07	199 05	Erebus.	7	1.924
-67 15	201 34	Terror.	8	1.935	-60 19	203 42	Terror.	4	1.920
-68 08	199 57	Terror.	8	1.955	-60 16	207 52	Erebus.	4	1.881
-68 29	199 55	Erebus.	9	1.991	-60 15	209 55	Terror.	8	1.907
-68 46	199 39	Terror.	13	1.961	-59 13	216 28	Terror.	4	1.910
-68 52	198 24	Terror.	10	1.966	-59 22	218 14	Terror.	4	1.900
-69 29	192 24	Erebus.	8	2.001	-58 33	220 27	Erebus.	7	1.878
-70 00	191 36	Terror.	9	1.965	-58 49	221 25	Terror.	4	1.913
-70 14	196 16	Terror.	15	1.976	-59 01	227 43	Terror.	4	1.897
-70 18	185 16	Terror.	10	1.983	-59 29	231 53	Erebus.	6	1.890
-70 23	185 33	Erebus.	8	1.996	-60 18	236 31	Erebus.	6	1.909
-70 27	181 59	Terror.	8	1.988	-60 05	235 56	Terror.	4	1.884
-70 28	181 20	Erebus.	5	1.999	-60 17	236 38	Terror.	4	1.892
-72 41	181 41	Terror.	8	2.001	-60 20	237 55	Erebus.	4	1.907
-72 46	181 46	Erebus.	4	1.989	-60 24	237 29	Terror.	4	1.907
-74 58	173 34	Terror.	10	2.008	-59 05	247 27	Terror.	4	1.875
-75 05	173 17	Erebus.	9	2.024	-59 31	245 13	Erebus.	8	1.861
-75 42	174 14	Terror.	7	2.006	-58 26	251 42	Terror.	4	1.885
-76 33	180 09	Erebus.	6	2.021	-58 33	254 45	Terror.	10	1.824
-77 02	181 37	Terror.	4	2.007	-58 36	255 30	Erebus.	7	1.821
-76 48	184 46	Terror.	4	2.009	-58 47	258 13	Terror.	8	1.832
-76 20	191 26	Terror.	4	2.024	-58 59	267 50	Terror.	4	1.783
-76 24	184 54	Terror.	4	2.004	-59 01	272 06	Terror.	4	1.747
-77 00	194 38	Erebus.	8	2.009	-58 58	272 35	Erebus.	6	1.747
-77 13	193 52	Terror.	10	2.011	-58 24	276 18	Terror.	4	1.722
-77 47	197 25	Terror.	4	2.001	-58 27	280 20	Terror.	12	1.672
-77 14	199 29	Terror.	10	1.992	-58 27	282 04	Erebus.	5	1.652
-75 20	194 36	Terror.	4	2.003	-58 36	285 33	Terror.	4	1.648
-74 50	193 45	Erebus.	2	1.999	-57 23	290 34	Terror.	8	1.592
-73 10	189 21	Terror.	4	2.000	-57 16	292 01	Erebus.	5	1.544
-72 24	188 47	Erebus.	4	1.990	-55 42	295 57	Terror.	8	1.495
-72 03	187 40	Terror.	10	1.999	-56 03	295 54	Erebus.	3	1.478
-71 34	186 09	Terror.	10	1.999	-52 40	299 52	Terror.	9	1.355
-71 08	184 59	Erebus.	4	2.009	-52 54	300 57	Erebus.	5	1.367
-69 54	179 55	Terror.	4	1.999	-52 05	301 39	Terror.	8	1.340
-69 48	179 56	Erebus.	4	1.994	-51 32	301 53	Erebus.	24	1.333†
-68 09	183 10	Terror.	4	1.981	-51 32	301 53	Terror.	30	1.336†
-68 04	183 25	Erebus.	4	1.981					

* Observed on ice,

† On shore at the Falkland Islands.

**DECLINATIONS observed on board Her Majesty's Ship Erebus, between June 1841
and August 1842.**

The Observers are distinguished in the column of Initials as follows:—R. Captain ROSS; S. Lieut. SIBBALD; W. Lieut. WOOD; T. Mr. TUCKER, Master; SM. Mr. SMITH, and O. Mr. OAKLEY, Mates; Y. Mr. YULE, Second Master. East Declination is characterised by the sign—.

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
May 10 19	-42° 52' 147° 24'	Hobarton, Van Diemen Island.	R.	-10° 24' 5	Mean, 7 days' hourly observations with Declin. No. 1.					-10° 24'	At the Magnetic Observatory.
			R.	-10° 24' 3							
June 29	At anchor.	R.	-10 36	N.	To obtain corrections for the ship's attraction.						
		R.	-11 24	N. by W.							
		R.	-12 11	N.N.W.							
		R.	-12 44	N. W. by N.							
		R.	-13 04	N.W.							
		R.	-13 22	N.W. by W.							
		R.	-14 01	W.N.W.							
		R.	-14 42	W. by N.							
		R.	-15 08	W.							
		R.	-15 06	W. by S.							
		R.	-14 51	W.S.W.							
		R.	-14 29	S.W. by W.							
		R.	-13 51	S.W.							
		R.	-13 08	S.W. by S.							
		R.	-12 25	S.S.W.							
		R.	-10 29	S. by W.							
		R.	- 9 26	S.							
		R.	- 7 38	S. by E.							
		R.	- 7 03	S.S.E.							
		R.	- 6 19	S.E. by S.							
		R.	- 5 36	S.E.							
		R.	- 5 09	S.E. by E.							
		R.	- 4 24	E.S.E.							
		R.	- 4 49	E. by S.							
		R.	- 5 02	E.							
		R.	- 5 24	E. by N.							
		R.	- 6 04	E.N.E.							
		R.	- 6 24	N.E. by E.							
		R.	- 7 01	N.E.							
		R.	- 7 30	N.E. by N.							
		R.	- 8 40	N.N.E.							
		R.	- 9 32	N. by E.							
July 7 P.M.	-43 17	148 07	R.	- 5 33	E.S.E.	-70 50	-4 44	-10 17	-0 37	-10 06	At the Magnetic Observatory.
9 P.M.	-42 04	149 24	T.	-12 30	W.N.W.	-69 40	+3 49	- 8 41			
10 A.M.	-40 55	149 12	T.	-10 15	N. by W.	-68 40	+0 39	- 9 36	-0 37	- 9 51	
10 P.M.	-40 26	149 34	T.	- 8 52	N.		0 00	- 8 52			
11 P.M.	-37 49	150 21	R.	-10 47	N.	-66 40	0 00	-10 47	-0 37	-11 01	
			R.	- 9 57	N.		0 00	- 9 57			
			T.	-10 56	N. by W.		+0 35	-10 21			
			T.	-10 55	N. by W.		+0 35	-10 20			
			R.	-10 54	N. by W.		+0 35	-10 19			
			R.	-10 04	N.		0 00	-10 04			
			R.	-11 44	N.N.W.		+1 10	-10 34			
			S.	-11 53	N. by W.		+0 35	-11 18			
			T.	-11 17	N. by W.		+0 35	-10 42			
	-37 43	150 22	R.	-10 18	N. by W.		+0 35	- 9 43			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
July 12 A.M.	-37° 24'	151° 27'	R.	- 6 30 "	N.E.	-66 00	-2 10	- 8 40	-0 37	- 9 31	By the magnetometers on shore.
			R.	- 6 11	N.E.		-2 10	- 8 21			
			R.	- 5 39	N.E.		-2 10	- 7 49			
	-37 22	151 28	W.	- 7 53	N.N.E.		-1 07	- 9 00			
12 P.M.	-37 17	151 39	S.	- 6 06	N.E. $\frac{3}{4}$ E.		-2 34	- 8 40			
			S.	- 6 37	N.E.		-2 10	- 8 47			
	-37 16	151 37	Y.	- 9 36	N. by w.		+0 34	- 9 02			
			R.	- 8 34	N. by w.		+0 34	- 8 00			
			S.	- 9 33	N. by w.		+0 34	- 8 59			
			S.	- 9 45	N. by w.		+0 34	- 9 11			
			R.	- 9 29	N. by w.	+0 34	- 8 55				
			T.	- 9 09	N.	0 00	- 9 09				
13 A.M.	-37 11	151 37	T.	-12 04	N.N.W.	-65 00	+1 03	-11 01			
Aug. 3	Garden Island, Sydney.		R.	- 9 51.5					- 9 51.5	
	-33 51	151 17									
6 A.M.	-33 54	153 50	S.	- 7 05	E.	-62 40	-3 13	-10 18	-0 37	-10 07	
			T.	- 5 42	E. by N.		-3 00	- 8 42			
8 P.M.	-33 30	160 56	S.	- 7 47	E. by N.	-61 30	-2 50	-10 37	-0 37	-12 02	
			S.	- 7 58	E.		-3 03	-11 01			
			O.	- 7 54	E. by N.		-2 50	-10 44			
			R.	- 8 21	E.		-3 03	-11 24			
			R.	- 6 30	E.	-60 40	-3 03	- 9 33	-0 37	-13 34	
9 A.M.	-33 38	163 50	T.	-10 37	E.		-2 56	-13 13			
			R.	- 9 45	E.		-2 56	-12 41			
			T.	- 9 23	E.		-2 56	-12 19			
10 A.M.	-33 42	166 25	R.	-12 53	N.N.E.	-60 10	-0 48	-13 41	-0 37	-13 27	
			T.	-10 59	S.E. by E.		-2 50	-13 49			
			S.	- 9 55	E.		-2 52	-12 47			
			T.	- 9 28	E. by S.		-2 59	-12 27			
	-33 41	166 19	W.	-11 20	E.S.E.	-59 40	-2 59	-14 19	-0 37	-12 54	
			Sm.	- 8 55	E.		-2 52	-11 47			
10 P.M.	-33 39	166 34	O.	- 8 35	E. by N.		-2 39	-11 14			
			T.	-10 50	E. by N.		-2 39	-13 29			
11 A.M.	-33 32	167 34	R.	-11 56	N.E. by N.	-59 30	-1 10	-13 06	-0 37	-13 56	
			T.	-10 46	E.S.E.		-2 56	-13 42			
			W.	-10 32	E. $\frac{1}{2}$ N.		-2 42	-13 14			
			O.	-10 51	E.S.E.		-2 56	-13 47			
			Sm.	- 7 46	E. by S.	-58 10	-2 56	-10 42	-0 37	-12 54	
			T.	-10 32	E.		-2 49	-13 21			
	-33 32	167 41	S.	- 9 03	E. by S.		-2 56	-11 59			
	-33 31	167 51	S.	-11 11	E.N.E.		-2 16	-13 27			
			R.	-11 04	E.N.E.	-59 30	-2 16	-13 20	-0 37	-13 56	
			R.	-11 13	E.		-2 48	-14 01			
			O.	-10 48	E. by N.		-2 42	-13 30			
			S.	- 9 45	E. by N.		-2 42	-12 27			
	-33 32	167 59	R.	-10 29	E. by N.	-58 10	-2 42	-13 11	-0 37	-13 56	
15 A.M.	-33 55	171 58	T.	- 8 13	E. by S.		-2 47	-11 00			
			O.	- 8 02	E. $\frac{1}{2}$ S.		-2 44	-10 46			
			S.	- 8 33	E. $\frac{1}{2}$ S.		-2 44	-11 17			
			T.	- 8 15	E. by S.	-58 10	-2 47	-11 02	-0 37	-13 56	
	-33 54	171 58	R.	- 8 22	E. by S. $\frac{1}{2}$ S.		-2 47	-11 09			
16 A.M.	-34 25	172 51	Y.	-14 11	N.N.W. $\frac{1}{2}$ W.		+0 53	-13 18			
			Y.	-13 09	N.W. $\frac{1}{2}$ W.		+1 38	-11 31			
			Y.	-14 46	N.W. by N.	-58 10	+1 04	-13 42	-0 37	-13 56	
			T.	-14 58	N.W. $\frac{1}{2}$ N.		+1 14	-13 44			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.	
	Lat.	Long.										
Aug. 17 A.M.	-34 15	173 12	T.	-11 14	E. by S.	-58 10	-2 48	-14 02	-0 37	-13 56	By the magnetometers on shore.	
17 P.M.	-34 37	173 55	S.	-10 11	E.S.E.		-2 48	-12 59				
			O.	-11 20	E.S.E.		-2 48	-14 08				
			R.	-10 18	E.S.E.		-2 48	-13 06				
			R.	-10 39	E. by S. 1/2 S.		-2 48	-13 27				
			O.	-9 25	E. by S. 1/2 S.		-2 48	-12 13				
			R.	-11 27	E. by S.	-2 48	-14 15					
Aug. & Sept.	Bay of Islands.											
	-35 16	174 00	R.	-13 36	-13 36		
Nov. 24 A.M.	-36 27	177 20	SM.	-8 57	E.S.E.	-59 40	-2 45	-11 42	-1 20	-14 24		
		177 21	O.	-8 51	E.S.E.		-2 45	-11 36				
24 P.M.	-36 34	177 47	S.	-10 45	S.E. by E.		-2 36	-13 21				
		177 56	S.	-11 46	S.E. by E.		-2 36	-14 22				
	-36 40	177 58	O.	-11 52	S.E. by E.		-2 36	-14 28				
	-36 42	178 08	R.	-9 47	S.E. by E.		-2 36	-12 23				
	-36 44	178 10	R.	-10 38	S.E. by E.	-2 36	-13 14					
			T.	-10 19	S.E. by E.	-2 36	-12 55					
			T.	-11 20	S.E. by E.	-2 36	-13 56					
	-36 50	178 18	R.	-10 13	S.E. by E.	-2 36	-12 49					
			R.	-10 27	S.E. by E.	-2 36	-13 03					
25 A.M.	-37 59	179 37	T.	-11 54	S.E. by S.	-60 14	-1 56	-13 50	-1 20	-14 44		
			SM.	-11 11	S.E. by S.		-1 56	-13 07				
	-38 01	179 40	T.	-11 07	S.E. 1/2 S.		-2 09	-13 16				
			SM.	-10 29	S.E. by S.		-1 56	-12 25				
			O.	-11 42	S.E. 1/2 S.		-2 09	-13 51				
			S.	-10 06	S.E.		-2 22	-12 28				
	-38 03	179 41	T.	-11 15	S.E. 1/2 S.	-2 09	-13 24					
25 P.M.	-38 22	180 10	R.	-10 43	E.S.E.	-60 20	-2 49	-13 32	-1 20	-14 43		
			Y.	-10 19	S.E. 1/2 E.		-2 32	-12 51				
	-38 27	180 02	R.	-11 09	S.E. 1/2 E.		-2 32	-13 41				
			R.	-11 26	S.E. by E.		-2 40	-14 06				
			T.	-10 06	S.E. by E. 1/2 E.		-2 44	-12 50				
			R.	-11 39	S.E. by E.		-2 40	-14 17				
26 P.M.	-39 04	182 29	O.	-11 29	S.E. by E.	-61 05	-2 44	-14 13	-1 20	-14 43		
			T.	-10 10	S.E. 1/2 E.		-2 35	-12 45				
			T.	-11 05	S.E. by E.		-2 44	-13 49				
	-39 05	182 32	R.	-10 37	S.E. by E. 1/2 E.		-2 49	-13 26				
			R.	-9 39	E.S.E.		-2 53	-12 32				
			R.	-10 36	S.E. by E.		-2 44	-13 20				
	-39 08	182 36	T.	-9 49	S.E. by E.	-2 44	-12 33					
	-39 09	182 40	R.	-9 49	E.S.E.	-2 53	-12 42					
27 A.M.	-39 16	182 59	T.	-11 47	N.E. by E.	-61 42	-1 58	-13 45	-1 20	-14 43		
			SM.	-11 09	S.E. by E.		-2 48	-13 57				
			S.	-12 33	N.		0 00	-12 33				
			T.	-12 30	N.N.E. 1/4 E.		-0 53	-13 23				
	-39 17	182 58	O.	-12 41	N.N.E. 1/2 E.		-0 58	-13 39				
28 A.M.	-40 23	183 04	S.	-12 02	s. by E.		-0 45	-12 47				
	-40 27	183 03	T.	-11 20	s. by E.	-0 45	-12 05					
28 P.M.	-40 22	183 14	R.	-9 10	S.S.E. 1/2 E.	-62 12	-1 46	-10 56	-1 20	-12 57		
			T.	-9 32	S.S.E.		-1 27	-10 59				
		183 16	R.	-8 46	S.E. by S.		-2 04	-10 50				
			O.	-8 53	S.E. 1/2 S.		-2 17	-11 10				
	-41 07	183 22	R.	-9 34	S.E.		-2 31	-12 05				
			S.	-10 10	S.E.		-2 31	-12 41				
	-41 09	183 23	R.	-10 33	S.S.E.	-1 26	-11 59					
	-41 10	183 24	R.	-9 12	S.E. by S.	-2 03	-11 15					
	-41 11	183 25	R.	-8 56	S.E. by S.	-2 03	-10 59					

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Nov. 29 A.M.	-41 28	183 41	Y.	-15 20	w.s.w.	-63 20	+3 09	-12 11	-1 20	-14 24	
			T.	-14 41	s.w. $\frac{1}{2}$ S.		+2 23	-12 18			
			T.	-11 59	s. by E.		-0 47	-12 46			
			T.	-12 55	s. by E.		-0 47	-13 42			
	-41 30	183 43	T.	-13 02	s. by E.	-65 00	-0 47	-13 49	-1 20	-14 24	
			S.	-10 38	s. by E.		-0 47	-11 25			
			T.	-12 15	s. by E.		-0 47	-13 02			
			O.	-13 14	s. by E.		-0 47	-14 01			
30 A.M.	-43 28	183 04	R.	-13 23	s. $\frac{1}{4}$ E.	-66 30	-0 16	-13 39	-1 20	-16 35	
			T.	-14 02	s.		0 0	-14 02			
Dec. 1 A.M.	-43 30	183 03	O.	-12 49	s.	-67 55	0 0	-12 49	-1 20	-16 35	
			T.	-12 16	S.E. by E. $\frac{1}{2}$ E.		-3 24	-15 40			
			W.	-11 47	S.E. by E.		-3 18	-15 05			
			Y.	-13 08	S.E. by E.		-3 18	-16 26			
	-45 32	183 11	T.	-11 02	S.E. by E. $\frac{1}{2}$ E.	-67 55	-3 24	-14 26	-1 20	-16 35	
			W.	-10 22	S.E. by E.		-3 18	-13 40			
			S.	-12 26	S.E. by E.		-3 18	-15 44			
			T.	-12 30	S.E. by E. $\frac{1}{2}$ E.		-3 44	-16 14			
2 A.M.	-46 40	184 18	W.	-11 54	S.E. by E.	-67 55	-3 36	-15 30	-1 20	-16 35	
			Y.	-10 33	S.E. by E.		-3 36	-14 09			
			Sm.	-11 24	S.E. by E.		-3 36	-15 00			
			T.	-12 31	S.E. by E. $\frac{1}{2}$ E.		-3 44	-16 15			
	-46 45	183 13	T.	-11 33	E.S.E.	-67 55	-3 52	-15 25	-1 20	-15 45	
			Sm.	-11 07	S.E. by E.		-3 36	-14 43			
			S.	-11 28	E. by S.		-3 57	-15 25			
			T.	-11 00	S.E. $\frac{1}{2}$ E.		-3 24	-14 24			
2 P.M.	-47 26	184 42	T.	-11 29	S.E. by E. $\frac{1}{2}$ E.	-67 55	-3 44	-15 13	-1 20	-15 45	
			T.	-10 36	S.E. by E.		-3 36	-14 12			
			W.	-11 28	S.E. $\frac{1}{2}$ E.		-3 24	-14 52			
			S.	-11 32	S.E. by E.		-3 36	-15 08			
	-47 32	184 53	T.	-10 43	S.E. by E.	-69 05	-3 36	-14 19	-1 20	-16 23	
			O.	-11 07	S.E. $\frac{1}{2}$ E.		-3 24	-14 31			
			R.	-10 27	S.E. $\frac{3}{4}$ E.		-3 30	-13 57			
			R.	-9 25	S.E. by E.		-3 36	-13 01			
	-47 38	185 00	R.	-9 47	S.E. by E. $\frac{1}{2}$ E.	-69 05	-3 44	-13 31	-1 20	-16 23	
			S.	-12 19	N.E. by E. $\frac{1}{2}$ E.		-3 11	-15 30			
			S.	-11 26	E.S.E.		-4 04	-15 30			
			T.	-11 35	E. $\frac{1}{2}$ N.		-3 52	-15 27			
	-48 53	186 49	R.	-10 25	S.E. by E.	-69 05	-3 47	-14 12	-1 20	-16 23	
			R.	-11 01	S.E. by E.		-3 47	-14 48			
			O.	-10 53	S.E. by E. $\frac{1}{2}$ E.		-3 55	-14 48			
			Sm.	-11 32	S.E. by E.		-3 47	-15 19			
	-48 50	186 44	Y.	-10 48	S.E. by E. $\frac{1}{2}$ E.	-69 05	-3 55	-14 43	-1 20	-16 23	
			T.	-10 49	S.E. by E.		-3 47	-14 36			
			W.	-10 59	S.E. by E.		-3 47	-14 46			
			S.	-11 20	S.E. by E.		-3 47	-15 07			
	-48 54	186 46	R.	-10 23	E.S.E.	-69 40	-4 04	-14 27	-1 20	-17 51	
			T.	-10 49	E.S.E.		-4 04	-14 53			
			R.	-11 42	S.E. by E.		-3 47	-15 29			
			R.	-12 35	S.E. $\frac{1}{2}$ E.		-3 33	-16 08			
4 A.M.	-49 10	187 32	R.	-12 52	E. by S.	-69 40	-4 18	-17 10	-1 20	-17 51	
5 A.M.	-49 32	188 59	T.	-11 28	E. by S.		-4 18	-15 46			
			O.	-11 12	E. by S.		-4 18	-15 30			
			S.	-13 13	E. by S.		-4 18	-17 31			
5 P.M.	-49 31	189 20	S.	-13 21	E. by S.	-69 40	-4 18	-17 39	-1 20	-17 51	
			W.	-11 45	E. by S.		-4 18	-16 03			
			T.	-12 35	E. by S.		-4 18	-16 53			
			R.	-11 28	E.		-4 07	-15 35			
	-49 32	189 28	R.	-11 28	E.						

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declination.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Dec. 6 A.M.	-49 57	191 06	R.	-11 47	E. by S.	-69 37	-4 18	-16 05	-1 20	-18 23	
			R.	-12 34	E. by S.		-4 18	-16 52			
			T.	-12 58	E. by S.		-4 18	-17 16			
			O.	-13 50	E. by S.		-4 18	-18 08			
	-50 04	191 15	S.	-13 13	E. by S.		-4 18	-17 31			
6 P.M.	-50 03	191 38	T.	-14 25	N.E. $\frac{3}{4}$ E.		-2 52	-17 17			
			T.	-14 02	E. by N.		-3 53	-17 55			
			S.	-15 52	N.E. by N.		-1 54	-17 46			
			T.	-12 37	E.S.E.		-4 12	-16 49			
	-50 04	191 40	T.	-13 40	E. by S. $\frac{1}{2}$ S.		-4 15	-17 55			
		191 44	R.	-11 21	E.S.E.	-69 49	-4 12	-15 33	-1 20	-18 18	
	-50 06	191 56	S.	-11 44	S.E. $\frac{1}{2}$ E.		-3 40	-15 24			
7 A.M.	-50 36	192 00	Sm.	-15 43	S. by E. $\frac{3}{4}$ E.		-1 40	-17 23			
	-50 51	192 20	S.	-13 39	E.S.E.		-4 14	-17 53			
	-50 54	192 40	R.	-13 51	S.E. $\frac{1}{2}$ S.		-3 06	-16 57			
		192 45	T.	-13 58	S.E.		-3 26	-17 24			
			R.	-12 42	S.E. $\frac{1}{2}$ E.		-3 40	-16 22			
	-50 56	192 44	R.	-12 24	S.E.		-3 26	-15 50			
8 A.M.	-51 30	193 57	T.	-11 39	E. by S.		-4 25	-16 04			
	-51 31	194 00	T.	-11 54	E. by S.		-4 25	-16 19			
			W.	-11 28	E. by S.	-70 11	-4 25	-15 53	-1 20	-15 16	
			W.	-11 27	E. by S.		-4 25	-15 52			
			T.	-12 48	E. by S.		-4 25	-17 13			
			Sm.	-13 15	E. by S.		-4 25	-17 40			
	-51 31	194 03	O.	-12 32	E. by S.		-4 25	-16 57			
8 P.M.	-51 41	195 04	T.	-8 21	E. $\frac{1}{2}$ S.		-4 20	-12 41			
			O.	-8 34	E. $\frac{1}{2}$ S.		-4 20	-12 54			
			S.	-9 39	E. $\frac{1}{2}$ S.		-4 20	-13 59			
			T.	-9 54	E. $\frac{1}{2}$ S.		-4 20	-14 14			
	-51 45	195 26	R.	-8 29	E. $\frac{1}{2}$ S.		-4 20	-12 49			
			T.	-8 27	E. $\frac{1}{2}$ S.	-70 11	-4 20	-12 47	-1 20	-13 58	
	-51 46		W.	-9 09	E. $\frac{1}{2}$ S.		-4 20	-13 29			
			R.	-8 48	E. $\frac{1}{2}$ S.		-4 20	-13 08			
	-51 47	195 37	R.	-8 07	E. by S.		-4 25	-12 32			
			T.	-8 24	E. by S.		-4 25	-12 49			
	-51 49	195 46	R.	-8 06	E. by S.		-4 25	-12 31			
9 A.M.	-52 26	198 23	T.	-9 29	E. by S.		-4 30	-13 39			
			R.	-9 09	E. by S.		-4 30	-13 39			
			O.	-9 17	E. by S.		-4 15	-12 16			
11 P.M.	-52 50	204 00	T.	-8 01	E. $\frac{1}{2}$ N.		-4 12	-13 16			
			S.	-9 04	E. $\frac{3}{4}$ N.	-70 38	-4 25	-12 39	-1 20	-13 06	
			O.	-8 14	E. $\frac{1}{4}$ S.		-4 22	-11 27			
			T.	-7 05	E.		-4 27	-10 49			
			R.	-6 22	E.S.E.		-4 27	-12 02			
			T.	-7 35	E.S.E.		-4 27	-12 25			
		203 15	W.	-7 58	E.S.E.		-4 20	-11 07			
12 A.M.	-53 10	205 15	Sm.	-6 47	E.S.E.		-4 20	-11 55			
			Y.	-7 35	E.S.E.		-4 20	-11 57			
			O.	-7 37	E.S.E.		-4 20	-12 15			
	-53 04	205 18	S.	-7 55	E.S.E.		-4 20	-11 41			
			T.	-7 21	E.S.E.	-70 11	-4 20	-11 43	-1 20	-13 06	
			O.	-7 23	E.S.E.		-4 20	-11 43			
			R.	-7 23	E.S.E.		-4 20	-11 42			
			T.	-7 22	E.S.E.		-4 20	-11 35			
			R.	-7 15	E.S.E.		-4 20	-12 28			
			T.	-8 08	E.S.E.		-4 20	-11 34			
			W.	-7 14	E.S.E.		-4 10	-11 29			
12 P.M.	-53 22	206 10	R.	-7 19	S.E. by E. $\frac{1}{2}$ E.		-4 10	-11 29			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Dec. 13 A.M.	-54 45	209 02	S.	- 7 35	E.S.E.	-70 47	-4 27	-12 02	-1 20	-14 26	
			T.	- 7 51	S.E. by E. $\frac{1}{2}$ E.		-4 17	-12 08			
	-54 46	209 07	R.	- 7 18	S.E. by E. $\frac{1}{2}$ E.		-4 17	-11 35			
			T.	- 7 06	S.E. by E. $\frac{1}{2}$ E.		-4 17	-11 23			
	-54 48	209 10	W.	- 7 40	S.E. by E. $\frac{1}{2}$ E.		-4 07	-11 47			
			R.	-10 24	S.E. by E. $\frac{1}{2}$ E.		-4 17	-14 41			
	13 P.M.	-55 16 210 14	S.	-11 36	S.E. by E.		-4 07	-15 43			
		-55 17 210 20	S.	-11 20	S.E. by E.		-4 07	-15 27			
14 A.M.	-56 06	211 33	T.	-12 31	S.E. by S.		-3 03	-15 34			
	-56 04		Y.	-12 14	S.E. by S.		-3 03	-15 17			
	-56 10	211 44	T.	-11 45	S.E. by S.		-3 03	-14 48			
			Sm.	-12 52	S.E. by S.		-3 03	-15 55			
14 P.M.	-56 15	211 49	R.	-11 57	S.E. by S.	-72 00	-3 03	-15 00	-1 20	-15 43	
	-56 22	211 56	T.	- 8 36	E. $\frac{1}{4}$ N.		-4 35	-13 11			
			S.	- 9 02	E.N.E.		-4 02	-13 04			
			T.	- 9 44	E.N.E.		-4 02	-13 46			
			T.	-10 01	N.E.		-2 54	-12 55			
			S.	- 9 03	N.E. $\frac{1}{2}$ E.		-3 13	-12 16			
			S.	- 8 11	E. $\frac{1}{2}$ N.		-4 35	-12 46			
		211 58	R.	- 8 51	E.N.E.		-4 02	-12 53			
	-56 23	211 59	W.	- 8 51	E. by N.	-72 00	-4 27	-13 18	-1 20	-13 50	
			R.	- 8 37	S.E. by S.		-3 03	-11 40			
			T.	- 9 10	S.E. by S.		-3 03	-12 13			
			W.	- 9 02	S.E. by S.		-3 03	-12 05			
			T.	- 9 31	S.E. by S.		-3 03	-12 34			
	-56 24	211 59	W.	- 9 44	S.E. by S.		-3 03	-12 47			
	15 A.M.	-56 50 212 12	T.	-11 01	S. by E. $\frac{1}{2}$ E.		-1 40	-12 41			
			Sm.	-11 34	S. by E.		-1 08	-12 42			
			Y.	-10 29	S.S.E.	-72 39	-2 13	-12 42	-1 20	-13 32	
			T.	-10 25	S.S.E.		-2 13	-12 38			
			S.	- 9 31	S.S.E.		-2 13	-11 44			
	-56 59	212 41	O.	- 9 21	S.E. by S.		-3 09	-12 30			
			R.	- 8 24	S.E. by S.		-3 09	-11 33			
	-57 01	212 42	R.	- 7 56	S.E. by S.		-3 09	-11 05			
	15 P.M.	-57 13 212 45	T.	- 9 41	S.S.E.		-2 10	-11 51			
			S.	- 9 43	S.S.E.		-2 10	-11 53			
			W.	- 9 36	S.S.E.		-2 10	-11 46			
			R.	- 9 45	S.S.E.		-2 10	-11 55			
	-57 14	212 45	T.	- 9 28	S.S.E.		-2 10	-11 38			
			R.	- 9 51	S.S.E.		-2 10	-12 01			
			Y.	-11 51	S.S.E.	-72 12	-2 10	-14 01	-1 20	-13 54	
	-57 16	212 45	T.	-10 12	S.S.E.		-2 10	-12 22			
			T.	- 9 11	E.N.E.		-4 05	-13 16			
			S.	- 8 07	E.N.E.		-4 05	-12 12			
			S.	- 9 29	E.S.E.		-4 47	-14 16			
			S.	- 8 53	S.E.		-3 51	-12 44			
	-57 19	212 47	R.	-11 12	S.S.E.		-2 10	-13 22			
	16 A.M.	-58 12 213 09	S.	- 9 20	S.S.E.						
	-58 13	213 08	T.	- 9 27	S.S.E.						
			O.	- 9 44	S.S.E.						
			S.	-10 37	S.S.E.						
	-58 15	213 08	T.	-10 08	S.S.E.						
			Y.	-10 47	S.S.E.	-73 55	-2 21	-13 12	-1 20	-14 37	
			T.	-11 56	S.S.E.						
	-58 21	213 17	R.	-12 32	S.S.E.						
			W.	-11 17	S.S.E.						
			R.	-12 08	S.S.E.						
	-58 25	213 06	R.	-11 28	S.S.E.						
	17 A.M.	-60 02 213 45	S.	-11 32	S.S.E.		-75 40	-2 40			
								-14 12			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Dec. 18 A.M.	-62 40	212 49	T.	-17 18	s. $\frac{1}{2}$ E.	°	-0 44	-18 02	°	°	
			R.	-19 25	s. by w.		+1 28	-17 57			
			W.	-19 14	s. $\frac{1}{4}$ w.		+0 22	-18 52			
			R.	-20 47	s. by w.		+1 28	-19 19			
18 P.M.	-62 45	212 44	SM.	-19 54	s. $\frac{1}{2}$ w.	-76 49	+0 44	-19 10	-1 20	-20 14	
			R.	-26 11	s.w. $\frac{1}{2}$ w.		+5 30	-20 41			
	-62 50	211 46	R.	-25 40	s.w. $\frac{1}{2}$ w.		+5 30	-19 10			
			R.	-23 59	s.w. $\frac{1}{2}$ w.		+5 30	-18 29			
	-62 53	211 34	T.	-23 47	s.w. $\frac{1}{2}$ w.		+5 30	-18 17			
			W.	-25 11	s.w. $\frac{3}{4}$ w.		+5 41	-19 30			
			R.	-21 25	s.s.w.		+2 57	-18 28			
			R.	-21 49	s.s.w.		+2 57	-18 52			
19 A.M.	-63 19	210 25	S.	-23 12	s.w.	-77 40	+5 27	-17 45	-1 20	-20 39	
			O.	-23 26	s.s.w. $\frac{1}{2}$ w.		+3 45	-19 41			
	-63 20	210 22	W.	-23 32	s.s.w. $\frac{1}{2}$ w.		+3 45	-19 47			
			T.	-23 34	s.w. by s.		+4 25	-19 09			
			T.	-22 11	s.s.w.		+3 11	-19 00			
			R.	-22 07	s. by w.		+1 33	-20 34			
	-63 19	210 17	R.	-19 19	Observed on ice.	-77 36		-19 19	-0 06		H 162
			R.	-20 43				-20 43			
			R.	-22 35				-22 35	+1 00	-19 59	H 167
			R.	-18 24				-18 24			
			R.	-18 44				-18 44	-0 06		H 166
			R.	-18 44				-18 44			
19 P.M.	-63 23	210 05	S.	-13 00	E.N.E.		-6 07	-19 07			
			T.	-13 39	E. by N.		-6 40	-20 19			
			T.	-26 28	w.s.w.		+6 46	-19 42			
			T.	-21 32	s. by w. $\frac{3}{4}$ w.		+2 44	-18 48			
			S.	-23 31	s.s.w. $\frac{1}{4}$ w.		+3 27	-20 04			
			T.	-23 58	s. 42° w.		+5 10	-18 48			
			S.	-24 37	s.w.	-77 36	+5 25	-19 12	-1 20	-20 44	
			S.	-26 46	s.w. by w. $\frac{1}{2}$ w.		+6 22	-20 24			
			T.	-21 44	s. 22° w.		+3 07	-18 37			
			T.	-24 23	s. 42° w.		+5 10	-19 13			
			T.	-23 43	s. 33° w.		+4 18	-19 25			
			S.	-23 21	s.w. by s.		+4 21	-19 00			
			T.	-25 01	s. 54° w.		+6 20	-18 41			
			T.	-27 10	w.s.w.		+6 47	-20 23			
20 A.M.	-63 24	209 39	S.	-23 40	s.w. by s.		+4 39	-19 01			
	-63 36	208 45	O.	-23 49	s.s.w.		+3 17	-20 32			
			T.	-23 16	s. by w. $\frac{1}{2}$ w.		+2 29	-20 47			
			T.	-19 00	s. $\frac{1}{2}$ E.		-0 50	-19 50			
21 A.M.	-64 39	206 55	S.	-18 26	s.s.e.		-3 17	-21 43	-1 20	-22 00	
			T.	-18 31	s. by E.		-1 40	-20 11			
			W.	-18 08	s. by E. $\frac{1}{2}$ E.	-78 30	-2 29	-20 37			
			T.	-20 30	s.		0 0	-20 30			
			S.	-21 18	s.		0 0	-21 18			
			R.	-25 18	s.w. by s.		+4 39	-20 39			
	-64 49	206 10	W.	-20 29	s. by E.		-1 40	-22 09			
	-64 50	206 05	T.	-19 35	s. $\frac{1}{2}$ E.		-0 51	-20 26			
			R.	-21 56	s. $\frac{3}{4}$ w.		+1 16	-20 40			
			R.	-19 25	s. $\frac{3}{4}$ E.		-1 16	-20 41			
	-64 54	206 06	R.	-18 54	s. by E.	-78 50	-1 40	-20 34	-1 20	-22 51	
			R.	-22 38	s. 11° E.		-1 36	-24 14			
			R.	-20 24	s. 9° E.		-1 18	-21 42			
			R.	-17 56	s. 8° E.		-1 09	-19 05			
	-64 56	206 04	R.	-23 07	s. 11° E.		-1 36	-24 43			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Dec. 22 A.M.	-65 14	206 07	S.	-22 02	s. $\frac{3}{4}$ w.	-79 20	+1 20	-20 42	-1 20	-21 51	
	-65 13	205 55	O.	-24 24	s. by w. $\frac{1}{2}$ w.		+2 38	-21 46			
	-65 13	205 47	T.	-22 14	s. by w.		+1 47	-20 27			
	-65 13	205 47	S.	-22 39	s. by w.		+1 47	-20 52			
	-65 16	206 00	Y.	-22 02	s. by w.	-79 20	+1 47	-20 15	-1 20	-21 51	
	-65 16	206 00	O.	-20 44	s. by w.		+1 47	-18 57			
	-65 16	206 00	T.	-22 13	s. by w.		+1 47	-20 26			
	-65 16	206 00	T.	-22 58	s. by w. $\frac{1}{4}$ w.		+2 14	-20 44			
	-65 21	206 08	W.	-23 00	s.s.w.	-79 20	+3 28	-19 32	-1 20	-22 46	
	-65 21	206 08	W.	-19 56	s.		0 0	-19 56			
	-65 23	206 06	R.	-22 43	s. $\frac{1}{2}$ w.		+0 53	-21 50			
	-65 23	206 06	R.	-23 11	s. $\frac{1}{2}$ w.		+0 53	-22 18			
22 P.M.		205 50	S.	-18 11	s.s.e.	-79 20	-3 28	-21 39	-1 20	-22 46	
	-65 38	205 47	T.	-21 14	s. $\frac{1}{2}$ w.		+0 26	-20 48			
	-65 39	205 44	Y.	-22 02	s.		0 0	-22 02			
	-66 00	205 46	R.	-21 18	N. by E. $\frac{1}{2}$ E.		-2 06	-23 24			
24 P.M.	-65 59	203 47	T.	-27 28	s.s.w.	-79 45	+3 35	-23 53	-1 20	-24 13	
25 P.M.	-66 01	203 56	T.	-26 45	N.W. by N.		+4 20	-22 25			
	-66 16	203 44	T.	-14 34	S.E. by E. $\frac{1}{2}$ E.		-7 50	-22 24			
	-66 17	203 36	S.	-14 42	E.S.E.		-8 10	-22 52			
27 A.M.	-66 16	203 44	S.	-16 17	E. by N. $\frac{1}{2}$ N.	-80 00	-8 02	-24 19	-1 20	-25 36	
28 A.M.	-66 17	203 36	T.	-30 17	s.w. by s.		+5 17	-25 00			
	-66 17	203 36	T.	-29 00	s.s.w. $\frac{1}{2}$ w.		+4 28	-24 32			
	-66 17	203 36	R.	-30 56	s.w.		+6 39	-24 17			
	-66 24	203 51	W.	-30 50	s.w.	-80 00	+6 39	-24 11	-1 20	-25 36	
	-66 24	203 51	W.	-31 36	W.N.W.		+7 43	-23 53			
	-66 24	203 51	T.	-31 41	W.N.W.		+7 43	-23 58			
	-66 24	203 51	T.	-30 30	N.W. $\frac{1}{2}$ w.		+6 18	-24 12			
29 P.M.	-66 25	203 51	S.	-17 13	E. by N. $\frac{1}{2}$ N.	-79 45	+8 02	-25 15	-1 20	-26 36	
	-66 25	203 51	R.	-31 25	S.W. by W. $\frac{1}{2}$ w.		+8 02	-23 23			
	-66 31	203 06	T.	-30 38	s.w.		+6 39	-23 59			
30 P.M.	-66 31	203 06	T.	-30 38	s.w.		+6 39	-23 59			
1842.											
Jan. 6 P.M.	-66 04	203 17	R.	-26 58	s. $\frac{1}{4}$ w.	-79 56	+0 28	-26 30	-1 20	-26 59	
	-66 04	203 17	Sm.	-26 38	s. $\frac{1}{2}$ w.		+0 56	-25 42			
	-66 04	203 17	R.	-28 16	s. by w. $\frac{1}{4}$ w.		+2 20	-25 56			
	-66 04	203 17	Sm.	-28 38	s. by w. $\frac{1}{2}$ w.		+2 46	-25 52			
	-66 05	203 13	R.	-23 42	N. by E.	-79 45	-1 33	-25 14	-1 20	-26 36	
	-66 05	203 13	R.	-27 26	N. by w. $\frac{1}{4}$ w.		+1 54	-25 32			
	-66 05	203 13	T.	-27 14	N. by w. $\frac{1}{2}$ w.		+2 16	-24 58			
	-66 05	203 13	T.	-30 55	N.W. $\frac{1}{4}$ N.		+6 26	-25 29			
7 P.M.	-66 20	204 19	T.	-32 04	N.W. $\frac{1}{2}$ w.	-79 45	+6 07	-25 57	-1 20	-26 36	
	-66 20	204 19	T.	-32 41	N.W. $\frac{1}{2}$ w.		+6 07	-26 37			
	-66 14	204 48	R.	-32 34	S.W. by w.		+7 31	-25 03			
	-66 15	204 50	R.	-16 07	E. by s.		-8 28	-24 35			
	-66 15	204 50	R.	-33 01	s.w. by w.	-79 52	+7 31	-25 30	-1 20	-25 55	
	-66 15	204 50	R.	-28 21	s.s.w. $\frac{1}{2}$ w.		+4 26	-23 56			
	-66 12	204 26	Sm.	-16 58	E.		-8 25	-25 23			
	-66 12	204 26	O.	-16 49	S.E. by E. $\frac{1}{2}$ E.		-7 55	-24 44			
	-66 15	204 26	S.	-16 50	E. by s. $\frac{1}{2}$ s.	-79 52	-8 24	-25 14	-1 20	-25 55	
	-66 15	204 26	T.	-31 46	s.w.		+6 33	-25 13			
	-66 15	204 26	O.	-30 14	s.w. $\frac{1}{2}$ s.		+5 54	-24 20			
	-66 15	204 26	S.	-17 09	E. $\frac{1}{2}$ s.		-8 26	-25 35			
	-66 15	204 26	T.	-15 31	E. by s. $\frac{1}{2}$ s.	-79 52	-8 24	-23 55	-1 20	-25 55	
	-66 15	204 26	Y.	-15 38	E. $\frac{1}{2}$ s.		-8 26	-24 04			
	-66 15	204 26	W.	-14 22	E. by s. $\frac{1}{2}$ s.		-8 24	-22 46			
	-66 15	204 26	T.	-16 12	E. by s. $\frac{1}{2}$ s.		-8 24	-24 36			

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.							
	Lat.	Long.																
Jan. 9 P.M.	-66 05	204 22	T.	-30 35	S.W. $\frac{1}{2}$ S.	-79 52	+5 54	-24 42	-1 20	-25 48								
			R.	-32 12	W.S.W.		+8 15	-23 57										
			T.	-31 41	S.W. $\frac{1}{2}$ W.		+7 04	-24 37										
			T.	-33 36	W. by S. $\frac{1}{4}$ S.		+8 28	-25 08										
			T.	-31 17	S.W. $\frac{1}{4}$ W.		+6 48	-24 29										
			S.	-30 16	S.W.		+6 33	-23 43										
			-66 03	204 25	T.		-15 20	S.E. by E. $\frac{1}{2}$ E.				-7 55	-23 15					
			T.	-16 04	E. by S. $\frac{1}{2}$ S.		-8 24	-24 28										
	-66 04	204 17	R.	-17 33	S.E. $\frac{1}{4}$ S.		-6 14	-23 47				-1 20	-25 48					
		204 14	R.	-32 25	S.W. by W. $\frac{3}{4}$ W.		+8 05	-24 20										
	-66 06	204 11	T.	-32 10	S.W. by W.		+7 35	-24 35				-79 48	-1 20	-25 26				
			R.	-16 55	S.E. by E. $\frac{3}{4}$ E.		-8 05	-25 00										
			T.	-17 02	S.E. by E.		-7 35	-24 37										
			R.	-33 07	S.W. by W. $\frac{1}{2}$ W.		+7 55	-25 12										
			Sm.	-33 10	W.S.W.		+8 15	-24 55										
			R.	-16 37	E. by N.		-8 15	-24 52										
S.			-17 38	S.E.	-6 28	-24 06												
O.			-17 28	S.E. $\frac{1}{4}$ E.	-6 44	-24 12												
-65 58	204 11	S.	-17 30	S.E. $\frac{1}{4}$ E.	-6 44	-24 14	-79 48	-1 20	-25 24									
		T.	-15 30	E. by S.	-8 31	-24 01												
		Y.	-15 21	E. by S.	-8 31	-23 52												
		W.	-17 02	S.E. by E. $\frac{1}{2}$ E.	-7 50	-24 52												
		T.	-16 03	S.E. by E. $\frac{1}{2}$ E.	-7 50	-23 53												
		T.	-31 55	W. by S. $\frac{1}{2}$ S.	+8 18	-23 37												
		W.	-32 25	W.S.W.	+8 09	-24 16												
		Y.	-31 49	W.S.W.	+8 09	-23 40												
10 P.M.	-66 04	204 18	T.	-31 50	S.W. by W.	+7 31	-24 19	-79 48	-1 20	-25 24								
			-65 58	204 14	R.	-16 36	S.E. by E.					-7 31	-24 07					
					T.	-15 49	S.E. by E. $\frac{3}{4}$ E.					-8 00	-23 49					
					T.	-32 23	W. by S.					+8 31	-23 52					
	-65 58	204 16			T.	-27 46	S.S.W.					+3 37	-24 09					
			O.	-32 16	S.W. by W.	+7 31	-24 45											
			-65 57	204 13	R.	-16 26	E. by S. $\frac{1}{4}$ S.					-8 25	-24 51					
					T.	-16 15	E. by S.					-8 31	-24 46					
T.	-31 12	S.W. by W.			+7 31	-23 41												
W.	-32 18	S.W.			+6 28	-25 50												
11 A.M.	-65 58	204 10	R.	-30 27	S.W. $\frac{1}{4}$ S.	+6 10	-24 17	-79 48	-1 20	-24 58								
			R.	-29 31	S.W. $\frac{3}{4}$ S.	+5 30	-24 01											
			R.	-30 14	S.W. $\frac{1}{2}$ S.	+5 50	-24 24											
			R.	-32 13	W. by S. $\frac{3}{4}$ S.	+8 18	-23 55											
	-66 01	203 51	Sm.	-21 04	S. by E.	-1 52	-22 56											
			-65 56	203 44	Y.	-19 51	S.E. by S.					-5 12	-25 03					
					T.	-26 27	S. by W. $\frac{1}{4}$ W.					+2 16	-24 43					
					Y.	-27 21	N.N.W. $\frac{1}{2}$ W.					+3 40	-23 41					
T.	-31 34	N.W. by W. $\frac{1}{2}$ W.			+7 07	-24 27												
12 A.M.	-65 52	203 45	T.	-31 42	S.W. by W.	+7 31	-24 11	-79 48	-1 20	-24 58								
			R.	-31 52	S.W. by W.	+7 31	-24 21											
			W.	-31 58	W. by S. $\frac{3}{4}$ S.	+8 18	-23 40											
			R.	-26 53	S.S.W.	+3 37	-23 16											
12 P.M.	-65 56	203 24	T.	-27 00	S.S.W.	+3 37	-23 23	-79 43	-1 20	-24 58								
			T.	-23 49	S.	0 0	-23 49											
			S.	-22 48	S.	0 0	-22 48											
			T.	-22 36	S. $\frac{3}{4}$ E.	-1 24	-24 00											
	-65 57	203 26	R.	-20 23	S. by E.	-1 52	-22 15					-79 43	-1 20	-24 58				
			14 A.M.	-66 10	202 50	Sm.	-24 36									S. by W.	+1 52	-22 44
						Sm.	-22 06									S. $\frac{3}{4}$ E.	-1 24	-23 30
						T.	-15 17									E. by N. $\frac{3}{4}$ N.	-7 40	-22 57

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Jan. 16 P.M.	-65 47	202 13	R.	-22 19	Observed on ice.	-22 19	-3 03	-25 15	R H 162 H 167 CCL CCL CCH
			R.	-26 36				-26 36	-0 05		
			R.	-24 45				-24 45	-0 28		
			R.	-24 00				-24 00	-1 20		
			R.	-23 16				-23 16	-1 20		
			R.	-22 58				-22 58	-1 20		
28 P.M.	-67 39	204 24	T.	-29 56	N. by W. $\frac{1}{2}$ W.	-80 34	+2 25	-27 31	-1 20	-27 46	
			T.	-19 02	S.S.E. $\frac{1}{2}$ E.		-4 44	-23 46			
		204 28	R.	-36 04	W. by N. $\frac{1}{4}$ N.		+8 44	-27 20			
			T.	-17 30	E.N.E.		-8 13	-25 43			
	-67 40	204 27	T.	-17 42	E. $\frac{1}{2}$ S.		-9 12	-26 54			
			R.	-16 49	E. $\frac{1}{2}$ S.		-9 12	-26 01			
			R.	-35 09	S.W. $\frac{1}{4}$ W.		+7 20	-27 49			
29 A.M.	-67 34	203 59	T.	-27 58	S. $\frac{1}{2}$ W.		+1 00	-26 58			
			T.	-16 57	E. $\frac{3}{4}$ N.		-8 57	-25 54			
31 A.M.	-67 20	202 20	T.	-28 40	S. by W. $\frac{1}{2}$ W.		+3 00	-25 40			
	-67 21	202 02	T.	-28 20	S. $\frac{1}{2}$ W.		+1 01	-27 19			
			R.	-25 59	S. $\frac{1}{2}$ E.		-1 01	-27 00			
			T.	-26 30	S.	0 0	-26 30				
			T.	-22 51	S. by E. $\frac{3}{4}$ E.	-3 28	-26 19	-1 20	-27 36		
			R.	-24 19	S. by E. $\frac{1}{2}$ E.	-3 00	-27 19				
Feb. 1 P.M.	-67 19	201 56	T.	-20 23	S.S.E. $\frac{1}{2}$ E.	-4 45	-25 08				
			W.	-19 08	S.E. by S.	-5 42	-24 50				
			T.	-34 20	N.W. by W.	+7 27	-26 53				
			R.	-37 09	W. $\frac{3}{4}$ N.	+9 09	-26 00				
			O.	-34 45	N.W. by W.	+7 27	-26 18				
			T.	-28 10	S. by W.	+2 02	-26 08				
			W.	-29 43	S. by W.	+2 02	-27 41	-1 20	-28 12		
			R.	-29 29	N.N.W. $\frac{1}{4}$ W.	+3 26	-26 03				
			R.	-25 12	N. $\frac{1}{2}$ E.	-0 50	-26 02				
		201 55	R.	-36 14	S.W. $\frac{1}{2}$ S.	+6 26	-29 48				
2 A.M.	-67 43	200 00	T.	-31 31	S.S.W.	+4 04	-27 27				
	-68 18	202 24	R.	-39 16	N.W. by W. $\frac{3}{4}$ W.	+7 55	-31 21				
	-68 17	202 32	T.	-39 48	W.S.W.	+9 19	-30 29				
3 A.M.	-68 04	199 45	W.	-21 19	S. by E. $\frac{1}{4}$ E.	-2 34	-23 53				
	-68 03	199 47	T.	-21 36	S.S.E. $\frac{1}{2}$ E.	-4 57	-26 33				
	-68 37	200 03	S.	-21 34	S.E. $\frac{1}{2}$ S.	-6 36	-28 10				
			R.	-22 08	S.E. by S.	-5 51	-27 59	-1 20	-30 25		
	-68 41	199 54	R.	-23 06	S.E. $\frac{3}{4}$ S.	-6 13	-29 19				
			R.	-39 53	W. $\frac{3}{4}$ S.	+9 42	-30 11				
			W.	-38 58	W. $\frac{1}{2}$ S.	+9 42	-29 16				
			T.	-40 19	W. $\frac{1}{2}$ S.	+9 42	-30 37				
			S.	-40 25	W. $\frac{3}{4}$ S.	+9 42	-30 43				
			O.	-39 34	W. by S.	+9 42	-29 52				
	-68 44	199 50	R.	-40 56	W. by S. $\frac{1}{2}$ S.	+9 30	-31 26				
4 A.M.	-68 49	199 42	Sm.	-24 47	S. by E. $\frac{1}{2}$ E.	-3 20	-28 07				
	-68 50		T.	-29 49	S. $\frac{1}{2}$ W.	+1 08	-28 41				
	-68 51		O.	-29 42	S. by E.	-2 16	-31 58				
	-68 46	199 48	W.	-37 01	N.N.W. $\frac{1}{2}$ W.	+4 35	-32 26				
			W.	-35 15	N.W. $\frac{1}{2}$ N.	+6 15	-29 00				
			R.	-35 57	N.W. $\frac{1}{2}$ N.	+6 15	-29 42				
			T.	-35 54	N.W. $\frac{1}{2}$ N.	+6 15	-29 39	-1 20	-32 33		
	-68 45	199 53	R.	-34 23	N.N.W. $\frac{3}{4}$ W.	+5 03	-29 20				
	-68 44	199 46	T.	-32 17	N. by W.	+2 16	-30 01				
			R.	-33 05	N. by W. $\frac{1}{4}$ W.	+2 22	-30 43				
			R.	-38 42	S.W. $\frac{1}{2}$ S.	+7 07	-31 35				
			T.	-38 31	S.W. $\frac{1}{4}$ S.	+7 31	-31 00				
	-68 45	199 50	R.	-35 32	S.S.W. $\frac{1}{4}$ W.	+4 52	-30 40				

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Feb. 8. A.M.	-70 07	186 36	S.	-27 52	S.S.E.	-83 39	-5 37	-33 29	-1 20	-35 42	
			T.	-26 51	S.S.E. $\frac{1}{2}$ E.		-6 51	-33 42			
			O.	-30 31	S. by E. $\frac{1}{4}$ E.		-3 31	-34 02			
	-70 08	186 25	S.	-33 41	S.		0 0	-33 41			
			W.	-30 23	S. by E. $\frac{1}{4}$ E.		-3 31	-33 54			
			T.	-29 56	S. by E. $\frac{1}{2}$ E.		-4 12	-34 08			
8 P.M.		186 24	T.	-33 40	S. $\frac{1}{4}$ E.		-0 43	-34 23			
	-70 34	185 47	R.	-32 55	S. by E.		-2 54	-35 49			
			T.	-33 18	S. by E.		-2 54	-36 12			
9 A.M.	-70 34	185 33	T.	-52 48	W. $\frac{1}{2}$ N.		+14 29	-38 19			
			W.	-50 28	W. by N.		+14 15	-36 13			
9 P.M.	-70 30	185 25	R.	-50 00	W. $\frac{1}{2}$ N.		+14 29	-35 31			
	-70 38	185 26	O.	-52 27	W. $\frac{1}{2}$ S.		+14 40	-37 47			
	-70 33	185 20	R.	-51 21	W. $\frac{1}{4}$ S.		+14 41	-36 20			
			T.	-51 05	W. $\frac{1}{4}$ S.		+14 41	-36 24			
			W.	-52 05	W. $\frac{1}{4}$ N.		+14 36	-37 29			
			T.	-50 17	W. $\frac{1}{4}$ N.		+14 36	-35 41			
	-70 31	185 13	R.	-51 58	W. $\frac{1}{4}$ S.		+14 41	-37 17			
			T.	-52 43	W.		+14 43	-38 00			
			R.	-52 35	W. $\frac{3}{4}$ N.		+14 22	-38 13			
	-70 26	185 05	R.	-53 52	W. $\frac{1}{4}$ N.		+14 18	-39 34			
			T.	-51 49	W. $\frac{1}{2}$ N.		+14 11	-37 38			
			R.	-51 12	W. $\frac{1}{2}$ N.		+14 11	-37 01			
	-70 25	185 00	S.	-54 00	W.		+14 25	-39 35			
	-70 22	184 17	T.	-49 11	W. $\frac{1}{2}$ S.		+14 22	-34 49			
10 A.M.			Sm.	-49 13	W.		+14 25	-34 48			
			T.	-49 48	W. $\frac{1}{2}$ N.		+14 11	-35 37			
	-70 20	184 10	Sm.	-49 51	W. $\frac{3}{4}$ S.		+14 20	-35 31			
			T.	-47 56	W. by S. $\frac{3}{4}$ S.		+13 50	-34 06			
	-70 16	183 54	O.	-46 47	S.W. by W. $\frac{1}{2}$ W.		+12 59	-33 48			
			S.	-47 11	W.S.W.		+13 34	-33 37			
			T.	-47 05	S.W. by W. $\frac{1}{2}$ W.		+12 57	-34 08			
			S.	-50 09	W. by S. $\frac{1}{2}$ S.		+13 54	-36 15			
10 P.M.	-70 11	183 52	R.	-27 10	S.E. by S.		-8 24	-35 34			
	-70 13	183 51	R.	-26 53	S.E.		-10 37	-37 30			
	-70 12	183 50	O.	-50 12	W. by S.		+14 13	-35 59			
			T.	-48 52	W. by S.		+14 13	-34 39			
			R.	-48 27	W. $\frac{1}{2}$ S.		+14 16	-34 11			
			T.	-49 13	W. $\frac{1}{4}$ N.		+14 12	-35 01			
			W.	-47 54	W. $\frac{1}{2}$ N.		+14 05	-33 49			
	-70 14	183 54	T.	-49 53	W. $\frac{1}{4}$ N.		+14 12	-35 41			
13 A.M.	-72 10	180 58	S.	-30 58	S.E.		-13 19	-44 17			
16 A.M.	-75 08	173 20	T.	-55 14	S.E. $\frac{3}{4}$ S.		-19 18	-74 32			
			R.	-56 11	S.E. $\frac{1}{2}$ S.		-20 33	-76 44			
	-75 03	173 03	T.	-56 01	S.E. $\frac{1}{2}$ S.		-20 33	-76 34			
	-76 48	182 33	T.	-85 00	N.		0 0	-85 00			
18 P.M.			R.	-84 09	N. $\frac{1}{2}$ E.		-2 39	-86 48			
			S.	-88 09	N.		0 0	-88 09			
			T.	-84 23	N.		0 0	-84 23			
			W.	-90 46	N. by W. $\frac{1}{2}$ W.		+7 53	-82 53			
	-76 47	182 33	R.	-80 25	N. $\frac{1}{2}$ E.		-2 39	-83 04			
	-76 21	194 43	T.	-63 58	S.E. $\frac{3}{4}$ S.		-12 25	-76 23			
22 A.M.	-76 29		O.	-72 18	S.S.E. $\frac{1}{2}$ E.		-9 49	-82 07			
			S.	-70 54	S.S.E.		-8 03	-78 57			
			T.	-71 09	S. by E. $\frac{1}{2}$ E.		-6 05	-77 14			
	-76 32	194 39	T.	-68 08	S.S.E. $\frac{1}{4}$ E.		-9 00	-77 08			
			W.	-72 15	S. by E.		-4 05	-76 20			
	-76 58	194 35	R.	-59 41	E. by S.		-20 00	-79 41			
	-76 57	194 28	T.	-59 00	E. by S.		-20 00	-79 00			
			R.	-59 18	E. by S.		-20 00	-79 18			
			R.	-59 57	E. by S.		-20 00	-79 57			

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declina- tion.	Remarks.			
	Lat.	Long.												
Feb. 23 A.M.	-77° 45'	198° 16'	T.	-96° 30'	S.S.W.	-85° 00'	+ 7° 08'	-89° 22'	-1° 20'	-88° 08'				
			O.	-96° 31'	S.S.W. $\frac{1}{2}$ W.		+ 8° 43'	-87° 48'						
			S.	-96° 05'	S.S.W.		+ 7° 08'	-88° 57'						
			T.	-93° 06'	S.S.W.		+ 7° 08'	-85° 58'						
			O.	-93° 39'	S.W. by S.		+10° 19'	-83° 20'						
	-77° 42'	198° 00'	T.	-94° 06'	S.S.W. $\frac{1}{2}$ W.		+ 8° 43'	-85° 23'						
			S.	-94° 02'	S.W. by S.		+10° 19'	-83° 43'						
			W.	-98° 12'	S.W. by S.		+10° 19'	-87° 53'						
			T.	-99° 25'	S.W. by S.		+10° 19'	-89° 06'						
	-77° 50'	197° 54'	W.	-98° 09'	S.W. $\frac{1}{2}$ S.		+11° 41'	-86° 28'						
23 P.M.	-77° 48'	197° 03'	R.	-69° 54'	E. $\frac{1}{2}$ S.	-85° 00'	-17° 41'	-87° 35'	-1° 20'	-87° 31'				
	-77° 56'	197° 40'	T.	-69° 07'	E. $\frac{3}{4}$ S.		-17° 39'	-86° 46'						
	-78° 00'	197° 26'	R.	-70° 06'	E. by S.		-17° 37'	-87° 43'						
			T.	-68° 51'	E. $\frac{3}{4}$ S.		-17° 39'	-86° 30'						
	-78° 02'	197° 24'	S.	-70° 14'	E.		-17° 46'	-88° 00'						
	-78° 07'	197° 34'	R.	-67° 13'	E. $\frac{1}{2}$ S.		-17° 41'	-84° 54'						
			T.	-66° 56'	E. $\frac{1}{2}$ S.		-17° 41'	-84° 37'						
			S.	-68° 23'	E.		-17° 46'	-86° 09'						
	-78° 10'	197° 43'	R.	-67° 53'	E. $\frac{1}{2}$ S.		-17° 41'	-85° 34'						
			T.	-66° 26'	E. by S.		-17° 37'	-84° 03'						
25 A.M.	-75° 13'	193° 50'	O.	-82° 32'	W.	-85° 00'	+17° 46'	-64° 46'	-1° 20'	-62° 17'				
			T.	-80° 13'	W.		+17° 46'	-62° 27'						
	-74° 40'	194° 01'	R.	-73° 01'	N.W. by W. $\frac{1}{2}$ W.		+15° 11'	-57° 50'						
	-74° 37'	194° 04'	R.	-73° 34'	W.N.W.		+16° 05'	-57° 29'						
	-74° 25'	194° 04'	T.	-76° 47'	W.N.W.		+16° 05'	-60° 42'						
		193° 55'	R.	-76° 45'	N.W. by W.		+14° 17'	-62° 28'						
27 P.M.	-71° 59'	186° 42'	T.	-57° 42'	S.W. by W. $\frac{1}{4}$ W.		+14° 00'	-43° 42'				-1° 20'	-45° 11'	
	-71° 54'	186° 30'	R.	-57° 40'	S.W. by W.		+13° 40'	-44° 00'						
28 A.M.	-71° 11'	185° 03'	T.	-52° 06'	S.W. by W. $\frac{1}{2}$ W.		+13° 51'	-38° 15'						
	-71° 09'	184° 58'	S.	-50° 45'	W.S.W.		+14° 30'	-36° 15'						
			T.	-53° 25'	S.W. by W. $\frac{1}{2}$ W.	+13° 51'	-39° 34'							
	-71° 05'	184° 45'	T.	-53° 20'	W. $\frac{1}{2}$ S.	+15° 19'	-38° 01'							
			R.	-53° 16'	W.	+15° 23'	-37° 53'							
Mar. 1 A.M.	-70° 11'	180° 32'	O.	-46° 44'	W.N.W.	+13° 52'	-32° 52'							
			T.	-45° 32'	W. by N. $\frac{1}{2}$ N.	+14° 22'	-31° 10'							
			S.	-44° 09'	W.N.W.	+13° 52'	-30° 17'							
	-70° 10'	180° 29'	T.	-46° 02'	W.N.W.	+13° 52'	-32° 10'							
			W.	-45° 45'	W.N.W.	+13° 52'	-31° 53'							
1 P.M.	-69° 36'	180° 02'	R.	-24° 21'	N. by E.	-83° 43'	- 2° 47'	-27° 08'	-1° 20'	-30° 50'				
			S.	-24° 00'	N. by E.		- 2° 47'	-26° 47'						
			T.	-24° 01'	N. by E. $\frac{1}{2}$ E.		- 4° 10'	-28° 11'						
			O.	-24° 05'	N. by E. $\frac{1}{2}$ E.		- 4° 10'	-28° 15'						
	-69° 32'	180° 08'	S.	-22° 09'	N.N.E. $\frac{1}{2}$ E.		- 6° 45'	-28° 54'						
	-69° 33'	180° 10'	T.	-21° 28'	N.N.E. $\frac{1}{2}$ E.		- 6° 45'	-28° 13'						
			R.	-21° 20'	N.N.E. $\frac{1}{2}$ E.		- 6° 45'	-28° 05'						
2 A.M.	-68° 50'	182° 38'	W.	-22° 58'	N.N.E.		- 4° 31'	-27° 29'						
	-68° 44'	182° 43'	T.	-22° 15'	N.N.E.		- 4° 31'	-26° 46'						
			W.	-22° 09'	N.N.E.		- 4° 31'	-26° 40'						
	-68° 40'	182° 53'	T.	-23° 34'	N. by E. $\frac{1}{2}$ E.	- 3° 24'	-26° 58'							
2 P.M.	-67° 53'	183° 44'	R.	-22° 49'	N. by E. $\frac{3}{4}$ E.	-82° 23'	- 3° 57'	-26° 46'	-1° 20'	-27° 32'				
	-67° 52'		S.	-20° 18'	N.E. by N.		- 6° 34'	-26° 52'						
	-67° 49'	184° 05'	T.	-17° 56'	N.E.		- 8° 27'	-26° 23'						
	-67° 47'	184° 25'	T.	-18° 59'	N.N.E. $\frac{1}{2}$ E.		- 5° 33'	-24° 32'						
			R.	-19° 10'	N. by E. $\frac{3}{4}$ E.		- 3° 57'	-23° 07'						
			W.	-16° 49'	N.E.		- 8° 27'	-25° 16'						
			R.	-18° 58'	N.E. by N.		- 6° 34'	-25° 32'						
	-67° 45'	184° 15'	R.	-21° 25'	N.E. by N.		- 6° 34'	-27° 59'						

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
March 3 A.M.	-67 34	185 19	O.	-17 21	N.E. $\frac{1}{2}$ E.	-82 00	-8 41	-26 02	-1 20	-27 32	
	-67 28	185 39	R.	-18 06	N.E. $\frac{1}{2}$ E.		-8 41	-26 47			
5 A.M.	-67 20	187 56	T.	-16 16	E. by N.	-81 10	-10 23	-26 39	-1 20	-27 32	
			W.	-14 45	E. $\frac{1}{2}$ N.		-10 35	-25 20			
6 A.M.	-65 27	191 35	Sm.	-19 52	N. by E.		-1 34	-21 26			
	-65 21	191 45	T.	-21 59	N. $\frac{1}{2}$ E.		-0 47	-22 46			
6 P.M.	-65 00	192 42	T.	-21 38	N. $\frac{3}{4}$ E.	-79 25	-1 10	-22 48	-1 20	-23 40	
		192 40	W.	-20 48	N. by E.		-1 34	-22 22			
			T.	-20 15	N. by E.		-1 34	-21 49			
			T.	-20 33	N. by E.		-1 34	-22 07			
	-64 58	192 44	T.	-21 55	N. $\frac{3}{4}$ E.	-78 17	-1 10	-23 05	-1 20	-21 57	
7 P.M.	-63 33	194 53	R.	-15 05	S.E. $\frac{1}{2}$ S.		-5 32	-20 37			
8 A.M.	-62 33	195 56	W.	-17 12	N. by E.		-1 17	-18 29			
			T.	-19 19	N. $\frac{3}{4}$ E.		-0 58	-20 17			
8 P.M.	-62 11	196 26	T.	-11 28	S.E.	-77 23	-5 44	-17 12	-1 20	-19 51	
		196 29	T.	-15 05	N.N.E. $\frac{1}{2}$ E.		-3 07	-18 12			
			R.	-15 53	N.N.E.		-2 32	-18 25			
9 A.M.	-61 15	198 29	T.	-14 36	N.E. by N.		-3 20	-17 56			
			Sm.	-13 54	N.E. by N.		-3 20	-17 14			
9 P.M.	-60 54	199 40	W.	-12 25	N.E. $\frac{3}{4}$ E.		-5 00	-17 25			
	-60 51	199 47	R.	-12 19	N.E. by E.	-76 09	-5 12	-17 30	-1 20	-18 42	
			S.	-12 12	N.E. by E.		-5 12	-17 23			
			W.	-14 24	N.E.		-4 22	-18 46			
	-60 50	199 49	R.	-11 40	N.E. by E.		-5 12	-16 52			
	-60 47	200 20	R.	-10 12	E.N.E.		-6 00	-16 12			
10 A.M.	-60 34	202 42	S.	-10 21	E.N.E.		-5 30	-15 51			
			O.	-10 09	E.N.E.	-74 15	-5 30	-15 39	-1 20	-17 31	
	-60 32	203 08	T.	-11 10	E.N.E.		-5 30	-16 40			
10 P.M.	-60 18	206 10	T.	-10 34	E. by N.		-6 00	-16 34			
12 A.M.	-60 17	212 56	S.	-10 54	E. by N.		-5 34	-16 28			
			O.	-9 58	E. by N.	-73 55	-5 34	-15 30	-1 20	-17 01	
	-60 13	213 07	T.	-8 29	E. by N. $\frac{1}{2}$ N.		-5 20	-13 49			
			S.	-11 19	E. by N.		-5 34	-16 53			
14 P.M.	-59 15	219 01	T.	-8 53	N.E.		-3 37	-12 30			
			T.	-8 33	N.E. by E.	-73 56	-4 26	-12 59			
		219 14	T.	-8 10	N.E. by E.		-4 26	-12 36			
15 A.M.	-58 44	221 51	T.	-10 06	E. by N. $\frac{1}{4}$ N.	-73 30	-5 10	-15 16	-1 20	-15 30	
			S.	-12 31	E.N.E.		-4 50	-17 21			
	-58 42	221 59	T.	-9 23	E.N.E.		-4 50	-14 13			
16 P.M.	-59 04	229 00	R.	-11 08	E. $\frac{1}{2}$ S.		-5 26	-16 34			
			S.	-11 15	E. $\frac{1}{2}$ S.	-73 00	-5 26	-16 41	-1 20	-17 49	
			O.	-10 47	E. $\frac{1}{2}$ S.		-5 26	-16 13			
			T.	-11 03	E. $\frac{1}{2}$ S.		-5 26	-16 29			
18 A.M.	-60 14	236 32	S.	-13 59	E.		-5 24	-19 23			
			O.	-15 28	E.	-73 00	-5 24	-20 52	-1 20	-20 56	
	-60 13	236 33	T.	-13 10	E.		-5 24	-18 34			
20 P.M.	-59 17	245 40	R.	-14 40	E.N.E.	-71 33	-4 14	-18 54	-1 20	-20 14	
22 A.M.	-58 40	251 52	T.	-15 41	E. by N.		-4 29	-20 10			
			W.	-15 48	E. by N.	-70 51	-4 29	-20 17	-1 20	-21 47	
			S.	-16 24	E. by N.		-4 29	-20 53			
23 A.M.	-58 42	254 46	T.	-17 28	E. $\frac{1}{2}$ N.		-4 26	-21 54			
			W.	-17 40	E. $\frac{1}{2}$ N.		-4 26	-22 06			
	-58 43	254 50	T.	-18 20	E.	-70 11	-4 35	-22 55	-1 20	-23 28	
23 P.M.	-58 38	255 34	R.	-17 58	N.E. by E. $\frac{1}{2}$ E.		-3 40	-21 38			
24 A.M.	-58 46	258 07	T.	-18 40	E.	-69 46	-4 29	-23 09	-1 20	-25 25	
			O.	-19 41	E. $\frac{1}{2}$ N.		-4 21	-24 02			
			S.	-20 42	E. $\frac{1}{2}$ N.		-4 21	-25 03			

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correction for ship's attraction.	Corrected Declina- tion.	Correction for index error.	True Declination.	Remarks.
	Lat.	Long.									
Mar. 26 A.M.	-59 00	268 07	T.	-20 21	E. by N. $\frac{1}{2}$ N.	° ' }	-3 32	-23 53	° ' }	° ' }	
			W.	-21 51	E. by N. $\frac{1}{2}$ N.		-3 32	-25 23			
		268 10	T.	-22 06	E. by N. $\frac{1}{2}$ N.		-3 32	-25 38			
26 P.M.	-59 02	268 40	T.	-22 17	E.N.E.	{-67 38	-3 24	-25 41	{-1 20	-26 17	
			R.	-22 10	E.N.E.		-3 24	-25 34			
		268 45	T.	-21 40	E.N.E.		-3 24	-25 04			
			R.	-21 31	E.N.E.		-3 24	-24 55			
			O.	-20 32	E.N.E.		-3 24	-23 56			
		269 10	R.	-21 02	E.N.E.	{-67 00	-3 24	-24 26	{-1 20	-26 51	
27 A.M.	-59 02	272 04	Sm.	-22 15	E.N.E.		-3 16	-25 31			
28 A.M.	-58 50	275 44	S.	-21 42	N.E. by E. $\frac{1}{2}$ E.		-2 50	-24 32			
			O.	-21 37	N.E. by E. $\frac{1}{2}$ E.	{-65 30	-2 50	-24 27	{-1 20	-26 18	
			W.	-24 04	N.E. by E.		-2 36	-26 40			
	-58 52	276 15	T.	-22 51	N.E. by E.		-2 36	-25 27			
	-58 54	276 53	R.	-21 06	N.E. by E.	{-64 50	-2 36	-23 42	{-1 20	-25 04	
29 A.M.	-58 24	280 05	T.	-22 22	N.E. $\frac{1}{2}$ E.		-2 15	-24 37			
29 P.M.	-58 20	280 34	R.	-20 55	N.E.		-2 02	-22 57			
	-58 19	280 31	T.	-22 12	N.E. $\frac{1}{2}$ E.	{-63 40	-2 15	-24 27	{-1 20	-26 14	
			W.	-21 09	N.E. $\frac{1}{2}$ E.		-2 15	-23 24			
		280 32	T.	-21 01	N.E. $\frac{1}{2}$ E.		-2 15	-23 16			
30 A.M.	-58 30	282 07	T.	-22 52	E.N.E.	{-63 00	-2 47	-25 39	{-1 20	-26 18	
			Sm.	-23 19	N.E. by E. $\frac{1}{2}$ E.		-2 35	-25 54			
			O.	-21 57	E.N.E.		-2 47	-24 44			
			S.	-21 46	E.N.E.	{-63 00	-2 47	-24 33	{-1 20	-26 18	
			T.	-21 53	E.N.E.		-2 47	-24 40			
	-58 29	282 01	S.	-22 24	N.E. by E.		-2 23	-24 47			
			W.	-20 46	E. by N. $\frac{1}{2}$ N.	{-63 00	-2 58	-23 44	{-1 20	-26 18	
			T.	-22 21	E.N.E.		-2 47	-25 08			
			S.	-22 09	N.E. by E.		-2 18	-24 27			
		282 22	T.	-23 34	N.E. $\frac{1}{2}$ E.	{-63 00	-2 04	-25 38	{-1 20	-26 18	
			S.	-21 39	N.E. $\frac{1}{2}$ E.		-2 04	-23 43			
	-58 28	282 24	T.	-23 30	N.E. $\frac{1}{2}$ E.		-2 04	-25 34			
31 A.M.	-58 40	285 29	W.	-24 06	N.E. $\frac{1}{2}$ N.	{-53 54	-1 36	-25 42	{-1 20	-26 29	
			S.	-22 42	N.E. by N.		-1 23	-24 05			
	-58 32	285 30	T.	-24 02	N.E. $\frac{1}{2}$ N.		-1 36	-25 38			
April 5 A.M.	-52 56	300 18	T.	-15 31	N.N.E.	{-52 30	-0 33	-16 04	{-1 20	-16 29	
			R.	-15 26	N.N.E.		-0 33	-15 59			
5 P.M.	-52 14	300 50	T.	-14 33	N. by E.		-0 16	-14 49			
6 A.M.	-51 50	301 43	T.	-12 06	E. by S.	{-52 30	-2 16	-14 22	{-1 20	-16 29	
			T.	-12 32	E. by S.		-2 16	-14 48			
			T.	-15 34	N.N.W. $\frac{1}{2}$ W.		+0 38	-14 56			

DECLINATIONS observed on board Her Majesty's Ship Terror, between June 1841 and August 1842.

The Observers are distinguished in the column of Initials as follows:—C. Captain CROZIER; P. Lieut. PHILLIPS;
Cr. Mr. COTTER, Master.

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decl- nat on.	Remarks.
	Lat.	Long.									
July 7.	-43 30	147 20	C.	- 9 37	S. 53° E.	-71 00	- 4 18	-13 55	+1 07	-12 35	Card P.
			C.	- 9 39	S. 48° E.		- 4 01	-13 40			
			C.	- 9 08	S. 48° E.		- 4 01	-13 09			
	9.	-42 23	149 31	C.	-10 05	S. 48° E.	- 4 01	-14 06	+1 07	-11 49	
				C.	-14 45	N. 22° W.	+ 1 24	-13 21			
				C.	-15 09	N. 32° W.	+ 2 03	-13 06			
		-42 08	149 30	Cr.	-14 07	N.N.W.	+ 1 25	-12 42	+1 07	-11 11	
				Cr.	-14 45	N.N.W.	+ 1 25	-13 20			
				Cr.	-13 37	N.N.W.	+ 1 25	-12 12			
	10.	-40 56	149 20	C.	-11 57	N. 12° W.	+ 0 39	-11 18	+1 07	-10 38	
				C.	-13 03	N. 12° W.	+ 0 39	-12 24			
				C.	-14 35	N. 15° W.	+ 0 58	-13 37			
11.	-40 33	149 26	C.	-12 15	N. 12° W.	+ 0 39	-11 36	+1 07	-11 32		
			Cr.	-12 55	N. 1/2° W.	+ 0 19	-12 36				
			C.	-12 58	N.	0 00	-12 58				
		-38 15	150 15	C.	-11 23	N. 15° W.	+ 0 50	-10 33	+1 07	-11 26	
				C.	-12 50	N. 8° W.	+ 0 27	-11 23			
				C.	-11 28	N. 8° W.	+ 0 27	-11 01			
	-37 47	150 21	C.	-11 46	N. 17° W.	+ 0 56	-10 50	+1 07	-10 38		
			C.	-12 35	N. 15° W.	+ 0 50	-11 45				
			C.	-12 59	N. 12° W.	+ 0 37	-12 22				
	12.	-37 25	151 25	Cr.	-13 10	N.	0 00	-13 10	+1 07	-11 32	
				C.	-10 38	N. 30° E.	- 1 31	-12 09			
				C.	- 9 55	N. 28° E.	- 1 23	-11 18			
		-37 13	151 42	C.	-11 38	N. 36° E.	- 1 47	-13 25	+1 07	-11 26	
				C.	-10 27	N. 38° E.	- 1 53	-12 20			
				C.	-12 14	N. 32° E.	- 1 37	-13 51			
-36 17		151 50	Cr.	-11 21	N.E. by N.	- 1 39	-13 00	+1 07	-11 32		
			Cr.	-11 06	N.E.	- 2 10	-13 16				
			Cr.	-12 57	N.	0 00	-12 57				
Aug. 6.		-36 17	151 50	C.	-12 47	N. 20° W.	+ 1 00	-11 47	+1 07	-11 18	
				C.	-13 23	N. 20° W.	+ 1 00	-12 23			
				C.	-10 06	N. 82° E.	- 3 01	-13 07			
	-33 56	151 0	C.	- 9 21	N. 85° E.	- 3 05	-12 26	+1 07	-11 26		
			C.	- 9 03	N. 83° E.	- 3 02	-12 05				
			C.	- 9 42	N. 70° E.	- 2 21	-12 03				
	8.	-33 25	160 45	C.	-13 21	N. 75° E.	- 2 45	-16 06	+1 07	-14 26	
				C.	-12 50	N. 70° E.	- 2 35	-15 25			
				C.	-12 41	N. 76° E.	- 2 47	-15 28			
	9.	-33 39	163 40	C.	-12 00	E.	- 2 56	-14 56	+1 07	-14 26	
				C.	-12 41	E.	- 2 56	-15 37			
				C.	-12 31	E.	- 2 56	-15 27			
10.	-33 44	166 30	C.	-12 35	N. 79° E.	- 2 43	-15 18	+1 30	-13 40		
			C.	-12 39	E.	- 2 56	-15 35				
			C.	-12 35	N. 85° E.	- 2 50	-15 25				
		-33 44	166 30	Cr.	-13 14	E.	- 2 56	-16 10	+1 30	-13 40	
				C.	-11 05	E.S.E	- 2 59	-14 04			
				C.	-13 11	S.E. by E.	- 2 50	-16 01			
	-33 44	166 30	C.	-12 22	N. 82° E.	- 2 42	-15 04	+1 30	-13 40		
			C.	-13 07	E.	- 2 52	-15 59				
			C.	-11 59	E. by S. 1/2° S.	- 2 59	-14 58				
	-33 44	166 30	C.	-12 23	E.S.E.	- 2 59	-15 22	+1 30	-13 40		
			C.	-13 25	S.E. 1/2° E.	- 2 40	-16 05				
			C.	-13 25	S.E. 1/2° E.	- 2 40	-16 05				

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.				
	Lat.	Long.													
Aug. 10.	-33 44	166 30	C.	-13 11	N. 70° E.	-60 10	-2 04	-15 15	+1 30	-13 40					
			C.	-14 20	N. 65° E.		-1 53	-16 13							
			C.	-13 12	N. 61° E.		-2 08	-15 20							
			C.	-11 15	S. 82° E.		-2 57	-14 12							
			C.	-13 13	N. 67° E.		-1 59	-15 12							
	-34 00	166 26	Cr.	-11 30	E. by N.	-2 39	-14 09								
			Cr.	-12 04	E.	-2 52	-14 56								
			Cr.	-11 33	E.S.E.	-2 59	-14 32								
			Cr.	-12 29	S.E. by E.	-2 50	-15 19								
			C.	-14 56	N. 77° E.	-2 36	-17 32								
11.	-33 32	167 35	C.	-14 34	E.		-2 49	-17 23							
			C.	-14 16	N. 73° E.		-2 27	-16 43							
			C.	-13 38	N. 78° E.		-2 36	-16 14							
			C.	-14 00	E.		-2 49	-16 49							
			C.	-12 41	S. 85° E.		-2 43	-15 24							
			C.	-13 28	N. 72° E.	-59 40	-2 25	-15 53	+1 30	-15 02					
			C.	-13 33	N. 72° E.		-2 25	-15 58							
			Cr.	-13 31	E.		-2 49	-16 20							
			C.	-13 57	N. 56° E.		-1 56	-15 53							
			C.	-15 39	N. 53° E.		-1 50	-17 29							
12.	-32 53	169 30	Cr.	-15 09	N.E.		-1 34	-16 43							
			C.	-13 22	E. 1/2 S.		-2 43	-16 05							
			C.	-11 27	E. by S.		-2 47	-14 14							
	-34 20	172 45	C.	-13 53	E.		-2 40	-16 33				+1 30	-13 45		
			C.	-14 08	E.		-2 40	-16 48							
			C.	-16 20	N. 26° W.	+0 46	-15 34								
			C.	-14 30	N. 38° W.	+1 15	-13 15								
			C.	-12 16	E.S.E.	-2 47	-15 03								
			Cr.	-15 30	N.W. by N.	+1 04	-14 26								
			Cr.	-12 34	E. by S.	-2 47	-15 21								
17.	-34 36	173 50	C.	-12 11	S. 83° E.		-2 45	-14 56	+1 30	-13 42					
			C.	-12 24	E. by S. 1/2 S.	-2 47	-15 11								
Nov. 24.	-34 17	173 35	C.	-13 20	E. by S. 1/2 S.	-58 10	-2 47	-16 07	+1 30	-13 42					
			C.	-11 38	E. by S. 1/2 S.		-2 47	-14 25							
			Cr.	-12 35	E. by S.		-2 47	-15 22							
	-36 17	177 12	Cr.	-13 51	E.S.E.		-59 40	-2 45				-16 36			
			C.	-15 02	S.E. 1/2 E.			-2 30				-17 32			
			C.	-14 57	S.E. 1/2 E.	-2 30		-17 27							
			C.	-15 53	S.E.	-2 22		-18 15							
			Cr.	-14 50	S.E. by S.	-1 56		-16 46							
			-38 17	179 54	Cr.	-14 26	S.E. by E.	-60 15	-2 39	-17 05	+1 30	-14 55			
					Cr.	-12 07	S.E. by E.		-2 39	-14 46					
-38 26	179 54	C.	-13 23	S.E. by E.	-2 39	-16 02									
		C.	-11 33	S.E. by E.	-2 39	-14 12									
26.	-39 03	182 33	C.	-12 50	S.E. by E. 1/2 E.		-2 43		-15 33						
			Cr.	-13 59	E. by S.		-2 54	-16 53							
			C.	-13 18	S.E. by E. 1/2 E.		-2 48	-16 06							
			C.	-15 57	S.E.		-2 26	-18 23							
			C.	-15 47	S.E. by E. 1/2 E.		-2 48	-18 35							
			Cr.	-14 19	S.E. by E.	-61 00	-2 44	-17 03	+1 30	-16 55					
			Cr.	-13 43	E.S.E.		-2 53	-16 36							
			Cr.	-12 32	E.S.E.		-2 53	-15 25							
			Cr.	-13 22	E.S.E.		-2 53	-16 15							
			C.	-18 06	S. by E.		-0 45	-18 51							
28.	-40 38	183 05	C.	-15 51	S.E.	-62 00	-2 31	-18 22							
			Cr.	-16 32	S.E.		-2 31	-19 03							

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Nov. 29.	-41 33	183 30	C.	-16 31	s.s.e.	-63 20	- 1 30	-18 01	+ 1 30	-15 13	
			C.	-17 03	s.e. by s.		- 2 08	-19 11			
			C.	-16 45	s. by e.		- 0 47	-17 32			
			C.	-17 09	s. by e.		- 0 47	-17 56			
			CR.	-16 08	s.		0 0	-16 08			
			CR.	-17 09	s. by w.		+ 0 47	-16 22			
			CR.	-14 51	s. by e.		- 0 47	-15 38			
			CR.	-15 02	s.s.e.		- 1 30	-16 32			
			CR.	-14 53	s. by e.		- 0 47	-15 40			
			CR.	-17 40	s.s.w.		+ 1 30	-16 10			
			CR.	-18 41	s.w. by w.		+ 2 58	-15 43			
			CR.	-18 32	s.w.		+ 2 38	-15 54			
			CR.	-18 51	w.s.w.	-65 00	+ 3 09	-15 42	+ 1 30	-15 17	
			CR.	-18 51	s.w. by s.		+ 2 08	-16 43			
			C.	-14 42	s.e. by s.		- 2 08	-16 50			
30.	43 37	183 05	C.	-16 41	s. $\frac{1}{2}$ E.		- 0 25	-17 06			
			C.	-17 56	s. $\frac{1}{2}$ W.		+ 0 25	-17 31			
			CR.	-15 53	s.		0 0	-15 53			
			CR.	-17 17	s.		0 0	-17 17			
Dec. 1.	-45 29	183 10	CR.	-14 58	s.e. by e.	-66 30	- 3 22	-18 20	+ 1 30	-16 52	
			CR.	-16 21	s.e. by e.		- 3 22	-19 43			
2.	-47 09	184 30	C.	-15 40	E.S.E.		- 3 36	-19 16			
			C.	-14 54	s.e. by E. $\frac{1}{2}$ E.		- 3 29	-18 23			
	-47 37	185 00	C.	-12 59	S.E. $\frac{1}{2}$ E.		- 3 11	-16 10			
			C.	-12 50	S.E. $\frac{3}{4}$ E.		- 3 16	-16 06			
			C.	- 9 24	S.E. by E. $\frac{3}{4}$ E.	-67 55	- 3 33	-12 57			
			C.	-12 04	s.e. by e.		- 3 22	-15 26			
	-47 11	184 24	CR.	-13 24	E.S.E.		- 3 36	-17 00			
	-47 33	184 54	CR.	-13 09	s.e. by e.		- 3 22	-16 31			
			CR.	-11 28	s.e. by e.		- 3 22	-14 50			
3.	-48 57	186 40	C.	-13 51	E. by s. $\frac{1}{2}$ S.	-69 05	- 4 07	-17 58			
			C.	-14 20	S.E. $\frac{3}{4}$ E.		- 3 40	-18 00			
5.	-49 33	189 22	C.	-13 32	E. $\frac{3}{4}$ S.		- 4 16	-17 48			
			C.	-15 03	E. $\frac{3}{4}$ S.		- 4 16	-19 19			
			C.	-13 40	E.S.E.	-69 40	- 4 13	-17 53			
			C.	-13 36	E. $\frac{1}{2}$ S.		- 4 13	-17 49			
	-49 33	188 54	CR.	-15 27	E. by s.		- 4 19	-19 46			
6.	-49 57	191 10	C.	-15 09	E. $\frac{1}{2}$ S.		- 4 15	-19 24			
			C.	-14 07	E. $\frac{1}{2}$ S.		- 4 15	-18 22			
			C.	-12 35	E. $\frac{3}{4}$ S.	-69 37	- 4 19	-16 54			
			C.	-12 44	E. $\frac{3}{4}$ S.		- 4 19	-17 03			
			C.	-13 55	E. $\frac{1}{2}$ S.		- 4 15	-18 10			
			C.	-13 49	E. $\frac{3}{4}$ S.		- 4 19	-18 08			
			CR.	-14 21	E. by s.		- 4 18	-18 39			
7.	-50 53	192 30	CR.	-15 02	s.e. by e.		- 3 56	-18 58			
			C.	-13 31	s.e. by E. $\frac{1}{2}$ E.	-69 50	- 4 06	-17 37			
			C.	-14 35	s.e. by e.		- 3 56	-18 31			
			C.	-15 00	S.E. $\frac{1}{2}$ E.		- 3 41	-18 41			
			C.	-14 59	s.e. by e.		- 3 56	-18 55			
			C.	-12 11	s.e. by E. $\frac{1}{2}$ E.		- 4 06	-16 17			
			CR.	-15 47	S.E. $\frac{1}{2}$ E.		- 3 41	-19 28			
			CR.	-12 14	E.S.E.		- 4 15	-16 29			
8.	-51 37	194 00	C.	-13 24	E. by s.	-70 11	- 4 25	-17 49			
	-51 53	195 17	C.	-12 57	E. by s.		- 4 25	-17 22			
			C.	-12 00	E. by s.		- 4 25	-16 25			
			C.	-11 26	E.S.E.		- 4 19	-15 45			
			C.	-12 15	E.S.E.		- 4 19	-16 34			
			C.	-11 50	E.S.E.		- 4 19	-16 09			
			C.	-13 02	E. by s.		- 4 25	-17 27			
			C.	-11 59	E. by s.		- 4 25	-16 24			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Dec. 9.	52° 27'	198° 14'	CR.	15° 16'	E.S.E.	-70 15	-4° 20'	-19° 36'	+1 30	-14 54	
12.	53 03	204 50	C.	12 10	E.S.E.		-4 20	-16 30			
			C.	11 33	S.E. by E. $\frac{3}{4}$ E.		-4 15	-15 58			
			C.	10 32	E. by S. $\frac{3}{4}$ S.		-4 23	-14 55			
			C.	10 52	E. by S. $\frac{3}{4}$ S.		-4 23	-15 15			
			C.	11 00	E.S.E.		-4 20	-15 20			
	53 18	205 46	C.	11 32	E.S.E.		-4 20	-15 52			
			C.	12 32	E.S.E.		-4 20	-16 52			
	53 06	205 24	CR.	12 11	E.S.E.		-4 20	-16 31			
			CR.	12 31	S.E. by E.		-4 01	-16 32			
	53 21	205 24	CR.	12 42	E.S.E.	-72 00	-4 20	-17 02	+1 30	-15 14	
14.	56 18	211 30	C.	13 27	S.E. $\frac{1}{4}$ E.		-3 57	-17 24			
			C.	12 37	S.E. $\frac{1}{4}$ E.		-4 13	-16 50			
			C.	13 57	S.E.		-3 49	-17 46			
			C.	13 54	S.E. $\frac{1}{2}$ S.		-3 26	-17 20			
	56 24	211 45	C.	12 24	E.		-4 43	-17 07			
			C.	12 01	E. $\frac{1}{4}$ N.		-4 35	-16 36			
			C.	21 03	S.W. $\frac{1}{4}$ W.		+3 57	-17 06			
			C.	13 05	N.E. $\frac{1}{4}$ N.		-2 44	-15 49			
	56 10	211 37	CR.	13 15	S.E. by S.		-3 03	-16 18			
			CR.	12 34	S.E. by S.	-72 30	-3 03	-15 37	+1 30	-15 14	
			CR.	11 19	S.E. by S.		-3 03	-14 22			
	56 29	211 50	CR.	14 50	S.E. by S.		-3 03	-17 53			
			CR.	14 52	S.S.E.		-2 09	-17 01			
			CR.	13 15	S.E.		-3 49	-17 04			
15.	56 55	212 00	C.	14 51	S.S.E. $\frac{1}{2}$ E.		-2 40	-17 31			
			C.	13 35	S.E. $\frac{1}{2}$ S.		-3 31	-17 06			
			C.	13 48	S.E. $\frac{3}{4}$ S.		-3 20	-17 08			
			C.	13 42	S.E. $\frac{3}{4}$ S.		-3 20	-17 02			
	57 09	212 26	C.	15 01	S.S.E.		-2 12	-17 13			
			C.	13 59	S.S.E.	-73 55	-2 12	-16 11	+1 30	-17 34	
			C.	13 30	S.S.E. $\frac{1}{4}$ E.		-2 25	-15 55			
			CR.	13 39	S.S.E.		-2 12	-15 51			
			CR.	14 43	S.S.E.		-2 12	-16 55			
			CR.	14 15	S.S.E.		-2 12	-16 27			
16.	58 21	213 00	C.	16 32	S. by E. $\frac{3}{4}$ E.		-2 06	-18 38			
			C.	17 39	S. by E. $\frac{1}{4}$ E.		-1 31	-19 10			
			C.	15 52	S.S.E.		-2 23	-18 15			
			C.	16 11	S. by E. $\frac{3}{4}$ E.		-2 06	-18 17			
			C.	16 05	S.S.E.		-2 23	-18 28			
			C.	15 42	S.S.E.	-75 40	-2 23	-18 05	+1 30	-20 03	
			CR.	15 47	S.S.E.		-2 23	-18 10			
			CR.	18 43	S.S.E.		-2 23	-21 06			
			CR.	19 07	S.S.E.		-2 23	-21 30			
17.	60 28	213 40	CR.	15 27	S.S.E.		-2 38	-18 05			
18.	62 53	212 48	C.	22 22	S. by W.	-76 50	+1 29	-20 53			
			C.	24 19	S. $\frac{1}{2}$ W.		+0 44	-23 35			
			C.	20 41	S. by E. $\frac{1}{4}$ E.		-1 52	-22 33			
			C.	21 10	S. $\frac{1}{2}$ E.		-0 44	-21 54			
	62 56	212 00	C.	28 15	S.W. by W.		+5 54	-22 21			
			C.	27 18	S.W. by W.		+5 54	-21 24			
			C.	27 54	S.W. $\frac{3}{4}$ W.		+5 44	-22 10			
			C.	28 15	S.W. by W.		+5 54	-22 21			
			C.	27 49	S.W. by W. $\frac{1}{2}$ W.		+6 11	-21 38			
			C.	27 16	S.W.		+5 08	-22 08			
	63 01	211 30	C.	23 57	S.S.W. $\frac{1}{2}$ W.		+3 32	-20 25			
			C.	24 06	S.S.W.		+2 58	-21 08			
			C.	24 02	S.S.W.		+2 58	-21 04			
	62 56	212 00	CR.	26 48	S.W.		+5 08	-21 40			

Observations of Declination. (Continued.)

1841.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Dec. 19.	-63 16	210 00	C.	-28 20	S.S.W. $\frac{3}{4}$ W.	-77 36	+ 4 02	-24 18	+ 1 30	-20 56	
			C.	-26 10	S.S.W. $\frac{1}{4}$ W.		+ 3 27	-22 43			
			C.	-31 10	W. by S. $\frac{1}{2}$ S.		+ 6 54	-24 16			
			C.	-25 18	S. by W. $\frac{1}{2}$ W.		+ 2 21	-22 57			
			C.	-23 47	S. $\frac{1}{4}$ W.		+ 0 23	-23 24			
			C.	-21 21	S.		0 0	-21 21			
	-63 23	209 40	C.	-28 21	W.S.W.		+ 6 47	-21 34			
			C.	-29 18	S.W.		+ 5 25	-23 53			
			C.	-26 15	S.S.W. $\frac{1}{2}$ W.		+ 3 46	-22 29			
			C.	-25 04	S.S.W.		+ 3 08	-21 56			
			C.	-27 23	S.W. $\frac{1}{4}$ W.		+ 5 38	-21 45			
			CR.	-24 51	S.W. by S.		+ 4 20	-20 31			
	-63 17	210 14	CR.	-25 00	S. 18° W.		+ 2 35	-22 25			
			CR.	-27 16	S. 40° W.		+ 4 52	-22 24			
			CR.	-27 06	S.S.W.		+ 3 08	-23 58			
			CR.	-28 50	S. 78° W.		+ 7 02	-21 48			
			CR.	-26 45	S. 78° W.		+ 7 02	-19 43			
			C.	-22 59	S. by E. $\frac{1}{4}$ E.		- 2 04	-25 03			
21.	-64 48	206 10	C.	-22 36	S.S.E.		- 3 17	-25 53			
			C.	-25 09	S. $\frac{1}{4}$ W.		+ 0 25	-24 44			
			C.	-24 11	S. $\frac{3}{4}$ E.		- 1 15	-25 26			
			C.	-28 03	S.S.W.		+ 3 17	-24 46			
			C.	-23 49	S.		0 0	-23 49			
			C.	-26 53	S. by W. $\frac{1}{2}$ W.		+ 2 28	-24 25			
	-65 21	205 20	C.	-23 09	S. $\frac{1}{2}$ E.		- 0 50	-23 59			
			C.	-20 51	S. $\frac{1}{2}$ E.		- 0 50	-21 41			
			C.	-25 11	S.		0 0	-25 11			
			C.	-25 56	S.		0 0	-25 56			
			C.	-27 31	S. $\frac{3}{4}$ W.		+ 1 20	-26 11			
			CR.	-27 12	S. by W.		+ 1 48	-25 24			
22.	-65 58	204 00	CR.	-27 32	S.		0 0	-27 32			
			C.	-26 57	S. by W. $\frac{1}{2}$ W.		+ 2 42	-24 15			
			CR.	-31 30	S.S.W. $\frac{1}{2}$ W.		+ 4 19	-27 11			
			C.	-23 15	N.E. $\frac{1}{4}$ N.		- 5 26	-28 41			
			C.	-29 29	S.		0 0	-29 29			
			C.	-27 27	S. $\frac{1}{2}$ E.		- 0 57	-28 24			
	-66 10	203 37	C.	-27 10	S. $\frac{3}{4}$ E.		- 1 25	-28 35			
			C.	-28 02	S. $\frac{1}{4}$ E.		- 0 28	-28 30			
			C.	-29 38	S. by W.		+ 1 54	-27 44			
			CR.	-31 14	N.N.W.		+ 3 00	-28 14			
			C.	-34 06	S.W. $\frac{1}{4}$ S.		+ 6 14	-27 52			
			C.	-20 52	E.S.E.		- 8 14	-29 06			
1842.	-66 02	204 00	C.	-34 46	S.W. by W. $\frac{1}{2}$ W.		+ 7 58	-26 48			
			C.	-20 09	E. $\frac{1}{2}$ S.		- 8 32	-28 41			
			C.	-34 42	S.W. $\frac{1}{2}$ S.		+ 5 54	-28 48			
			C.	-35 52	W. by S.		+ 8 32	-27 20			
			C.	-23 47	S.E. by S.		- 5 13	-29 00			
			C.	-20 29	S.E. $\frac{3}{4}$ E.		- 7 18	-27 47			
	9.	-66 02	C.	-33 58	S.W. $\frac{3}{4}$ W.		+ 7 18	-26 40			
			C.	-21 37	S.E. $\frac{3}{4}$ E.		- 7 18	-28 55			
			C.	-33 55	S.W. $\frac{3}{4}$ W.		+ 7 18	-26 37			
			C.	-34 19	S.W. $\frac{3}{4}$ W.		+ 7 18	-27 01			
			C.	-20 34	S.E. $\frac{3}{4}$ E.		- 7 18	-27 52			
			CR.	-34 41	S.W.		+ 6 34	-28 07			
Jan. 6.	-66 10	203 37	CR.	-19 20	E.S.E.		- 8 14	-27 34			
			CR.	-34 20	S.W. $\frac{1}{2}$ W.		+ 7 03	-27 17			
			CR.	-19 35	E. $\frac{1}{2}$ S.		- 8 32	-28 07			
			CR.	-20 54	S.E. by E. $\frac{3}{4}$ E.		- 8 04	-28 58			

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Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decl- ination.	Remarks.		
	Lat.	Long.											
Jan. 10.	-65° 58'	203° 54'	C.	-19° 32'	E. by N.	-79 48	-8 13	-27 45	+1 07	-25 00			
			C.	-34 59	w. by s.		+8 31	-26 28					
			C.	-18 30	E. $\frac{1}{4}$ S.		-8 31	-27 01					
			C.	-33 40	s.w.byw. $\frac{1}{4}$ w.		+7 44	-25 56					
			C.	-34 14	s.w. $\frac{3}{4}$ w.		+7 20	-26 54					
			C.	-33 09	s.w. $\frac{1}{2}$ w.		+7 35	-25 34					
			C.	-32 30	s.w. $\frac{1}{2}$ s.		+7 02	-25 28					
			C.	-30 16	s.s.w. $\frac{1}{4}$ w.		+4 01	-26 15					
			C.	-33 04	s.w. by w.		+7 34	-25 30					
			C.	-32 47	w. by s.		+8 32	-24 15					
			C.	-31 04	s.s.w. $\frac{3}{4}$ w.		+4 48	-26 16					
			C.	-32 00	s.s.w. $\frac{3}{4}$ w.		+4 48	-27 12					
			CR.	-23 04	s.e. $\frac{1}{2}$ s.		-7 02	-30 06					
			CR.	-34 10	w.s.w.		+8 12	-25 58					
			CR.	-19 17	s.e.		-6 32	-25 49					
			CR.	-16 56	s.e. by E.		-7 34	-24 30					
			CR.	-19 00	E.S.E.	-79 48	-8 12	-27 12	+1 07				
			CR.	-19 31	E.S.E.		-8 12	-27 43					
			CR.	-18 33	E. by s.		-8 31	-27 04					
			CR.	-21 18	s.e.		-6 32	-27 50					
			CR.	-19 20	E. by N.		-8 13	-27 33					
			CR.	-18 52	E.S.E.		-8 12	-27 04					
11.	-65 57	203 40	C.	-28 13	N. $\frac{3}{4}$ w.		+1 09	-27 04					
			C.	-34 41	w. by s. $\frac{1}{2}$ s.		+8 21	-26 20					
			C.	-29 53	s. $\frac{1}{4}$ w.		+1 26	-28 27					
			C.	-30 13	s. by w. $\frac{1}{2}$ w.		+2 44	-27 29					
			CR.	-26 44	s.		0 0	-26 44					
			CR.	-26 45	s.		0 0	-26 45					
12.	-65 46	203 22	CR.	-35 16	s.w.		-79 48	+6 32			-28 44	+1 07	-26 24
			CR.	-38 22	s.w. by w.			+7 34			-30 48		
13.	-66 10	202 40	C.	-26 00	s. $\frac{1}{4}$ E.			-1 26			-27 26		
			C.	-23 36	s. by E.			-1 52			-25 28		
			CR.	-25 26	s.	0 0		-25 26					
14.	-66 00	202 30	C.	-26 13	s. by E. $\frac{1}{2}$ E.	-2 44		-28 57					
			C.	-28 28	s. $\frac{1}{2}$ w.	-0 55		-27 33					
			C.	-20 54	E.N.E.	-7 34		-28 28					
			C.	-20 30	N.E. by E.	-6 42		-27 12					
28.	-67 40	204 10	CR.	-30 54	s. $\frac{1}{2}$ w.	-80 34		+1 01	-29 53	+1 07	-28 19		
			CR.	-29 04	s. $\frac{3}{4}$ E.			-1 30	-30 34				
			C.	-31 48	s. $\frac{3}{4}$ w.			+1 30	-30 18				
			C.	-26 53	N. $\frac{1}{2}$ E.			-0 50	-27 43				
			C.	-33 38	N.W. $\frac{1}{4}$ N.			+5 52	-27 46				
			C.	-36 47	s.w. $\frac{1}{4}$ s.			+6 38	-30 09				
			C.	-35 19	s.w. by s.			+5 36	-29 43				
			C.	-34 15	s.s.w.		+3 53	-30 22					
			C.	-19 11	E. $\frac{3}{4}$ s.		-9 14	-28 25					
29.	-67 36	204 00	CR.	-21 47	E. by s.		-80 40	-9 20	-31 07			+1 07	-28 37
			CR.	-35 06	s.s.w. $\frac{1}{4}$ w.			+4 20	-30 46				
31.	-67 16	202 10	C.	-32 27	s.s.w.			+3 57	-28 30				
			C.	-26 24	s. by E. $\frac{1}{2}$ E.			-2 58	-29 22				
			C.	-31 53	s. $\frac{1}{2}$ w.			+1 02	-30 51				
			C.	-31 04	s. $\frac{3}{4}$ w.			+1 33	-29 31				
			C.	-29 03	s. $\frac{1}{2}$ w.			+1 02	-28 01				
			C.	-31 39	s. by w.	+2 01		-29 38					
			C.	-32 19	s. $\frac{3}{4}$ w.	+1 33		-30 46					
	-67 13	202 35	CR.	-34 04	s.s.w. $\frac{1}{4}$ w.	+4 20		-29 44					
			CR.	-32 40	s.s.w.	+3 57		-28 43					

Observations of Declination (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Feb. 1.	-67 20	201 40	C.	-27 52	S.S.E.	-80 45	-3 57	-31 49	+1 07	-28 33	Card R.
			C.	-34 23	N. 72° W.		+ 8 45	-25 38			
			C.	-26 02	S. 27° E.		- 4 51	-30 53			
			C.	-31 38	N. 25° W.		+ 3 46	-27 52			
			C.	-35 59	N. 50° W.		+ 6 50	-29 09			
			C.	-30 21	S. 5° E.		- 1 00	-31 21			
			C.	-30 44	S. 5° E.		- 1 00	-31 44			
			C.	-26 52	N. 15° E.		- 2 20	-29 12			
			C.	-30 20	N. 14° W.		+ 2 11	-28 09			
			CR.	-37 20	W.		+ 9 25	-27 55			
			CR.	-28 37	S.S.E.	- 3 57	-32 34				
2.	-67 46	200 12	CR.	-37 55	S.S.W.	+ 4 04	-33 51				
3.	-68 06	199 40	C.	-28 02	S.S.E. 1/2 E.	- 4 57	-32 59				
	-68 40	200 00	C.	-29 23	S.E.	- 7 22	-36 45				
			C.	-31 03	S.E. 3/4 E.	- 7 39	-38 42				
			C.	-28 10	S.E. 1/4 S.	- 6 36	-34 46				
			C.	-44 56	W. by S.	+ 9 42	-35 14				
			C.	-44 26	W.S.W.	+ 9 19	-35 07				
			C.	-43 50	W.S.W.	+ 9 19	-34 31				
			C.	-42 51	W. by S. 1/2 S.	+ 9 30	-33 21				
			C.	-42 07	W. by S.	+ 9 42	-32 25				
	-67 58	199 50	C.	-41 14	W. by S.	+ 9 42	-31 32				
			CR.	-26 59	S.S.E.	- 4 04	-31 03				
			CR.	-30 29	S.S.E.	- 4 04	-34 33				
4.	-68 52	199 40	C.	-40 55	N.W. 1/4 W.	+ 7 20	-33 35				
			C.	-38 40	N.W. 3/4 N.	+ 5 52	-32 48				
			C.	-38 46	N.W. 1/4 N.	+ 6 38	-32 08				
			C.	-34 27	N.W. 3/4 N.	+ 5 52	-28 35				
			C.	-36 02	N.N.W. 3/4 W.	+ 5 03	-30 59				
			C.	-40 17	S.W. by S.	+ 6 19	-33 58				
			C.	-38 50	S.S.W. 1/4 W.	+ 4 51	-33 59				
8.	-70 06	186 20	C.	-37 51	S. 3/4 E.	- 2 08	-39 59				
			C.	-37 00	S. by E. 3/4 E.	- 4 53	-41 53				
			C.	-37 30	S. 1/2 E.	- 1 25	-38 55				
			CR.	-37 06	S. 3/4 E.	- 2 08	-39 14				
9.	-70 40	185 40	C.	-53 35	W.	+14 43	-38 52				
	-70 36	185 10	C.	-57 49	W. 3/4 S.	+14 38	-43 11				
			C.	-55 20	W. 1/2 S.	+14 40	-40 40				
			C.	-54 51	W.	+14 43	-40 08				
			C.	-55 48	S. 85° W.	+14 41	-41 07				
			C.	-54 57	S. 85° W.	+14 40	-40 17				
			C.	-55 05	W. 3/4 S.	+14 38	-40 27				
			C.	-54 54	W. 3/4 S.	+14 38	-40 16				
			C.	-56 07	W.	+14 43	-41 24				
			C.	-53 58	N. 70° W.	+13 31	-40 27				
			C.	-55 06	S. 78° W.	+14 15	-40 51				
	-70 22	185 00	C.	-53 56	W.	+14 43	-39 13				
			C.	-53 02	W. by N.	+14 15	-38 47				
	-70 40	185 40	CR.	-51 03	W.N.W.	+13 16	-37 47				
			CR.	-52 21	W. by N.	+14 15	-38 06				
	-70 36	185 10	CR.	-49 34	W.	+14 43	-34 51				
			CR.	-56 21	W.	+14 43	-41 38				
			CR.	-56 14	W. 1/2 N.	+14 30	-41 44				
			CR.	-53 30	W.N.W.	+13 16	-40 14				

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Feb. 10.	-70 14	184 00	C.	- 53 45	w.	- 83 45	+14 07	-39 38	+1 30	-37 19	
			C.	- 51 09	s.w.by w. $\frac{3}{4}$ w.		+13 03	-38 06			
			C.	- 28 40	S.E. $\frac{1}{4}$ E.		-10 54	-39 34			
			C.	- 28 57	S.E. by E.		-12 05	-41 02			
			C.	- 29 12	S.E. by E.		-12 05	-41 17			
			C.	- 54 07	w. by s. $\frac{1}{2}$ s.		+13 42	-40 25			
			C.	- 52 41	w. $\frac{3}{4}$ s.		+14 04	-38 37			
			C.	- 52 44	w. by s.		+14 02	-38 42			
			C.	- 51 25	w. $\frac{1}{4}$ s.		+14 05	-37 20			
			C.	- 50 32	w. by s.		+14 02	-36 30			
			C.	- 50 33	w.N.W.		+12 43	-37 50			
			C.	- 37 01	N. $\frac{1}{2}$ E.		- 1 17	-38 18			
			C.	- 38 12	N. by w.		+ 2 34	-35 38			
			Cr.	- 29 28	S.E. by s.		- 8 17	-37 45			
			Cr.	- 28 15	S.E. $\frac{1}{2}$ E.		-11 17	-39 32			
			Cr.	- 53 43	w. $\frac{1}{2}$ s.		+14 05	-39 38			
			Cr.	- 54 05	w. by s.		+14 02	-40 03			
12.	-71 04	180 46	C.	- 30 39	S.E. $\frac{1}{4}$ s.	- 84 30	-11 16	-41 55	+1 30	-40 45	
			C.	- 29 45	S.E.		-11 53	-41 38			
			C.	- 31 59	S.E. by s.		- 9 24	-41 23			
			C.	- 32 18	S.E. $\frac{3}{4}$ s.		-10 00	-42 18			
14.	-73 14	181 08	Cr.	- 32 09	S.E.	- 86 00	-11 53	-44 02	+1 30	-51 48	
			C.	- 37 39	S. 42° E.		-15 24	-53 03			
16.	-75 04	173 20	Cr.	- 39 01	S.E. $\frac{1}{2}$ s.	- 87 00	-14 32	-53 33	+1 30	-76 03	
			C.	- 59 26	S.E. by s.		-18 03	-77 29			
17.	-76 04	176 00	C.	- 40 57	S.E. by E.	- 87 00	-27 15	-68 12	+1 30	-82 28	
			C.	- 56 12	E. $\frac{3}{4}$ N.		-30 03	-86 15			
			C.	- 56 34	N.E. by E.		-24 47	-81 21			
18.	-76 54	182 17	C.	- 58 13	N.E. $\frac{3}{4}$ E.	- 86 50	-23 47	-82 00	+1 30	-70 22	
			C.	- 80 43	N. $\frac{1}{4}$ E.		- 1 19	-82 02			
			C.	- 75 23	N. $\frac{1}{4}$ W.		+ 1 19	-74 04*			
			C.	- 74 51	S. 25° E.		-13 23	-88 14			
20.	-76 12	191 40	C.	- 75 01	N. by E. $\frac{1}{4}$ E.	- 85 55	- 6 36	-81 37	+1 30	-81 23	
			C.	- 58 32	N.E.		-15 00	-73 32			
			C.	- 51 19	N.E. by E. $\frac{1}{2}$ E.		-18 53	-70 12			
22.	-76 32	194 40	C.	- 72 15	S.S.E. $\frac{1}{4}$ E.	- 85 30	- 8 47	-81 02	+1 30	-88 01	
			C.	- 74 30	S.S.E.		- 7 54	-82 24			
			C.	- 72 24	S.E. by s.		-11 26	-83 50			
			C.	- 60 26	E.S.E.		-18 42	-79 08			
			C.	- 72 10	E.S.E.		-18 42	-90 52			
			C.	- 65 19	E.S.E.		-18 42	-84 01			
			C.	- 72 44	S.S.E. $\frac{1}{4}$ E.		- 8 47	-81 31			
23.	-78 00	198 32	C.	- 60 43	E. by s.	- 85 30	-19 36	-80 19	+1 30	-64 33	
			C.	- 110 25	w. by N. $\frac{3}{4}$ N.		+18 19	-92 06			
			C.	- 70 48	E. $\frac{1}{2}$ s.		-19 42	-90 30			
			C.	- 69 12	E. $\frac{1}{2}$ s.		-19 42	-88 54			
			C.	- 70 07	E. $\frac{1}{2}$ s.		-19 42	-89 49			
			C.	- 70 25	E. $\frac{1}{2}$ s.		-19 42	-90 07			
			C.	-108 56	w. $\frac{1}{2}$ N.		+19 33	-89 23			
			C.	-103 22	w.N.W.		+17 59	-85 23			
			Cr.	- 70 09	E. by s.		-19 46	-89 55			
			Cr.	- 95 35	N.W.		+12 05	-83 30			
24.	-77 32	200 00	C.	- 84 54	w. $\frac{1}{2}$ N.	- 85 00	+17 30	-67 24	+1 30	-38 26	
			C.	- 79 11	N. 75° W.		+16 57	-62 14			
25.	-74 31	193 50	Cr.	- 71 00	N.W.	- 84 00	+12 05	-58 55	+1 30	-37 40	
			Cr.	- 56 32	N. $\frac{1}{2}$ E.		- 1 38	-58 10			
			C.	- 56 04	w.		+14 43	-41 21			
28.	-71 00	184 10	C.	- 55 15	w. $\frac{1}{4}$ N.	- 84 00	+14 29	-40 46	+1 30	-38 26	
			Cr.	- 52 17	w. by s.		+14 37	-37 40			
	-70 54	183 50									

* Doubtful ; omitted in the mean.

Observations of Declination. (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Mar. 1.	-70° 10'	180° 20'	C.	-46° 03'	w. by N. $\frac{1}{2}$ N.	-83° 45'	+14° 23'	-31° 40'	+1° 30'	-31° 26'	
			C.	-48° 05'	w. N.W.		+13° 52'	-34° 13'			
2.	-67° 54'	183° 40'	CR.	-47° 46'	w. by N.	-82° 20'	+14° 52'	-32° 54'	+1° 30'	-28° 50'	
			C.	-26° 18'	N.N.E.		-4° 27'	-30° 45'			
3.	-68° 24'	183° 20'	C.	-24° 31'	N.E. by N.	-82° 00'	-6° 31'	-31° 02'	+1° 30'	-29° 46'	
			C.	-25° 00'	N. by E. $\frac{1}{2}$ E.		-3° 21'	-28° 21'			
3.	-67° 30'	185° 00'	CR.	-26° 47'	N.N.E.	-82° 00'	-4° 27'	-31° 14'	+1° 30'	-29° 46'	
			C.	-22° 20'	N.E. $\frac{3}{4}$ E.		-9° 04'	-31° 26'			
5.	-67° 19'	187° 25'	C.	-19° 15'	N.E. $\frac{1}{4}$ N.	-81° 10'	-7° 30'	-26° 45'	+1° 30'	-25° 02'	
			C.	-24° 24'	N.E. $\frac{1}{2}$ N.		-7° 04'	-31° 28'			
6.	-65° 10'	191° 46'	C.	-23° 27'	E.N.E.	-79° 30'	-10° 37'	-34° 04'	+1° 30'	-19° 41'	
			C.	-24° 07'	N.E.		-7° 56'	-32° 03'			
8.	-64° 56'	192° 24'	CR.	-25° 40'	N.N.E. $\frac{1}{2}$ E.	-77° 30'	-5° 12'	-30° 52'	+1° 30'	-19° 49'	
			CR.	-22° 50'	N.E. by E.		-9° 26'	-32° 16'			
9.	-61° 00'	199° 00'	C.	-25° 52'	N. $\frac{1}{2}$ W.	-76° 10'	+0° 57'	-24° 55'	+1° 30'	-17° 19'	
			CR.	-26° 54'	N. by W.		+1° 54'	-25° 00'			
10.	-60° 20'	205° 36'	C.	-24° 59'	N. by E.	-75° 15'	-1° 35'	-26° 34'	+1° 30'	-16° 03'	
			C.	-24° 14'	N. by E. $\frac{1}{2}$ E.		-2° 21'	-26° 35'			
12.	-60° 18'	212° 00'	CR.	-25° 43'	N.N.E.	-74° 15'	-3° 08'	-28° 51'	+1° 30'	-22° 46'	
			C.	-27° 15'	N.		0° 0'	-27° 15'			
13.	-60° 06'	215° 52'	C.	-20° 31'	N. $\frac{3}{4}$ E.	-73° 55'	-0° 58'	-21° 29'	+1° 30'	-20° 57'	
			C.	-22° 33'	N.		0° 0'	-22° 33'			
14.	-59° 12'	219° 18'	CR.	-18° 16'	N. by E.	-73° 05'	-1° 18'	-19° 34'	+1° 30'	-20° 48'	
			CR.	-22° 28'	N. by W.		+1° 18'	-21° 10'			
15.	-58° 50'	222° 00'	C.	-17° 27'	N.E.	-73° 00'	-4° 20'	-21° 47'	+1° 30'	-20° 48'	
			C.	-14° 35'	E.N.E.		-5° 55'	-20° 30'			
16.	-58° 58'	227° 00'	CR.	-17° 46'	N.E.	-70° 51'	-4° 20'	-22° 06'	+1° 30'	-24° 46'	
			CR.	-15° 00'	E.N.E.		-5° 55'	-20° 55'			
18.	-60° 18'	236° 30'	C.	-15° 04'	E. by N. $\frac{1}{2}$ N.	-70° 11'	-5° 45'	-20° 49'	+1° 30'	-24° 46'	
			C.	-14° 25'	E.N.E.		-5° 30'	-19° 55'			
22.	-58° 28'	251° 40'	C.	-13° 58'	E.N.E.	-70° 11'	-5° 30'	-19° 28'	+1° 30'	-24° 46'	
			CR.	-13° 39'	E.N.E.		-5° 30'	-19° 09'			
23.	-58° 36'	255° 20'	C.	-12° 51'	E. by N.	-70° 11'	-5° 34'	-18° 25'	+1° 30'	-24° 46'	
			C.	-12° 57'	E. by N.		-5° 34'	-18° 31'			
23.	-58° 36'	255° 20'	C.	-12° 59'	E. by N.	-70° 11'	-5° 34'	-18° 33'	+1° 30'	-24° 46'	
			C.	-11° 39'	E.N.E.		-5° 06'	-16° 45'			
23.	-58° 36'	255° 20'	CR.	-16° 30'	N.E.	-70° 11'	-3° 43'	-20° 13'	+1° 30'	-24° 46'	
			CR.	-16° 01'	N.E. by E.		-4° 29'	-20° 30'			
23.	-58° 36'	255° 20'	C.	-12° 10'	E. by N.	-70° 11'	-5° 26'	-17° 36'	+1° 30'	-24° 46'	
			C.	-13° 06'	E.N.E.		-4° 59'	-18° 05'			
23.	-58° 36'	255° 20'	C.	-10° 27'	E. by N.	-70° 11'	-5° 26'	-15° 53'	+1° 30'	-24° 46'	
			C.	-13° 12'	E. by N.		-5° 26'	-18° 38'			
23.	-58° 36'	255° 20'	CR.	-13° 00'	E. by S.	-70° 11'	-5° 31'	-18° 31'	+1° 30'	-24° 46'	
			C.	-18° 40'	E.		-5° 24'	-24° 04'			
23.	-58° 36'	255° 20'	C.	-15° 26'	E.	-70° 11'	-5° 24'	-20° 50'	+1° 30'	-24° 46'	
			CR.	-17° 03'	E.		-5° 24'	-22° 27'			
23.	-58° 36'	255° 20'	CR.	-17° 53'	E.N.E.	-70° 11'	-4° 25'	-22° 18'	+1° 30'	-24° 46'	
			C.	-18° 33'	E. by N.		-4° 29'	-23° 02'			
23.	-58° 36'	255° 20'	CR.	-20° 01'	E.	-70° 11'	-4° 45'	-24° 46'	+1° 30'	-24° 46'	
			CR.	-19° 58'	E. by N.		-4° 29'	-24° 27'			
23.	-58° 36'	255° 20'	CR.	-20° 22'	E. by N.	-70° 11'	-4° 29'	-24° 51'	+1° 30'	-24° 46'	
			CR.	-20° 41'	E. by N.		-4° 18'	-24° 59'			
23.	-58° 36'	255° 20'	C.	-24° 18'	S.S.E.	-70° 11'	-2° 07'	-26° 25'	+1° 30'	-24° 46'	
			C.	-23° 57'	S.E. $\frac{1}{2}$ E.		-4° 00'	-27° 57'			
23.	-58° 36'	255° 20'	C.	-24° 13'	E. by N.	-70° 11'	-4° 18'	-28° 31'	+1° 30'	-24° 46'	
			C.	-21° 04'	N.E. by E. $\frac{1}{2}$ E.		-3° 41'	-24° 45'			
23.	-58° 36'	255° 20'	C.	-22° 07'	E. by N. $\frac{1}{4}$ N.	-70° 11'	-4° 09'	-26° 16'	+1° 30'	-24° 46'	
			C.	-20° 43'	E. by N.		-4° 18'	-25° 01'			

Observations of Declination (Continued.)

1842.	Position.		Initials.	Declination observed.	Direction of ship's head.	Inclination.	Correc- tion for ship's at- traction.	Corrected Declination.	Correc- tion for index error.	True Decli- nation.	Remarks.
	Lat.	Long.									
Mar. 24.	-58 46	257 50	C.	-21 52	E. $\frac{3}{4}$ N.	-69 45	-4 15	-26 07	+1 30	-26 13	
			C.	-24 59	E. by N.		-4 11	-29 10			
			CR.	-23 41	E. by N.	-68 50	-4 11	-27 52	+1 30	-26 25	
			CR.	-27 53	E.N.E.		-3 38	-31 31			
25.	-58 54	262 48	C.	-23 47	E.N.E.	-67 40	-3 24	-27 11	+1 30	-26 08	
26.	-59 02	268 40	C.	-24 43	E. by N. $\frac{3}{4}$ N.		-3 29	-28 12			
			C.	-23 30	E. by N. $\frac{1}{2}$ N.	-67 00	-3 34	-27 04	+1 30	-27 13	
			C.	-25 31	N.E. by E. $\frac{3}{4}$ E.		-3 17	-28 48			
			CR.	-22 22	E.N.E.	-65 30	-3 24	-25 46	+1 30	-28 25	
			CR.	-25 51	N.E.		-2 24	-28 15			
			CR.	-22 29	E.	-64 50	-4 01	-26 30	+1 30	-27 08	
			C.	-25 45	E.N.E.		-3 16	-29 01			
27.	-59 04	272 20	C.	-26 39	E.N.E.	-63 40	-3 16	-29 55	+1 30	-28 25	
			CR.	-25 53	E.N.E.		-3 16	-29 09			
			CR.	-23 12	E.N.E.	-63 30	-3 16	-26 28	+1 30	-27 13	
			C.	-26 15	N.E. by E.		-2 35	-28 50			
28.	-58 56	275 50	C.	-27 37	N.E. by E.	-63 00	-2 35	-30 12	+1 30	-28 25	
			C.	-30 22	N. by E.		-0 33	-30 55			
	-58 54	276 40	C.	-29 25	N. by E.	-64 50	-0 33	-29 58	+1 30	-27 13	
			C.	-27 06	N.E. by E.		-2 35	-29 41			
			C.	-27 54	N.E. by E.	-63 40	-2 35	-30 29	+1 30	-28 25	
			CR.	-26 44	N.E. by E.		-2 35	-29 19			
29.	-58 22	279 30	C.	-24 53	N.E. by E.	-63 00	-2 30	-27 23	+1 30	-27 13	
			C.	-25 19	N.E. by E.		-2 30	-27 49			
	-58 20	280 00	C.	-31 06	N. by W.	-63 00	+0 31	-30 35	+1 30	-26 49	
			C.	-29 30	N. by E.		-0 31	-30 01			
			C.	-24 59	E.	-63 00	-3 30	-28 29	+1 30	-27 13	
			C.	27 46	N.E. $\frac{1}{2}$ E.		-2 15	-30 01			
			C.	-25 09	E.N.E.	-63 00	-2 55	-28 04	+1 30	-28 25	
			C.	-25 27	E.N.E.		-2 55	-28 22			
	-58 22	279 30	CR.	-27 45	N.	-63 00	0 0	-27 45	+1 30	-27 13	
			CR.	-25 08	E.		-3 30	-28 38			
30.	-58 30	282 00	C.	-24 51	N.E. by E. $\frac{1}{2}$ E.	-63 00	-2 35	-27 26	+1 30	-26 49	
			C.	-24 19	E.N.E.		-2 47	-27 06			
			C.	-25 46	N.E. $\frac{1}{2}$ E.	-63 00	-2 08	-27 54	+1 30	-27 13	
			C.	-25 46	N.E. by E.		-2 23	-28 09			
			C.	-25 16	N.E. by E.	-63 00	-2 23	-27 39	+1 30	-26 49	
			C.	-25 49	N.E. by E.		-2 23	-28 12			
			C.	-27 18	N.E. by E.	-63 00	-2 23	-29 41	+1 30	-28 25	
			C.	-25 46	N.E. by E.		-2 23	-28 09			
			C.	-26 05	N.E. by E. $\frac{1}{2}$ E.	-63 00	-2 35	-28 40	+1 30	-27 13	
			C.	-27 48	N.E. by E.		-2 23	-30 11			
	-58 30	282 30	C.	-25 46	E. by N.	-63 00	-3 02	-28 48	+1 30	-26 13	
			C.	-25 43	E. by N.		-3 02	-28 45			
			CR.	-25 04	E.N.E.	-63 00	-2 41	-27 45	+1 30	-26 13	
			CR.	-25 25	E. by N.		-3 02	-28 27			
			CR.	-23 46	E.N.E.	-63 00	-2 41	-26 27	+1 30	-20 26	
			C.	-26 49	N.E. by N.		-1 23	-28 12			
31.	-58 26	285 08	C.	-25 59	N.E. by N.	-61 13	-1 23	-27 22	+1 30	-20 26	
			CR.	-24 06	N.E.		-1 50	-25 26			
April 1.	-58 30	285 35	C.	-25 30	N.E. by N.	-59 00	-1 16	-26 46	+1 30	-25 16	
			CR.	-21 46	N.E.		-1 30	-23 16			
3.	-56 46	294 30	C.	-19 07	N.E.	-53 54	-1 30	-20 37	+1 30	-18 25	
			CR.	-21 21	N. by E.		-0 17	-21 38			
5.	-52 22	301 00	C.	-18 20	N. by E.	-52 30	-0 17	-18 38	+1 30	-20 26	
			C.	-20 32	N. by E.		-0 17	-20 49			
6.	-51 50	301 35	C.	-19 07	N.N.W.	-52 30	+0 30	-18 37			

Observations of the INCLINATION made on board Her Majesty's Ship Erebus, with
Needle R. F. 5, between April 1841 and August 1842.

Observers Captain Sir JAMES CLARK ROSS and Lieutenant ALEXANDER SMITH, R.N.

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
April 19.	Hobarton, Magnetic Observatory. -42 52 147 24		Direct.	-70 18.4	Observed on shore.	-6	-70 32 -70 32	R. F. 4, used as deflector.
			S.	-70 38.2					
			N.	-70 30.9					
			N.S.	-70 22.1					
20.			Direct.*	-70 26.3					
			N.S. at 24° 44'.	-70 30.6					
			S. at 56° 20'.	-70 02.7					
			N. at 53° 02'.	-70 12.5					
24.			Direct.	-70 24.3					R. F. 3, used as deflector.
			S.	-70 34.4					
			N.	-70 41.6					
			S. at 38° 11'.	-70 32.7					
			N. at 43° 54'.	-70 29.9					
June 29.	At anchor.		Direct.	-71 38.9	N.	+81	-7	-70 31 } -70 35 } -70 52 } -70 42 } -70 45 } -70 42 } -70 43 } -70 44 } -70 34 } -70 46 } -70 35 } -70 39 } -70 32 } -70 34 } -70 35 } -70 39 } -70 32 } -70 34 } -70 35 } -70 39 } -70 39 }	R. F. 4, used as deflector.
			S.	-71 50.7	N.	+81	-7		
			Direct.	-71 40.5	N.N.E.	+78	-7		
			S.	-71 52.5	N.N.E.	+78	-7		
			Direct.	-71 38.0	N.E.	+67	-7		
			S.	-71 57.3	N.E.	+67	-7		
			Direct.	-71 13.4	E.N.E.	+47	-6		
			S.	-71 31.8	E.N.E.	+47	-7		
			Direct.	-70 55.5	E.	+20	-6		
			S.	-71 02.4	E.	+20	-6		
			Direct.	-70 21.5	E.S.E.	-12	-6		
			S.	-70 25.8	E.S.E.	-12	-6		
			Direct.	-69 53.6	S.E.	-43	-6		
			S.	-69 55.1	S.E.	-43	-6		
			Direct.	-69 17.0	S.S.E.	-67	-5		
			S.	-69 46.4	S.S.E.	-67	-6		
			Direct.	-69 03.3	S.	-80	-5		
			S.	-69 14.9	S.	-80	-5		
			Direct.	-69 26.5	S.S.W.	-67	-6		
			S.	-69 40.3	S.S.W.	-67	-6		
			Direct.	-69 41.0	S.W.	-43	-6		
			S.	-69 51.4	S.W.	-43	-6		
			Direct.	-70 14.8	W.S.W.	-12	-6		
			S.	-70 26.6	W.S.W.	-12	-6		
			Direct.	-70 42.2	W.	+20	-6		
			S.	-70 49.1	W.	+20	-6		
			Direct.	-71 10.4	W.N.W.	+47	-6		
			S.	-71 19.3	W.N.W.	+47	-7		
			Direct.	-71 32.2	N.W.	+67	-7		
			S.	-71 37.8	N.W.	+67	-7		
			Direct.	-71 42.4	N.N.W.	+78	-7		
			S.	-71 58.3	N.N.W.	+78	-7		
			Direct.	-71 42.5	N.	+81	-7		
			S.†	-72 03.3	N.	+81	-7		

* Observed on shore;
face west. { Direct. -71 40.6
S. -71 09.6
N. -71 20.1
N.S. -71 10.8

† Face west. { Direct. -73 07.8 } Head north.
S. -72 34.9

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
July 7.	° '	° '	Direct.	-70 16·1	S.E. $\frac{1}{2}$ E.	-37	-6	° ' ° '	
			S.	-70 03·4	S.E. $\frac{1}{2}$ E.	-37	-6		
			N.	-70 05·4	S.E. $\frac{1}{2}$ E.	-37	-6		
			N.S.	-70 12·0	S.E. $\frac{1}{2}$ E.	-37	-6		
			Direct.	-70 18·9	S.E. $\frac{1}{2}$ E.	-37	-6		
8.	-43 00	148 28	Direct.	-71 27·3	N.N.E.	+78	-7		
			S.	-71 43·2	N.N.E.	+78	-7		
			N.	-71 36·7	N.N.E.	+78	-7		
			N.S.	-71 39·1	N.N.E.	+78	-7		
			Direct.	-71 32·2	N.N.E.	+78	-7		
9.	-42 13	149 25	Direct.	-70 46·5	N.N.W.	+77	-6		
			S.	-70 56·3	N.N.W.	+77	-6		
			N.	-71 12·6	N.N.W.	+77	-7		
			N.S.	-70 30·2	N.N.W.	+77	-6		
			Direct.	-70 36·5	N.N.W.	+77	-6		
10.	-40 55	149 12	Direct.	-69 52·4	N. by w.	+76	-6		
			S.	-69 53·7	N. by w.	+76	-6		
			N.	-69 47·1	N. by w.	+76	-6		
			N.S.	-69 49·2	N. by w.	+76	-6		
11.	-37 50	150 22	Direct.	-67 47·8	N. by w.	+72	-5		
			N.	-67 53·9	N. by w.	+72	-5		
			N.S.	-67 28·9	N. by w.	+72	-5		
			Direct.	-67 40·4	N. by w.	+72	-5		
12.	-37 21	151 33	Direct.	-67 01·6	N.E.	+62	-4		
			S.	-66 58·0	N.E.	+62	-4		
			N.	-67 03·3	N.E.	+62	-4		
			N.S.	-66 49·4	N.E.	+62	-4		
			Direct.	-67 04·8	N.E.	+62	-4		
13.	-36 01	151 48	Direct.	-66 19·0	N.W. by N.	+64	-4		
			N.	-65 57·0	N.W. by N.	+64	-4		
			N.S.	-65 52·9	N.W. by N.	+64	-4		
			Direct.	-66 08·5	N.W. by N.	+64	-4		
14.	-33 52	151 21	Direct.	-64 05·9	N.	+67	-3		
			S.	-64 20·3	N.	+67	-3		
			N.	-64 05·4	N.	+67	-3		
			N.S.	-64 00·8	N.	+67	-3		
			Direct.	-65 03·8	N.	+67	-3		
14.	-33 51	151 20	Direct.	-63 49·0	N. by w.	+66	-3		
			Direct.	-63 37·9	N.W.	+58	-3		
			Direct.	-62 05·5	S.W. by w.	-17	-2		
			Direct.	-62 03·1	S.E.	-35	-2		
			Direct.	-61 52·5	S.S.W. $\frac{1}{2}$ W.	-51	-2		
31.			Direct.	-63 11·9	W.	+25	-2		
	At anchor.		S.	-63 24·0	W.	+25	-3		
	-33 51	151 17	Direct.	-62 19·1	W.S.W.	- 2	-2		
			Direct.	-61 12·6	S.	-63	-2		
			S.	-61 26·1	S.	-63	-2		
			Direct.	-61 31·5	S.S.W.	-53	-2		
			S.	-61 47·5	S.S.W.	-53	-2		
Aug. 3.			Direct.	-63 30·1	N.E.	+58	-3		
			S.	-63 40·9	N.E.	+58	-3		

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
July 15.	Garden Island, Sydney. -33 51 151 17		Direct.	-62° 40' 8"	Observed on shore.		-2		
			S.	-62 50.1			-2		
			N.	-62 49.9			-2		
			N.S.	-62 42.9			-2		
Aug. 4.			Direct.	-62 45.9†			-2	-62 48	-62 48
			S.	-62 50.1			-2		
			N.	-62 50.2			-2		
			N.S.	-62 40.3			-2		
5.			Direct.	-63 40.6	N.N.E.	+64	-3	-62 40	
			Direct.	-63 03.4	E. by N.	+35	-2		
			Direct.	-63 06.5	E. by N.	+35	-2		
			S.	-63 22.6	E. by N.	+35	-3	-62 43	-62 42
			N.	-63 26.1	E. by N.	+35	-3		Running out of harbour.
			N.S.	-63 23.0	E. by N.	+35	-3		
6.	-33 52 154 07		Direct.	-63 09.8	E. by N.	+35	-2		
			Direct.	-63 09.3	E. by N.	+35	-2		
			S.	-63 38.9	E. by N.	+35	-3		
			N.	-63 11.4	E. by N.	+35	-2	-62 47	-62 47
			N.S.	-63 30.2	E. by N.	+35	-3		Much motion.
			Direct.	-63 03.3	E. by N.	+35	-2		
7.			Direct.	-62 47.0	E. by N.	+35	-2		
			S.	-62 43.3	E. by N.	+35	-2		
			N.	-62 35.7	E. by N.	+35	-2	-62 07	-62 07
			N.S.	-62 31.5	E. by N.	+35	-2		Much motion.
			Direct.	-62 42.7	E. by N.	+35	-2		
8.			Direct.	-62 04.4	E. by N.	+35	-2		
	-33 27 160 43		S.	-61 59.5	E. by N.	+35	-2		
			N.	-61 55.1	E. by N.	+35	-2	-61 30	-61 30
			N.S.	-62 13.7	E. by N.	+35	-2		
			Direct.	-62 02.0	E. by N.	+35	-2		
9.			Direct.	-61 02.5	E.	+26	-1		
			S.	-61 31.5	E.	+26	-2		
			N.	-61 14.6	E.	+26	-2	-60 48	-60 48
			N.S.	-61 18.4	E.	+26	-2		
			Direct.	-61 04.0	E. by N.	+35	-1		
10.			Direct.	-61 11.7	N.E.	+56	-1		
			S.	-61 06.7	N.E.	+56	-1	-60 06	-60 07
			N.	-60 45.7	N.E.	+56	-1		
	-33 22 167 40		N.S.	-61 03.9	N.E.	+56	-1	-60 08	
			Direct.	-60 33.2	E.	+26	-1		
11.			Direct.	-60 12.3	E. by N.	+35	-1		
			S.	-60 22.3	E. by N.	+35	-1		
			N.	-60 06.9	E. by N.	+35	-1	-59 39	-59 39
			N.S.	-60 15.0	E. by N.	+35	-1		
			Direct.	-60 11.0	E. by N.	+35	-1		
12.			Direct.	-59 44.4	E.N.E.	+43	-1		
			S.	-59 43.5	E.N.E.	+43	-1		
			N.	-59 38.7	E.N.E.	+43	-1	-59 04	-59 04
			N.S.	-59 54.7	E.N.E.	+43	-1		
			Direct.	-59 49.1	E.N.E.	+43	-1		

* Observed on shore; face west. { Direct. -63 53.3
S. -63 44.8
N. -63 33.1
N.S. -63 38.5

† Observed on shore; face west. { Direct. -63 51.7

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Aug. 13.	-32° 12'	170° 27'	Direct.	-58° 47.3	S.E. by E.	-12	0		
			S.	-58 30.2	S.E. by E.	-12	0	-58 33	-58 33
			N.	-58 09.7	S.E. by E.	-12	0		
			N.S.	-57 55.2	S.E. by E.	-12	0		
14.	-33 27	171 21	Direct.	-57 30.0	S.E. by E.	-12	+1		
15.	-33 55	171 54	Direct.	-58 49.5	E. ½ S.	+20	0		
			S.	-59 03.7	E. ½ S.	+20	0		
			N.	-59 02.9	E. ½ S.	+20	0	-58 24	-58 24
			N.S.	-58 59.8	E. ½ S.	+20	0		
			Direct.	-58 42.5	E. ½ S.	+20	0		
16.	-34 00	172 01	Direct.	-57 46.5	S.E. by E. ½ E.	-4	+1		
16.	-34 21	178 48	Direct.	-58 49.3	E.S.E.	+4	0		
17.	-34 29	173 36	Direct.	-58 26.0	E.S.E.	+4	0		
			S.	-58 42.5	E.S.E.	+4	0		
			N.	-58 02.7	E.S.E.	+4	0	-58 26	-58 26
			N.S.	-58 42.0	E.S.E.	+4	0		
			Direct.	-58 17.0	E.S.E.	+4	0		
			Direct.	-58 50.8	E.S.E.	+4	0		
23.	Bay of Islands.		Direct.	-59 26.4					
	-35 16	174 00	S.	-59 34.5					
			N.	-59 29.1					
			N.S.	-59 22.6					
Oct. 27.			Direct.	-59 28.2*	Observed on shore.	-1	-59 29	-59 29
			Direct.	-59 28.0†					
			S.	-59 43.2					
			N.	-59 31.9					
			N.S.	-59 26.2					
			Direct.	-59 28.3†					
20.	At anchor.		Direct.	-60 17.1	N.W. ½ N.	+54	-1		
			S.	-61 03.1	N.W. ½ N.	+54	-1	-59 49	
			Direct.	-58 31.7	S.	-57	0		
			S.	-59 05.6	S.	-57	0		
Nov. 23.	-35 15	174 39	Direct.	-59 25.0	E.S.E.	+1	-1	-59 25	-59 28
			Direct.	-59 37.7	E. by S.	+15	-1		
			Direct.	-59 30.7	E. by S.	+15	-1		
			S.	-59 23.8	E. by S.	+15	-1	-59 11	
			N.	-59 11.7	E. by S.	+15	-1		
			N.S.	-59 22.3	E. by S.	+15	-1		
24.	-36 27	177 34	Direct.	-59 50.0	E.S.E.	0	-1		
			Direct.	-59 56.2	E.S.E.	0	-1		
			S.	-59 48.2	E.S.E.	0	-1	-59 54	-59 54
			N.	-59 48.2	E.S.E.	0	-1		
			N.S.	-60 03.2	E.S.E.	0	-1		
25.	-38 17	179 51	Direct.	-59 55.3	S.E. by S.	-34	-1		
			S.	-59 34.4	S.E. by S.	-34	-1		
			N.	-60 02.2	S.E. by S.	-34	-1	-60 32	-60 34
			N.S.	-60 14.7	S.E. by S.	-34	-1		
			Direct.	-59 57.2	S.E. by S.	-34	-1		
			Direct.	-60 19.5	S.E.	-23	-1	-60 43	

* Observed on shore; face west. { Direct. -60° 33.0
S. -60 30.1
N. -60 28.4
N.S. -60 19.6
Direct. -60 31.9

† Observed on shore; face west. { Direct. -60° 30.1
S. -60 33.1
N. -60 40.4
N.S. -60 14.9
Direct. -60 32.0

‡ Observed on shore; face west. { Direct. -60° 29.0
S. -60 28.8
N. -60 19.1
N.S. -60 18.9
Direct. -60 28.8

Nov. 13.

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.	
						Ship's attraction.	Index.			
Nov. 25.	—38 54	181 12	Direct.	—61 13.0	E.S.E.	0	—2	—61 15	A heavy sea and very much motion.	
26.	—39 01	182 12	Direct.	—61 27.8	E. by s.	+14	—2	—61 15		
			S.	—61 04.7	E. by s.	+14	—1			
			N.	—61 43.4	E. by s.	+14	—2			
			N.S.	—61 29.7	E. by s.	+14	—2			
			Direct.	—61 30.4	E. by s.	+14	—2	—61 34		
27.	—39 18	182 58	Direct.	—61 02.9	s.	—50	—1			
			S.	—61 01.5	s.	—50	—1			
			N.	—61 16.4	s.	—50	—2			
			N.S.	—61 11.1	s.	—50	—1	—61 57		
			Direct.	—60 59.6	s.	—50	—1			
28.	—40 47	183 03	Direct.	—62 03.3	S.E. by E.	—10	—2			
			S.	—62 35.5	S.E. by E.	—10	—2			—62 21
			N.	—61 59.9	S.E. by E.	—10	—2			
			N.S.	—61 59.8	S.E. by E.	—10	—2			
			Direct.	—61 29.8	s. by E.	—49	—2			
29.	—41 49	183 41	Direct.	—62 29.9	s. by E.	—49	—2	—62 21		—63 28
			S.	—62 34.4	s. by E.	—49	—2			
			N.	—62 43.2	s. by E.	—49	—2			
			N.S.	—62 47.0	s. by E.	—49	—2			
			Direct.	—62 32.0	s. by E.	—49	—2	—64 44		—64 44
30.	—43 32	183 03	Direct.	—63 38.3	S. ½ W.	—52	—3			
			S.	—64 16.6	S. ½ W.	—52	—3			
			N.	—63 48.1	S. ½ W.	—52	—3			
			N.S.	—63 43.9	S. ½ W.	—52	—3	—66 35		—66 35
Dec. 1.	—45 40	183 20	Direct.	—66 08.5	S.E. by E.	—15	—4			
			S.	—66 34.2	S.E. by E.	—15	—4			
			N.	—66 03.2	S.E. by E.	—15	—4			
			N.S.	—66 29.2	S.E. by E.	—15	—4	—67 56	—67 56	
			Direct.	—66 05.3	S.E. by E.	—15	—4			
2.	—47 19	184 40	Direct.	—67 41.2	S.E. by E. ½ E.	—11	—5			
			S.	—67 34.0	S.E. by E. ½ E.	—11	—5			
			N.	—67 34.0	S.E. by E. ½ E.	—11	—5	—69 01	—69 05	
			N.S.	—67 32.5	S.E. by E. ½ E.	—11	—5			
			Direct.	—67 56.0	S.E. by E. ½ E.	—11	—5			
3.	—48 43	186 30	Direct.	—68 51.5	E.S.E.	—5	—5			
			Direct.	—68 46.1	S.E. by E.	—20	—5	—69 08	—69 05	
			S.	—68 38.6	S.E. by E.	—20	—5			
			N.	—68 43.6	S.E. by E.	—20	—5			
			N.S.	—68 41.6	E.S.E.	—5	—5			
			Direct.	—68 49.7	S.E. by E.	—20	—5	—68 52	—69 15	
4.	—49 20	187 41	Direct.	—69 32.4	E. by s.	+6	—6			
			S.	—70 10.2	E. by s.	+6	—6			
			N.	—69 48.6	E. by s.	+6	—6			
			N.S.	—69 50.0	E. by s.	+6	—6	—69 41	—69 41	
			Direct.	—69 24.4	E. by s.	+6	—6			
5.	—49 27	189 13	Direct.	—69 36.0	E. by s.	+6	—6			
			S.	—69 47.2	E. by s.	+6	—6			
			N.	—69 32.9	E. by s.	+6	—6	—69 34	—69 43	
			N.S.	—69 28.2	E. by s.	+6	—6			
6.	—50 00	191 00	Direct.	—69 17.5	E. by s.	+6	—6			
			S.	—69 51.7	E. by s.	+6	—6			
			N.	—69 37.0	E. by s.	+6	—6	—69 34	—69 43	
			N.S.	—69 38.2	E. by s.	+6	—6			
	—50 48	192 20	Direct.	—69 28.5	E. by s.	+6	—6			

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 7.	—50 48	192 20	Direct.	—69 18.8	S.E. by E.	—21	—6	—69 58	—69 43
			S.	—70 01.5	S.E. by E.	—21	—6		
			N.	—69 17.2	S.E. by E.	—21	—6		
			N.S.	—69 04.5	S.E. $\frac{1}{2}$ E.	—26	—5		
8.	—51 34	194 29	Direct.	—69 17.0	S.E. $\frac{1}{2}$ E.	—26	—6	—69 42	
			Direct.	—70 04.1	E. by S.	+ 6	—6		
			S.	—70 33.6	E. by S.	+ 6	—6		
			N.	—70 12.3	E. by S.	+ 6	—6		
9.	—52 02	197 53	N.S.	—69 53.8	E. by S.	+ 6	—6	—70 10	
			Direct.	—70 06.0	E. by S.	+ 6	—6		
			Direct.	—70 19.0	E. by S.	+ 6	—6		
			S.	—70 49.0	E. by S.	+ 6	—6		
10.	—53 01	202 11	N.	—70 29.1	E. by S.	+ 6	—6	—70 21	
			N.S.	—70 11.2	E. by S.	+ 6	—6		
			Direct.	—70 17.0	E. by S.	+ 6	—6		
			Direct.	—70 18.0	E. by S.	+ 6	—6		
11.	—52 48	203 50	Direct.	—71 08.0	E. $\frac{1}{2}$ N.	+25	—6	—70 32	
			S.	—71 26.2	E. $\frac{1}{2}$ N.	+25	—7		
			N.	—71 13.0	E. $\frac{1}{2}$ N.	+25	—7		
			N.S.	—71 09.7	E. $\frac{1}{2}$ N.	+25	—6		
12.	—53 01	205 08	Direct.	—71 05.0	E. $\frac{1}{2}$ N.	+25	—6	—70 44	Ship unsteady ; much motion.
			Direct.	—70 35.9	E.	+19	—6		
			S.	—70 53.5	E.	+19	—6		
			N.	—70 54.6	E.	+19	—6		
13.	—54 55	209 30	N.S.	—71 11.2	E.	+19	—6	—70 35	
			Direct.	—70 30.4	E.	+19	—6		
			Direct.	—69 56.8	E.S.E.	— 6	—6		
			S.	—70 11.6	E.S.E.	— 6	—6		
14.	—55 08	210 04	N.	—70 00.7	E.S.E.	— 6	—6	—70 10	—70 10
			N.S.	—69 42.3	E.S.E.	— 6	—6		
			Direct.	—69 56.5	E.S.E.	— 6	—6		
			Direct.	—70 01.5	E.S.E.	— 6	—6		
15.	—55 20	210 28	Direct.	—70 21.0	S.E. by E. $\frac{1}{2}$ E.	—14	—6	—70 54	
			S.	—70 55.7	S.E. by E. $\frac{1}{2}$ E.	—14	—6		
			N.	—70 30.0	S.E. by E. $\frac{1}{2}$ E.	—14	—6		
			N.S.	—70 44.5	S.E. by E. $\frac{1}{2}$ E.	—14	—6		
16.	—55 20	211 52	Direct.	—70 23.5	S.E. by E. $\frac{1}{2}$ E.	—14	—6	—70 58	
			Direct.	—70 26.5	S.E. by E. $\frac{1}{2}$ E.	—14	—6		
			S.	—71 04.2	S.E. by E. $\frac{1}{2}$ E.	—14	—6		
			N.	—70 34.7	S.E. by E. $\frac{1}{2}$ E.	—14	—6		
17.	—55 20	211 52	N.S.	—71 03.0	S.E. by E. $\frac{1}{2}$ E.	—14	—6	—71 13	
			Direct.	—70 27.5	S.E. by E. $\frac{1}{2}$ E.	—14	—6		
			Direct.	—70 35.5	S.E. by E. $\frac{1}{2}$ E.	—15	—6		
			S.	—71 13.5	S.E. by E. $\frac{1}{2}$ E.	—15	—7		
18.	—56 20	211 52	N.	—70 48.7	S.E. by E. $\frac{1}{2}$ E.	—15	—6	—71 11	
			N.S.	—70 53.0	S.E. by E. $\frac{1}{2}$ E.	—15	—6		
			Direct.	—70 39.0	S.E. by E. $\frac{1}{2}$ E.	—15	—6		
			Direct.	—70 38.0	S.E. by S.	—47	—6		
19.	—56 20	211 52	S.	—71 23.9	S.E. by S.	—47	—7	—71 28	
			N.	—71 01.3	S.E. by S.	—47	—6		
			N.S.	—70 36.2	S.E. by S.	—47	—6		
			Direct.	—70 43.0	S.E. by S.	—47	—6		

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 14.	—55 55	211 38	Direct.	—70 51.5	S.E. by S.	—48	—6	—72 03	
			S.	—71 59.2	S.E. by S.	—48	—7		
			N.	—71 00.7	S.E. by S.	—48	—6		
			N.S.	—71 04.0	S.E. by S.	—48	—6		
15.	—56 55	212 34	Direct.	—70 50.3	S.E. by S.	—48	—6	—72 18	
			Direct.	—71 09.5	S.S.E.	—58	—6		
			S.	—72 36.0	S.S.E.	—58	—7		
			N.	—71 18.2	S.S.E.	—58	—7		
	—56 06	212 20	N.S.	—71 14.5	S.S.E.	—58	—7	—72 33	
			Direct.	—71 07.5	S.S.E.	—58	—6		
			Direct.	—71 37.1	S.E. by S.	—48	—7		
			Direct.	—71 48.0	E.S.E.	—9	—7		
			S.	—72 14.8	E.S.E.	—9	—7	—72 08	
			N.	—71 30.0	E.S.E.	—9	—7		
			N.S.	—71 31.0	E.S.E.	—9	—7		
16.	—58 29	213 11	Direct.	—71 50.0	E.S.E.	—9	—7	—73 40	
			Direct.	—72 41.5	S.S.E.	—60	—7		
			S.	—72 49.3	S.S.E.	—60	—7		
			N.	—72 25.6	S.S.E.	—60	—7		
	—58 36	213 17	N.S.	—72 33.8	S.S.E.	—60	—7	—73 45	
			Direct.	—72 09.1	S.S.E.	—60	—7		
			Direct.	—72 38.0	S.S.E.	—60	—7		
			Direct.	—72 41.7	S.S.E.	—61	—7		
	—58 52	213 22	S.	—72 47.0	S.S.E.	—61	—7	—73 52	
			N.	—72 40.0	S.S.E.	—61	—7		
			N.S.	—72 44.6	S.S.E.	—61	—7		
			Direct.	—72 47.7	S.S.E.	—61	—7		
17.	—61 03	213 57	Direct.	—74 02.5	S.S.E.	—62	—8	—75 15	
			S.	—74 27.7	S.S.E.	—62	—8		
			N.	—73 50.0	S.S.E.	—62	—8		
			N.S.	—73 58.7	S.S.E.	—62	—8		
	—61 37	213 57	Direct.	—74 04.6	S.S.E.	—62	—8	—75 32	
			Direct.	—74 08.0	S.S.E.	—62	—8		
			Direct.	—74 32.0	S. by E.	—69	—8		
			S.	—74 53.0	S. by E.	—69	—8		
			N.	—74 07.0	S. by E.	—69	—8	—75 47	
			N.S.	—74 25.0	S. by E.	—69	—8		
			Direct.	—74 33.0	S. by E.	—69	—8		
18.	—62 40	212 53	Direct.	—75 01.5	S.	—72	—8	—76 38	
			S.	—75 20.3	S.	—72	—9		
			N.	—75 10.5	S.	—72	—8		
			N.S.	—75 47.0	S.	—72	—9		
	—63 23	210 02	Direct.	—75 07.8	S.	—72	—8	—76 36	
			Direct.	—75 10.0	S. by W.	—70	—8		
			Direct.	—75 18.0	S. by W.	—70	—9		
			Direct.	—76 17.0	S.S.W.	—63	—9		
	—63 23	210 02	S.	—76 23.3	S.S.W.	—63	—9	—77 26 —77 26	
			N.	—75 54.0	S.S.W.	—63	—9		
			N.S.	—76 24.0	S.S.W.	—63	—9		
			Direct.	—76 12.6	S.S.W.	—63	—9		
19.	—63 23	210 02	Direct.	—77 03.3	Observed on Ice.	—10	—77 25 —77 25	
			S.	—77 45.7		—9		
			N.	—77 08.3		—9		
			N.S.	—77 04.6*		—9		

* Observed on ice; } Direct. —78° 20' 3.
face west.

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 19.	-63 23	210 02	Direct.	-76 48.8	s.w. by w.	-28	-9	-77 26	-77 30
			Direct.	-77 02.5	w.s.w.	-13	-9	-77 25	
20.	-63 47	208 26	Direct.	-76 31.2	s.w. by s.	-55	-9	-77 35	-77 57
			Direct.	-76 26 6	s. by w.	-71	-9	-77 58	
			S.	-77 23.7	s. by w.	-71	-10	-77 58	-77 57
			N.	-76 03.0	s. by w.	-71	-9	-77 46	
			N.S.	-76 36.6	s.s.w.	-63	-9	-77 46	-78 20
			Direct.	-76 33.7	s.	-74	-9	-78 32	
21.	-64 38	206 53	Direct.	-76 42.5	s.	-74	-10	-78 09	-78 20
			S.	-77 34.8	s. by w.	-72	-9	-78 23	
			N.	-76 39.4	s. by w.	-72	-9	-78 21	-78 57
			N.S.	-76 49.5	s. by w.	-72	-10	-78 27	
	-64 50	206 37	Direct.	-76 54.0	s. by w.	-72	-9	-78 27	-79 06
			Direct.	-77 02.0	s. by E.	-72	-9	-78 37	
			Direct.	-76 58.0	s.	-74	-9	-78 37	-79 31
			Direct.	-77 13.3	s.s.w.	-64	-10	-79 03	
	-64 53	206 30	Direct.	-77 15.8	s. by w.	-72	-10	-79 03	-79 34
			S.	-78 13.2	s. by w.	-72	-10	-79 04	
			N.	-77 18.0	s. by w.	-72	-10	-79 04	-79 53
			N.S.	-77 22.6	s. by w.	-72	-10	-79 04	
			Direct.	-77 13.1	s.	-74	-10	-79 04	-79 53
			Direct.	-77 37.4	s.	-75	-10	-79 04	
22.	-65 30	205 41	Direct.	-77 37.4	s.	-75	-10	-79 04	-79 53
			S.	-78 00.3	s.	-75	-10	-79 04	
			N.	-77 47.2	s.	-75	-10	-79 04	-79 53
			N.S.	-77 27.6	s.	-75	-10	-79 04	
			Direct.	-77 38.0	s.	-75	-10	-79 04	-79 53
			Direct.	-79 50.3	E.N.E.	+40	-11	-79 04	
23.	-65 59	204 16	S.	-80 53.5	E.N.E.	+40	-11	-79 04	-79 53
			Direct.	-78 04.0	s. by w.	-73	-10	-79 04	
			S.	-79 32.3	s. by w.	-73	-11	-79 04	-79 53
			N.	-78 11.2	s. by w.	-73	-10	-79 04	
			Direct.	-77 53.0	s.	-75	-10	-79 04	-79 53
			S.	-78 44.7	s.	-75	-10	-79 04	
			N.	-78 06.5	s.	-75	-10	-79 04	-79 53
			N.S.	-77 51.8	s.	-75	-10	-79 04	
24.	65 57	203 53	Direct.	-78 30.4	s.w. by w.	-30	-10	-79 10	-79 31
			Direct.	-80 25.6	N. by w.	+74	-11	-79 23	
			Direct.	-80 11.7	N.E. by N.	+67	-11	-79 16	-79 31
			Direct.	-79 49.2	N.W. $\frac{1}{2}$ W.	+57	-11	-79 03	
			Direct.	-80 27.2	N.	+76	-11	-79 22	-79 31
			Direct.	-80 01.6	N.W.	+60	-11	-79 13	
			Direct.	-79 16.6	w. by N.	+28	-11	-79 00	-79 31
			Direct.	-79 33.4	w.N.W.	+40	-11	-79 04	
	-65 58	203 51	Direct.	-78 14.3	s.s.w.	-65	-10	-79 29	-79 31
			S.	-79 34.4	s.w. by s.	-57	-11	-79 47	
			N.	-78 17.8	s.w. by s.	-57	-10	-79 47	-79 31
			N.S.	-78 05.6	s.w. by s.	-57	-10	-79 15	
25.	-66 00	203 46	Direct.	-78 20.1	s.w.	-45	-10	-79 15	-79 31
			Direct.	-79 38.5	E.	+14	-11	-80 08	
			S.	-80 52.7	E.	+14	-11	-80 08	-79 53
			N.	-79 46.8	E.	+14	-11	-79 54	
			Direct.	-79 39.7	E.	+14	-11	-79 41	
			Direct.	-80 29.6	N.W.	+60	-11	-79 41	
			Direct.	-79 45.6	E. by N.	+28	-11	-79 41	

Fast to a piece of ice.

On the 24th lying becalmed along-side pieces of ice.

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 26.	-66 11	203 36	Direct.	-78 57.0	S.E. by E.	-30	-10	-80 07	-79 53
			S.	-79 45.1	S.E. by E.	-30	-11		
			N.	-79 16.2	S.E. by E.	-30	-11		
			Direct.	-79 02.1	S.E. by E.	-30	-10	-80 11	
			Direct.	-79 59.2	N.W.	+60	-11		
			S.	-81 36.5	N.W.	+60	-12		
27.	-66 16	203 31	Direct.	-79 51.5	E.	+14	-11	-79 48	
			Direct.	-79 48.5	E. 1/2 N.	+21	-11	-79 39	
28.	-66 20	203 22	Direct.	-81 15.2	N.	+76	-12	-80 05	
			Direct.	-81 05.8	N.	+76	-11		
			Direct.	-80 43.5	N.E.	+60	-11		
29.	-66 24	203 51	Direct.	-80 43.5	N.E.	+60	-12	-80 14	
			S.	-81 22.4	N.E.	+60	-12	-79 57	
			Direct.	-79 55.6	E.	+14	-11		-79 53
30.	-66 31	203 07	Direct.	-80 39.2	N.N.E.	+72	-11		-79 38
			Direct.	-80 57.8	N.	+76	-11	-79 53	
			Direct.	-79 05.4	S.W.	-45	-10	-80 00	
			Direct.	-80 39.1	N.W. by W.	+55	-11	-79 55	
31.	-66 32	203 33	Direct.	-78 51.6	S.W. by S.	-57	-10	-79 59	
			Direct.	-78 30.1	S. by W. 1/2 W.	-69	-10	-79 49	
1842.									
Jan. 1.	-66 32	203 32	Direct.	-78 23.9	S.S.E.	-65	-10	-79 48	-79 55
			S.	-78 47.5	S.S.E.	-65	-10		
			N.	-78 39.1	S.S.E.	-65	-10		
			N.S.	-78 29.0	S.S.E.	-65	-10		
			Direct.	-78 24.8	S.S.E.	-65	-10	-80 07	
3.	-66 35	203 29	Direct.	-80 56.0	N. by W. 1/2 W.	+73	-11		
			S.	-81 30.1	N. by W. 1/2 W.	+73	-12		
			N.	-81 08.1	N. by W. 1/2 W.	+73	-11	-79 42	
			N.S.	-81 03.3	N. by W. 1/2 W.	+73	-11		
			Direct.	-81 05.3	N. by W. 1/2 W.	+73	-11		
			Direct.	-79 01.8	S.E. by E.	-30	-10	-79 42	
			Direct.	-78 25.4	S. by E.	-73	-10	-79 48	
6.	-66 06	204 24	Direct.	-78 07.2	S.	-75	-10	-79 39	
			S.	-78 45.8	S.	-75	-10		
			N.	-78 16.1	S.	-75	-10		
			N.S.	-77 58.2	S.	-75	-10	-79 44	
			Direct.	-78 06.1	S.	-75	-10		
7.	-66 13	204 19	Direct.	-78 11.3	S.	-75	-10		
			Direct.	-80 04.6	N.W.	+60	-10	-80 15	
		204 25	Direct.	-78 13.7	S. by W.	-73	-10	-79 37	
			S.	-78 48.3	S.	-75	-10	-79 51	
			N.	-78 26.9	S.	-75	-10		
			N.S.	-78 02.6	S.	-75	-10		
			Direct.	-80 11.0	N.W.	+60	-10	-79 21	
8.	-66 14	204 33	Direct.	-80 35.1	N.	+76	-11	-79 30	
			Direct.	-80 09.6	N.E.	+60	-11	-79 21	
			Direct.	-79 31.2	E.	+14	-11	-79 28	
			Direct.	-78 47.1	S.E.	-45	-10	-79 42	
			Direct.	-78 13.7	S.	-75	-10	-79 39	
			Direct.	-78 09.7	S.S.E.	-65	-10	-79 25	
	-66 12	204 33	Direct.	-80 19.2	N.W.	+60	-11	-79 34	
			S.	-80 44.6	N.W.	+60	-11		
			N.	-80 35.3	N.W.	+60	-11		
			N.S.	-80 20.0	N.W.	+60	-11	-79 34	
			Direct.	-78 09.7	S.S.E.	-65	-10		
			S.	-78 21.6	S.S.E.	-65	-10		
			Direct.	-79 35.7	W.	+14	-11	-79 34	
			Direct.	-78 53.6	S.W. by W.	-30	-10		

Fast to the same piece of ice as Terror, distant 25 fathoms from her.

Sailing amongst loose ice.

Fast to the same piece of ice as Terror, distant 25 fathoms from her.

Sailing amongst loose ice.

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.	
						Ship's attraction.	Index.			
Jan. 9.	—66 04	204 19	Direct.	—78 48.7	s.w. $\frac{1}{2}$ w.	—37	—10	—79 36	° ' }	
			Direct.	—79 24.0	E. by s.	—1	—11	—79 36		
			Direct.	—78 39.5	s.w.	—45	—10	—79 35		
10.	—65 59	204 12	Direct.	—78 50.8	s.w. by w.	—30	—10	—79 41	—79 38	
			S.	—79 41.0	s.w. by w.	—30	—11			
			N.	—78 40.9	s.w. by w.	—30	—10			
			N.S.	—78 47.0	s.w. by w.	—30	—10			
			Direct.	—79 32.0	E.	+14	—11	—79 36		
			S.	—79 45.4	E.	+14	—11	—79 36		
11.	—65 58	203 44	Direct.	—80 18.8	N.E. by E.	+55	—11	—79 35		
			Direct.	—78 19.8	s.	—75	—10	—79 45		
12.	—65 54	203 32	Direct.	—78 25.0	s.w.	—45	—10	—79 38		
			S.	—79 00.8	s.w.	—45	—10			
			Direct.	—78 26.9	s.w. $\frac{1}{2}$ s.	—51	—10	—79 28		
13.	—66 11	203 03	Direct.	—79 08.0	s.w. $\frac{3}{4}$ w.	—34	—10	—79 52		
			Direct.	—79 06.4	s.w. by w.	—30	—10	—79 46		
	—66 12	203 05	Direct.	—78 02.0	S.S.E.	—65	—10	—79 24	—79 35	
			S.	—78 26.2	S.S.E.	—65	—10			
			N.	—78 00.7	S.S.E.	—65	—10			
			N.S.	—78 07.4	S.S.E.	—65	—10			
			Direct.	—80 37.5	N.N.E.	+72	—10	—79 43		
			S.	—80 51.9	N.N.E.	+72	—10			
			N.	—80 36.8	N.N.E.	+72	—11			
			N.S.	—80 40.1	N.N.E.	+72	—11	—79 37		
			Direct.	—80 35.5	N.N.E.	+72	—11	—79 50		
14.	—66 14	203 09	Direct.	—80 34.2	N.E. by E.	+55	—11	—79 50		
			Direct.	—78 00.9	s. by w.	—73	—10	—79 24	—79 33	
			Direct.	—80 28.4	N.E.	+60	—11	—79 39		
			Direct.	—78 08.3	s. by w.	—73	—10	—79 31		
15.	—66 02	202 30	Direct.	—78 28.0	s.w.	—45	—10	—79 23		
16.	—65 49	202 02	Direct.	—79 21.4	E.	+14	—11	—79 18		
			S.	—79 28.9	Observed on ice.		—11	—79 47	—79 47	
			N.	—79 33.2			—11			
			N.S.	—79 58.8			—11			
			Direct.	—79 22.4*			—11			
19.	—66 18	201 22	Direct.	—79 08.3	s.w. by w.	—30	—10	—79 48		
			Direct.	—81 06.4	N. by E.	+74	—11	—80 03		
21.	—66 49	202 40	Direct.	—78 33.0	s. by E.	—73	—10	—80 05	—80 01	
			S.	—79 08.5	s. by E.	—73	—10			
			N.	—78 35.4	s. by E.	—73	—10			
			N.S.	—78 29.5	s. by E.	—73	—10			
28.	—67 38	204 01	Direct.	—81 23.9	N.	+76	—12	—80 30		
			N.	—81 37.4	N.	+76	—12			
			S.	—81 39.4	N.	+76	—12			
			Direct.	—78 53.5	s.	—75	—10	—80 19		
			Direct.	—79 00.5	s. by w. $\frac{1}{2}$ w.	—69	—10	—80 20		—80 22
29.	—67 32	203 59	Direct.	—79 00.4	S.S.W.	—65	—10			
			S.	—79 04.6	S.S.W.	—65	—10			
			N.	—79 01.8	S.S.W.	—65	—10			
			N.S.	—79 01.9	S.S.W.	—65	—10			

* Observed on ice, } Direct. —80° 39'.2.
face west

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Jan. 30.	—67 18	203 39	Direct.	—79 30.8	s.w. $\frac{1}{2}$ s.	—51	—11	—80 47	
			S.	—80 28.3	s.w. $\frac{1}{2}$ s.	—51	—11		
			N.	—79 38.7	s.w. $\frac{1}{2}$ s.	—51	—11		
			N.S.	—79 25.5	s.w. $\frac{1}{2}$ s.	—51	—11		
			Direct.	—79 59.3	s. by w.	—73	—10	—81 22	—80 26
31.	—67 21	202 15	Direct.	—79 04.4	s.w.	—45	—10	—80 02	
			S.	—79 19.5	s.w.	—45	—11		
			N.	—79 04.2	s.w.	—45	—10		
			N.S.	—79 00.3	s.w.	—45	—10		
			Direct.	—79 39.1	w.s.w.	—15	—11	—80 09	
Feb. 1.	—67 11	202 07	Direct.	—79 48.5	w.s.w.	—15	—11	—80 18	
2.	—67 57	200 00	Direct.	—79 22.4	S.E.	—45	—11		
			Direct.	—79 59.5	s. by w.	—73	—11		
			Direct.	—79 32.0	S.S.E. $\frac{1}{2}$ E.	—61	—11		—80 46
			S.	—79 49.7	S.S.E. $\frac{1}{2}$ E.	—61	—11	—80 44	
			N.	—79 30.2	S.S.E. $\frac{1}{2}$ E.	—61	—11		
			N.S.	—79 23.0	S.S.E. $\frac{1}{2}$ E.	—61	—11		
			Direct.	—79 27.3	S.S.E. $\frac{1}{2}$ E.	—61	—11		
3.	—68 21	200 03	Direct.	—80 01.0	S.E. by S.	—57	—11	—81 04	
			S.	—79 53.0	S.E. by S.	—57	—11		
			N.	—79 50.4	S.E. by S.	—57	—11		
			N.S.	—79 57.1	S.E. by S.	—57	—11		
			Direct.	—79 56.8	S.E. by S.	—57	—11	—81 14	
4.	—68 42	199 44	Direct.	—79 58.7	S. $\frac{1}{2}$ E.	—74	—11		—81 24
			S.	—80 17.9	S. $\frac{1}{2}$ E.	—74	—11		
			N.	—79 57.9	S. $\frac{1}{2}$ E.	—74	—11		
			N.S.	—79 41.9	S. $\frac{1}{2}$ E.	—74	—11		
	—68 49	199 41	Direct.	—82 12.8	N. by w.	+74	—12	—81 09	
5.	—68 59	196 07	Direct.	—80 53.5	s.w.	—45	—11	—81 00	
		195 51	Direct.	—80 49.0	s.w. by s.	—57	—11	—81 57	
			S.	—81 02.2	s.w. by s.	—57	—11		
			N.	—80 46.0	s.w. by s.	—57	—11		
			N.S.	—80 39.6	s.w. by s.	—57	—11		
			Direct.	—81 52.8	w. $\frac{1}{2}$ N.	+22	—12	—81 43	—82 35
6.	—69 48	192 25	Direct.	—81 08.5	s. by w.	—74	—11	—82 35	
			S.	—81 28.9	s. by w.	—74	—12		
			N.	—81 11.0	s. by w.	—74	—11		
			N.S.	—80 47.4	s. by w.	—74	—11		
			Direct.	—81 12.3	s. by w.	—74	—12	—82 43	
7.	—70 05	191 10	Direct.	—81 45.1	s.w.	—46	—12		—82 51
			S.	—81 50.1	s.s.w.	—66	—12		
			N.	—81 38.8	s.s.w.	—66	—12		
			N.S.	—81 13.2	s.s.w.	—66	—12		
			Direct.	—81 29.8	s.s.w.	—66	—12	—82 53	
	—70 17	190 15	Direct.	—81 43.0	s.s.w.	—66	—12		
	—70 26	189 00	Direct.	—82 07.0	s.s.w.	—66	—12		
			S.	—81 39.2	s.s.w.	—66	—12		
			N.	—81 44.5	s.s.w.	—66	—12	—83 07	
			N.S.	—81 27.0	s.s.w.	—66	—12		
			Direct.	—82 10.2	s.s.w.	—66	—12		
8.	—70 18	186 01	Direct.	—81 50.6	s.	—77	—12		
			S.	—81 59.7	s.	—77	—12	—83 18	
			N.	—81 49.3	s.	—77	—12		
			N.S.	—81 37.1	s.	—77	—12		
			Direct.	—81 50.0	s.	—77	—12		

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Feb. 9.	—70 39	185 31	Direct.	—82 06.3	s. by E.	—75	—12	—83 33	—83 35
			Direct.	—82 24.5	S.E. by s.	—58	—12	—83 36	
			S.	—82 50.4	S.E. by s.	—58	—12		
			N.	—82 14.6	S.E. by s.	—58	—12		
			N.S.	—82 17.0	S.E. by s.	—58	—12		
			Direct.	—82 23.2	S.E. by s.	—58	—12		
10.	—70 11	183 50	Direct.	—83 23.9	w. by s.	0	—13		—83 33
			S.	—83 21.9	w. by s.	0	—13		
			N.	—83 17.2	w. by s.	0	—13		
			N.S.	—83 17.1	w. by s.	0	—13		
			Direct.	—83 21.9	w. by s.	0	—13		
	—70 04	183 36	Direct.	—83 25.0*	s. by w.	—75	—13	—84 53	A head swell.
11.	—70 06	181 50	Direct.	—82 47.0	s.w. by s.	—58	—12	—83 57	
	—70 10	181 34	Direct.	—82 58.5	s.w.	—47	—12	—83 49	—84 06 A heavy cross sea.
			N.	—83 07.2	s.w.	—47	—12		
			N.S.	—82 25.0	s.w.	—47	—12		
12.	—71 00	180 44	Direct.	—83 01.3	S.E. by s.	—58	—12		
			S.	—83 03.7	S.E. by s.	—58	—12		
			N.	—83 18.7	S.E. by s.	—58	—13		
			N.S.	—83 12.7	S.E. by s.	—58	—13		
			Direct.	—83 05.5	S.E. by s.	—58	—12		
13.	—72 46	181 46	Direct.	—83 32.6	S.E. by s.	—59	—13		—85 01
			S.	—84 23.9	S.E. by s.	—59	—13		
			N.	—83 46.0	S.E. by s.	—59	—13		
			N.S.	—83 45.2	S.E. by s.	—59	—13		
			Direct.	—83 36.7	S.E. by s.	—59	—13		—85 04
			Direct.	—84 04.8	S.E.	—47	—13	—85 05	
14.	—73 23	183 04	Direct.	—84 36.5	S.E. $\frac{1}{2}$ S.	—53	—13	—85 42	—86 02 Very much motion.
15.	—74 24	177 09	Direct.	—85 07.0	S.S.E. $\frac{1}{2}$ E.	—63	—13	—86 23	
16.	—74 56	173 36	Direct.	—85 17.0	S.S.E.	—69	—14		—86 48
			S.	—85 51.8	S.S.E.	—69	—14		
			N.	—85 20.5	S.S.E.	—69	—14		
			N.S.	—85 10.0	S.S.E.	—69	—13		
			Direct.	—85 21.0	s. by E. $\frac{1}{2}$ E.	—74	—14	—86 49	—86 52 Very unsteady.
			Direct.	—86 03.6	S.E.	—48	—14	—87 06	
	—75 10	173 08	Direct.	—86 46.9	E.	+16	—14		—86 59
			S.	—87 28.5	E.	+16	—15		
			N.	—87 06.9	E.	+16	—14		
			N.S.	—86 56.4	E.	+16	—14		
			Direct.	—86 48.5	E.	+16	—14		
17.	—75 53	175 05	Direct.	—87 01.5	E.N.E.	+42	—14		—86 44
	—76 00	175 15	Direct.	—87 03.5	E.N.E.	+42	—14		
			S.	—87 29.1	E.N.E.	+42	—15		
			N.	—87 26.9	E.N.E.	+42	—15		
			N.S.	—87 06.3	E.N.E.	+42	—14		
			Direct.	—87 07.0	E.N.E.	+42	—14		
18.	—76 58	181 03	Direct.	—86 58.5	E.N.E.	+42	—14		—86 46
			S.	—87 17.7	E.N.E.	+42	—15		
			N.	—87 37.8	E.N.E.	+42	—15		
			N.S.	—87 18.8	E.N.E.	+42	—15		
			Direct.	—86 57.8	E.N.E.	+42	—14		

* This observation differs so widely from the others made on the same day, that, considering the unfavourable state of the weather, I have omitted it in the mean results: possibly the ship's head may have been W. by S. instead of S. by W., in which case the observation would agree well with the others.—E. S.

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Feb. 19.	-76 42	184 09	Direct.	-87 24.5	N. by E.	+78	-15	-86 07	Ship pitching.
			S.	-86 57.7	N. by E.	+78	-14		
			N.	-87 15.6	N. by E.	+78	-15		
			N.S.	-86 56.5	N. by E.	+78	-14		
			Direct.	-87 21.2	N. by E.	+78	-15		
	-76 46	186 15	Direct.	-87 08.0	N.N.E.	+75	-14	-86 07	A head sea and much motion.
			Direct.	-85 58.3	N.E. $\frac{1}{2}$ E.	+60	-14		
			20. -76 14	192 35	S.W.	-47	-13		
			21. -75 53	194 52	S.E. by S.	-60	-13		
			22. -76 42	194 48	S.E. by S.	-60	-13		
	-76 42	194 10	S.	-84 19.6	S.E. by S.	-60	-13	-85 25	A swell from the southward.
			N.	-84 24.0	S.E. by S.	-60	-13		
			N.S.	-84 10.5	S.E. by S.	-60	-13		
			Direct.	-84 04.0	S.E. by S.	-60	-13		
			Direct.	-84 56.5	E.S.E.	-17	-13		
	-77 05	194 38	Direct.	-84 53.0	E. by S.	0	-13	-85 24	-85 24
			S.	-85 36.6	E. by S.	0	-14		
			N.	-85 16.0	E. by S.	0	-14		
			N.S.	-85 13.0	E. by S.	0	-14		
			Direct.	-84 55.0	E. by S.	0	-13		
23.	-77 49	197 24	Direct.	-84 26.5	E. by S.	0	-13	-84 40	-84 49
			Direct.	-84 05.3	S.W. by W.	-33	-13		
			Direct.	-84 40.3	E. $\frac{1}{2}$ S.	+8	-13		
			Direct.	-84 51.9	W. by N.	+30	-13		
			Direct.	-84 12.0	S.W.	-47	-13		
	-78 07	197 44	Direct.	-84 41.0	W.	+15	-13	-84 53	-84 49
			S.	-84 57.7	W.	+15	-13		
			N.	-85 13.0	W.	+15	-14		
			N.S.	-84 50.0	W.	+15	-13		
			Direct.	-84 50.3	W. by N.	+30	-13		
	-72 46	189 59	Direct.	-83 27.2	S.S.W.	-68	-13	-84 38	-84 38
			Direct.	-85 15.7	N.W. by W.	+57	-14		
			S.	-85 38.0	N.W. by W.	+57	-14		
			N.	-85 14.5	N.W. by W.	+57	-14		
			N.S.	-85 25.5	N.W. by W.	+57	-14		
27.	-72 01	187 35	Direct.	-85 11.3	N.W. by W.	+57	-13	-84 10	-84 10
			Direct.	-83 38.0	W.S.W.	-16	-13		
			S.	-83 48.2	W.S.W.	-16	-13		
			N.	-83 44.1	W.S.W.	-16	-13		
			N.S.	-83 44.2	W.S.W.	-16	-13		
	-71 08	184 59	Direct.	-83 40.8	W.S.W.	-16	-13	-84 04	-84 04
			Direct.	-84 05.5	W.	+15	-13		
			S.	-84 18.4	W.	+15	-13		
			N.	-84 06.5	W.	+15	-13		
			N.S.	-84 10.4	W.	+15	-13		
Mar. 1.	-69 52	180 04	Direct.	-84 04.5	W.	+15	-13	-83 34	-83 34
			Direct.	-83 48.6	W.	+15	-13		
			Direct.	-84 35.5	W. by N.	+33	-13		
			S.	-83 59.2	W. by N.	+33	-13		
			N.	-83 45.0	W. by N.	+33	-13		
	-69 44	179 53	N.S.	-83 39.7	W. by N.	+33	-13	-83 31	A northerly swell.
			Direct.	-83 32.0	W. by N.	+33	-13		
			Direct.	-84 59.1	N. by E.	+93	-13		
			S.	-84 36.6	N. by E.	+93	-13		
			N.	-84 54.2	N. by E.	+93	-13		
			N.S.	-84 52.0	N. by E.	+93	-13		
			Direct.	-84 54.0	N. by E.	+93	-13		

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.				
						Ship's attraction.	Index.						
Mar. 2.	68 04	183 25	Direct.	83 43.3	N.N.E.	+90	13	82 28	82 13				
			S.	83 54.0	N.N.E.	+90	13						
			N.	83 50.2	N.N.E.	+90	13						
			N.S.	83 38.2	N.N.E.	+90	13						
			Direct.	83 37.5	N.N.E.	+90	13						
			Direct.	83 03.2	N.E. by N.	+82	12						
			S.	83 14.4	N.E. by N.	+82	13						
			N.	83 12.7	N.E. by N.	+82	13						
			N.S.	83 04.7	N.E. by N.	+82	12						
			Direct.	82 59.0	N.E. by N.	+82	12						
			Direct.	82 31.0	E.N.E.	+51	12						
3.	67 32	185 09	S.	82 41.5	E.N.E.	+51	12	81 56	81 51				
			N.	82 44.3	E.N.E.	+51	12						
			N.S.	82 23.6	E.N.E.	+51	12						
			Direct.	82 48.7	N.E. by N.	+81	12						
			Direct.	82 34.8	N.E.	+74	12						
			Direct.	80 39.5	W.S.W.	20	11						
			Direct.	82 05.6	N. by E.	+91	12						
			N.	82 37.2	N. by E.	+91	12						
			N.S.	82 29.0	N. by E.	+91	12						
			Direct.	81 59.0	N. by E.	+91	12						
			Direct.	80 28.3	N. by E.	+89	11						
6.	65 25	191 48	N.	80 41.9	N. by E.	+89	11	79 19	79 19				
			N.S.	80 54.6	N. by E.	+89	11						
			Direct.	80 31.8	N. by E.	+89	11						
			Direct.	80 24.0	N. by E.	+89	11						
			Direct.	79 37.0	N. by E.	+88	11						
			Direct.	79 31.3	N. by E.	+88	11						
			S.	79 44.5	N. by E.	+88	11						
			N.	79 08.1	N. by E.	+88	10						
			N.S.	79 20.2	N. by E.	+88	11						
			Direct.	79 27.4	N. by E.	+88	11						
			Direct.	78 35.1	N. by E.	+87	10						
8.	62 16	196 10	S.	78 40.4	N. by E.	+87	10	77 17	77 17				
			N.	78 30.5	N. by E.	+87	10						
			N.S.	78 34.0	N. by E.	+87	10						
			Direct.	78 31.9	N. by E.	+87	10						
			Direct.	77 33.0	N.E. by N.	+76	10						
			S.	78 15.5	N.E. by N.	+76	10						
			N.	77 36.7	N.E. by N.	+76	10						
			N.S.	77 24.7	N.E. by N.	+76	10						
			Direct.	77 23.8	N.E. by N.	+76	10						
			Direct.	76 36.5	N.E. by N.	+75	9						
			S.	77 19.5	N.E. by N.	+75	10						
9.	61 14	198 38	N.	76 31.7	N.E. by N.	+75	9	75 33	75 33				
			N.S.	76 09.5	N.E. by N.	+75	9						
			Direct.	76 34.0	N.E. by N.	+75	9						
			Direct.	75 33.0	E.N.E.	+48	9						
			Direct.	75 23.0	E. by N.	+33	9						
			S.	76 07.5	E. by N.	+33	9						
			N.	76 18.0	E. by N.	+33	9						
			N.S.	75 48.2	E. by N.	+33	9						
			Direct.	75 24.4	E. by N.	+33	9						
			Direct.	74 27.0	E. by N.	+33	9						
			10.	60 18	203 55	Direct.	75 33.0	E.N.E.		+48	9	74 54	75 08
Direct.	75 23.0	E. by N.				+33	9						
S.	76 07.5	E. by N.				+33	9						
N.	76 18.0	E. by N.				+33	9						
N.S.	75 48.2	E. by N.				+33	9						
Direct.	75 24.4	E. by N.				+33	9						
Direct.	74 27.0	E. by N.				+33	9						
11.	60 18	208 29				Direct.	74 27.0	E. by N.	+33	9	75 11	A cross sea, ship pitching.	
						Direct.	74 27.0	E. by N.	+33	9			
						Direct.	74 27.0	E. by N.	+33	9			
						Direct.	74 27.0	E. by N.	+33	9			
			Direct.	74 27.0	E. by N.	+33	9						
			Direct.	74 27.0	E. by N.	+33	9						
			Direct.	74 27.0	E. by N.	+33	9						
			Direct.	74 27.0	E. by N.	+33	9						
			Direct.	74 27.0	E. by N.	+33	9						
			Direct.	74 27.0	E. by N.	+33	9						
			Direct.	74 27.0	E. by N.	+33	9						

A very heavy sea and much motion.

A very heavy swell from the westward.

Much motion.

A cross sea, ship pitching.

Very much motion.

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Mar. 12.	-60 13	211 34	Direct.	-74 06.5	E. by N.	+33	-8	<div> <div> <div>o</div> <div>'</div> <div>o</div> <div>'</div> </div> <div> <div>-74 21</div> <div>-74 21</div> </div> </div>	A heavy swell, ship very unsteady.
			S.	-74 23.3	E. by N.	+33	-8		
			N.	-74 57.0	E. by N.	+33	-8		
			N.S.	-74 57.5	E. by N.	+33	-8		
			Direct.	-74 18.0	E. by N.	+33	-8		
			Direct.	-74 02.5	E. by N.	+33	-8		
			Direct.	-73 56.0	N.E.	+67	-8		
			Direct.	-73 26.6	N.E. by E.	+59	-8		
			S.	-74 20.7	N.E. by E.	+59	-8		
			N.	-73 57.5	N.E. by E.	+59	-8		
			N.S.	-73 47.2	N.E. by E.	+59	-8		
			Direct.	-73 35.3	N.E. by E.	+59	-8		
			Direct.	-75 17.5	N.E. by E.	+59	-9		
			Direct.	-75 10.5	N.E. by E.	+59	-8		
			S.	-74 54.1	N.E. by E.	+59	-8		
			N.	-74 42.7	N.E. by E.	+59	-8		
			N.S.	-74 49.5	N.E. by E.	+59	-8		
			Direct.	-74 32.1	E.N.E.	+48	-8		
			S.	-74 07.2	E.N.E.	+48	-8		
			N.	-74 26.1	E.N.E.	+48	-8		
			N.S.	-74 11.7	E.N.E.	+48	-8		
			Direct.	-74 28.8	E.N.E.	+48	-8		
			Direct.	-73 57.5	E. by N.	+33	-8		
			Direct.	-73 55.0	E. by N.	+33	-8		
13.	-60 00	216 12	Direct.	-73 11.8	E.	+19	-7		
			Direct.	-73 11.0	E.	+19	-7		
			S.	-72 20.2	E.	+19	-7		
			N.	-73 06.0	E.	+19	-7		
			N.S.	-73 54.2	E.	+19	-8		
			Direct.	-73 14.5	E.	+19	-8		
			Direct.	-73 07.3	E.	+19	-7		
			Direct.	-72 45.0	E. $\frac{1}{2}$ S.	+12	-7		
			S.	-72 57.6	E. $\frac{1}{2}$ S.	+12	-7		
			N.	-73 23.0	E. $\frac{1}{2}$ S.	+12	-7		
			N.S.	-73 10.7	E. $\frac{1}{2}$ S.	+12	-7		
			Direct.	-72 39.0	E. $\frac{1}{2}$ S.	+12	-7		
14.	-59 24	218 58	Direct.	-72 24.5	E. $\frac{1}{2}$ S.	+12	-7		
			S.	-73 00.5	E. $\frac{1}{2}$ S.	+12	-7		
			N.	-73 16.7	E. $\frac{1}{2}$ S.	+12	-7		
			N.S.	-73 03.0	E. $\frac{1}{2}$ S.	+12	-7		
			Direct.	-72 35.5	E. by S.	+4	-7		
			S.	-73 02.2	E. by S.	+4	-7		
			N.	-73 21.7	E. by S.	+4	-8		
			N.S.	-72 57.0	E. by S.	+4	-7		
			S.	-73 04.2	E.	+19	-7		
			Direct.	-72 29.8	E.	+19	-7		
			S.	-73 16.5	E.	+19	-8		
			N.	-73 25.6	E.	+19	-8		
15.	-58 54	222 04	N.S.	-73 01.3	E.	+19	-7		
			Direct.	-72 33.0	E.	+19	-7		
			Direct.	-72 57.5	E. by N.	+33	-7		
			S.	-73 24.1	E. by N.	+33	-8		
			N.	-73 44.0	E. by N.	+33	-8		
			N.S.	-73 19.0	E. by N.	+33	-8		
			Direct.	-72 57.5	E. by N.	+33	-7		
			S.	-73 24.1	E. by N.	+33	-8		
			N.	-73 44.0	E. by N.	+33	-8		
			N.S.	-73 19.0	E. by N.	+33	-8		
			Direct.	-72 57.5	E. by N.	+33	-7		
			S.	-73 24.1	E. by N.	+33	-8		
			N.	-73 44.0	E. by N.	+33	-8		
16.	-59 04	228 57	N.S.	-73 19.0	E. by N.	+33	-8		
			Direct.	-72 57.5	E. by N.	+33	-8		
			Direct.	-73 55.0	E. by N.	+33	-8		
			Direct.	-73 11.8	E.	+19	-7		
			Direct.	-73 11.0	E.	+19	-7		
			S.	-72 20.2	E.	+19	-7		
			N.	-73 06.0	E.	+19	-7		
			N.S.	-73 54.2	E.	+19	-8		
			Direct.	-73 14.5	E.	+19	-8		
			Direct.	-73 07.3	E.	+19	-7		
			Direct.	-72 45.0	E. $\frac{1}{2}$ S.	+12	-7		
			S.	-72 57.6	E. $\frac{1}{2}$ S.	+12	-7		
17.	-59 39	232 48	N.	-73 23.0	E. $\frac{1}{2}$ S.	+12	-7		
			N.S.	-73 10.7	E. $\frac{1}{2}$ S.	+12	-7		
			Direct.	-72 39.0	E. $\frac{1}{2}$ S.	+12	-7		
			Direct.	-72 24.5	E. $\frac{1}{2}$ S.	+12	-7		
			S.	-73 00.5	E. $\frac{1}{2}$ S.	+12	-7		
			N.	-73 16.7	E. $\frac{1}{2}$ S.	+12	-7		
			N.S.	-73 03.0	E. $\frac{1}{2}$ S.	+12	-7		
			Direct.	-72 35.5	E. by S.	+4	-7		
			S.	-73 02.2	E. by S.	+4	-7		
			N.	-73 21.7	E. by S.	+4	-8		
			N.S.	-72 57.0	E. by S.	+4	-7		
			S.	-73 04.2	E.	+19	-7		
18.	-60 21	237 02	Direct.	-72 29.8	E.	+19	-7		
			S.	-73 16.5	E.	+19	-8		
			N.	-73 25.6	E.	+19	-8		
			N.S.	-73 01.3	E.	+19	-7		
			Direct.	-72 33.0	E.	+19	-7		
			Direct.	-72 57.5	E. by N.	+33	-7		
			S.	-73 24.1	E. by N.	+33	-8		
			N.	-73 44.0	E. by N.	+33	-8		
			N.S.	-73 19.0	E. by N.	+33	-8		
			Direct.	-72 57.5	E. by N.	+33	-7		
			S.	-73 24.1	E. by N.	+33	-8		
			N.	-73 44.0	E. by N.	+33	-8		
			N.S.	-73 19.0	E. by N.	+33	-8		

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Mar. 18.	—60 20	237 50	Direct.	—73 15.0	E. by N. $\frac{1}{2}$ N.	+40	—8	—72 34 —72 44	
	—60 19	238 00	Direct.	—72 24.5	E. by N. $\frac{1}{2}$ N.	+40	—7		
			S.	—72 55.7	E. by N. $\frac{1}{2}$ N.	+40	—7		
			N.	—73 24.6	E. by N. $\frac{1}{2}$ N.	+40	—8		
19.	—60 02	241 03	N.S.	—73 30.6	E. by N. $\frac{1}{2}$ N.	+40	—8	—72 40 —72 40	Much motion.
	—60 01	241 38	Direct.	—72 52.5	E.N.E.	+47	—7		
			Direct.	—72 45.5	E.N.E.	+47	—7		
			S.	—73 47.5	E.N.E.	+47	—8		
20.	—59 17	245 40	N.	—73 43.0	E.N.E.	+47	—8	—71 29 —71 29	
			N.S.	—73 28.0	E.N.E.	+47	—8		
			Direct.	—72 08.0	E.N.E.	+47	—7		
			S.	—72 12.0	E.N.E.	+47	—7		
21.	—59 15	248 12	N.	—72 01.0	E.N.E.	+47	—7	—71 26 —71 26	
			N.S.	—72 14.0	E.N.E.	+47	—7		
			Direct.	—72 09.5	E.N.E.	+47	—7		
			Direct.	—71 33.5	E. by N.	+33	—7		
	—59 04	248 50	S.	—72 10.0	E. by N.	+33	—7	—70 59	
	—58 58	249 24	N.	—71 55.9	E. by N.	+33	—7		
			N.S.	—72 11.2	E. by N.	+33	—7		
			Direct.	—71 35.2	E. by N.	+33	—7		
			Direct.	—71 53.5	N.E. $\frac{1}{2}$ E.	+61	—7	—71 08 —71 04	
			Direct.	—71 46.0	N.E. by E.	+58	—7		
			S.	—72 01.2	N.E. by E.	+58	—7		
			N.	—71 53.0	N.E. by E.	+58	—7		
22.	—58 28	252 01	N.S.	—72 14.7	N.E. by E.	+58	—7	—70 51 —70 44	
			Direct.	—71 30.6	E.N.E.	+47	—7		
	—58 29	252 22	Direct.	—71 11.0	E. by N.	+33	—6		
			Direct.	—71 02.4	E. $\frac{1}{2}$ N.	+26	—6		
23.	—58 35	255 10	S.	—71 33.5	E. $\frac{1}{2}$ N.	+26	—7	—70 52 —70 50	A head sea.
			N.	—71 05.8	E. $\frac{1}{2}$ N.	+26	—6		
			N.S.	—71 07.4	E. $\frac{1}{2}$ N.	+26	—6		
			Direct.	—70 26.0	E. $\frac{1}{2}$ N.	+26	—6		
			S.	—70 36.9	E. $\frac{1}{2}$ N.	+26	—6	—70 11 —70 11	
			N.	—70 45.2	E. $\frac{1}{2}$ N.	+26	—6		
			N.S.	—70 16.0	E. $\frac{1}{2}$ N.	+26	—6		
			Direct.	—70 30.0	E. $\frac{1}{2}$ N.	+26	—6		
24.	—58 44	257 49	Direct.	—70 04.5	E. $\frac{1}{2}$ N.	+26	—6	—69 47 —69 47	
			S.	—70 29.6	E. $\frac{1}{2}$ N.	+26	—6		
			N.	—70 24.7	E. $\frac{1}{2}$ N.	+26	—6		
			N.S.	—69 49.2	E. $\frac{1}{2}$ N.	+26	—6		
	—58 51	258 34	Direct.	—69 48.3	E. $\frac{1}{2}$ N.	+26	—6	—67 39 —67 39	A heavy swell.
25.	—58 56	263 52	Direct.	—68 52.8	E. by N. $\frac{1}{2}$ N.	+40	—5		
26.	—59 01	267 59	Direct.	—67 56.0	E. by N. $\frac{1}{2}$ N.	+40	—5		
			S.	—68 21.7	E. by N. $\frac{1}{2}$ N.	+40	—5		
			N.	—68 18.7	E. by N. $\frac{1}{2}$ N.	+40	—5	—67 01 —67 01	Ship unsteady.
			N.S.	—67 56.8	E. by N. $\frac{1}{2}$ N.	+40	—5		
			Direct.	—67 59.5	E. by N. $\frac{1}{2}$ N.	+40	—5		
			Direct.	—67 25.5	E.N.E.	+46	—5		
27.	—59 02	271 58	S.	—68 44.6	E.N.E.	+46	—5	—67 01 —67 01	
			N.	—67 35.7	E.N.E.	+46	—5		
			N.S.	—67 13.7	E.N.E.	+46	—5		
			Direct.	—67 30.5	E.N.E.	+46	—5		

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Mar. 28.	-58 55	276 30	Direct.	-66 10.0	N.E. by E.	+55	-4	-65 27 -65 27	
			Direct.	-66 13.0	N.E. by E.	+55	-4		
			S.	-66 41.4	N.E. by E.	+55	-4		
			N.	-66 22.2	N.E. by E.	+55	-4		
			N.S.	-66 14.5	N.E. by E.	+55	-4		
			Direct.	-66 09.5	N.E. by E.	+55	-4		
			Direct.	-65 40.5	N.E. $\frac{1}{2}$ E.	+57	-4		
			S.	-65 56.7	N.E. $\frac{1}{2}$ E.	+57	-4		
			N.	-65 46.0	N.E. $\frac{1}{2}$ E.	+57	-4		
			N.S.	-65 28.5	N.E. $\frac{1}{2}$ E.	+57	-4		
29.	-58 23	280 03	Direct.	-65 36.0	N.E. $\frac{1}{2}$ E.	+57	-4	-64 49 -64 49	
			Direct.	-64 27.9	N.E. by E. $\frac{1}{2}$ E.	+50	-3		
			S.	-64 27.7	N.E. by E. $\frac{1}{2}$ E.	+50	-3		
			N.	-64 39.2	N.E. by E. $\frac{1}{2}$ E.	+50	-3		
			N.S.	-64 29.9	N.E. by E. $\frac{1}{2}$ E.	+50	-3		
			Direct.	-64 22.0	N.E. $\frac{1}{2}$ E.	+54	-3		
			Direct.	-63 52.3	N.E. $\frac{1}{2}$ N.	+58	-3		
			Direct.	-63 49.0	N.E. by N.	+60	-3		
			N.	-64 34.2	N.E. by N.	+60	-3		
			N.S.	-64 10.0	N.E. by N.	+60	-3		
30.	-58 29	282 04	Direct.	-63 43.0	N.E. by N.	+60	-3	-63 44 -63 41	
			Direct.	-62 24.0	N.E. by N.	+56	-2		
			S.	-62 16.2	N.E. by N.	+56	-2		
			N.	-61 50.6	N.E. by N.	+56	-2		
			N.S.	-61 59.0	N.E. by N.	+56	-2		
			Direct.	-62 17.0	N.E. by N.	+56	-2		
			Direct.	-59 31.0	E.N.E.	+44	-1		
			S.	-59 28.3	E.N.E.	+44	-1		
			N.	-59 55.5	E.N.E.	+44	-1		
			N.S.	-58 59.0	E.N.E.	+44	-1		
31.	-58 28	282 32	Direct.	-59 25.3	E.N.E.	+44	-1	-63 31 -63 05	A very heavy swell.
			Direct.	-58 35.5	S.S.E.	-46	0		
			Direct.	-59 44.0	N.E.	+55	-1		
			S.	-60 36.7	N.E.	+55	-1		
			N.	-60 05.7	N.E.	+55	-1		
			N.S.	-59 36.5	N.E.	+55	-1		
			Direct.	-59 33.5	N.E.	+55	-1		
			Direct.	-57 34.0	N. by E.	+54	0		
			N.	-57 00.3	N. by E.	+54	0		
			N.S.	-57 10.0	N. by E.	+54	0		
April 1.	-57 22	289 50	Direct.	-57 24.0	N. by E.	+54	0	-56 10 -56 10	Too much motion to use S.
			Direct.	-54 47.5	N.N.E.	+47	+2		
			S.	-54 56.6	N.N.E.	+47	+2		
			N.	-54 45.7	N.N.E.	+47	+2		
			N.S.	-54 30.7	N.N.E.	+47	+2		
			Direct.	-54 26.0	N.N.E.	+47	+2		
			Direct.	-54 23.8	N.N.E.	+41	+2		
			Direct.	-53 08.0	N.W. by N.	+42	+3		
			Direct.	-52 10.0	E. by S.	+18	+3		
			Direct.	-52 29.1					
2.	-57 10	292 11	S.	-52 42.7	Observed on shore.	}	+3	-52 30 -52 30	A swell from the westward.
			N.	-52 37.9					
			N.S.	-52 41.2*					
3.	-57 17	292 32							
4.	-56 40	294 46							
5.	-52 54	300 27							
6.	-52 36	301 18							
7.	-51 47	302 15							
8.	-51 32	301 53							

* Observed on shore; face west. { Direct. -53 48.9
S. -53 29.2
N. -53 45.9
N.S. -53 41.5

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method. employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attrac- tion.	Index.		
Aug. 19.	—51° 32'	301° 53'	Direct.	—52° 20.6	} Observed on shore.	}	+3	—52° 30'	—52° 30'
			S.	—52 35.6					
			N.	—52 24.4					
			N.S.	—52 31.5*					
17.	—51 32	301 53	Direct.	—52 46.5	W.	+37	+3	} —52 14	}
			S.	—53 00.9	W.	+37	+3		
			Direct.	—52 38.8	W.N.W.	+38	+3		
			S.	—52 39.4	W.N.W.	+38	+3		
			Direct.	—52 45.8	N.W.	+42	+3		
			S.	—52 59.5	N.W.	+42	+3		
			Direct.	—52 53.0	N.N.W.	+41	+3		
			S.	—52 46.4	N.N.W.	+41	+3		
			Direct.	—52 54.0	N.	+41	+3		
			S.	—52 52.3	N.	+41	+3		
			Direct.	—52 37.5	N.N.E.	+41	+3		
			S.	—52 44.0	N.N.E.	+41	+3		
			Direct.	—52 42.5	N.E.	+42	+3		
			S.	—52 43.2	N.E.	+42	+3		
			Direct.	—52 42.2	E.N.E.	+38	+3		
			S.	—52 44.7	E.N.E.	+38	+3		
			Direct.	—52 32.0	E.	+37	+3		
			S.	—52 21.5	E.	+37	+3		
			Direct.	—52 31.0	E.S.E.	+9	+3		
			S.	—52 20.1	E.S.E.	+9	+3		
			Direct.	—52 13.2	S.E.	—14	+3		
			S.	—52 22.6	S.E.	—14	+3		
			Direct.	—51 51.7	S.S.E.	—32	+3		
			S.	—52 16.2	S.S.E.	—32	+3		
			Direct.	—51 21.0	S.	—40	+3		
			S.	—51 51.0	S.	—40	+3		
			Direct.	—51 33.0	S.S.W.	—32	+3		
			S.	—51 25.0	S.S.W.	—32	+3		
			Direct.	—51 51.0	S.W.	—14	+3		
			S.	—51 40.7	S.W.	—14	+3		
			Direct.	—52 22.0	W.S.W.	+9	+3		
			S.	—52 12.5	W.S.W.	+9	+3		
			Direct.	—52 46.8	W.	+37	+3		

* Observed on shore;
face west.

Direct.	-53° 34.2
S.	-53 31.8
N.	-53 24.3
N.S.	-53 21.8

Observations of the INCLINATION made in Her Majesty's Ship Terror, with Needle
F. C. B., between April 1841 and August 1842.

Observers Captain FRANCIS RAWDON CROZIER, and Mr. THOMAS MOORE, Mate, R.N.

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Apr. 19.	Hobarton Magnetic Observatory.		Direct.	-70 29.6	Observed on shore.	-35	-70 52 -70 52	Aspareneedle(marked C.) was used as deflector N. and deflector S.: and the magnets of the apparatus as Mag. N. Mag. S. and Mag. N.S.
	-42 52 147 24*	Direct.	-70 25.9		-35			
		Def. N.	-69 33.5		-81			
		Def. S.	-70 17.9		-35			
		Mag. N.S.	-70 09.6		-35			
		Mag. N.	-70 09.9		-35			
		Mag. S.	-70 10.7†		-35			
July 7.	Running out of Storm Bay.		Direct.	-69 46.5	S.E. $\frac{3}{4}$ E.	-32	-35	-71 00 -71 00	Ship steady.
		Def. N.	-69 29.9	S.E. $\frac{3}{4}$ E.	-32	-81			
		Def. S.	-69 38.8	S.E. $\frac{3}{4}$ E.	-32	-35			
8.	-43 03 148 20		Direct.	-69 51.2	S.E. $\frac{3}{4}$ E.	-32	-35	-71 18	Ship very steady.
		Direct.	-70 58.0	W. $\frac{1}{2}$ N.	+27	-35			
		Def. N.	-70 50.4	W. $\frac{1}{2}$ N.	+27	-81			
		Def. S.	-71 02.0	W. $\frac{1}{2}$ N.	+27	-35			
		Direct.	-71 04.0	W. $\frac{1}{2}$ N.	+27	-35			
9.	-42 24 149 30		Direct.	-70 43.3	N.N.W.	+76	-35	-70 44	
		Def. N.	-70 34.1	N.N.W.	+76	-81	-70 10		
		Def. S.	-70 36.0	N.N.W.	+76	-35			
		Direct.	-70 45.5	N.N.W.	+76	-35			
10.	-40 51 149 28		Direct.	-69 42.7	N. by W.	+78	-35	-69 05 -69 05	Ship very steady.
		Def. N.	-69 19.7	N. by W.	+78	-81			
		Def. S.	-69 37.7	N. by W.	+78	-35			
		Direct.	-69 47.0	N. by W.	+78	-35			
11.	-38 17 150 22		Direct.	-67 41.3	N. by E.	+73	-35	-66 57 -66 57	Ship very steady.
		Def. N.	-67 23.3	N. by E.	+73	-81			
		Def. S.	-67 07.0	N. by E.	+73	-35			
		Direct.	-67 42.7	N. by E.	+73	-35			

* Observations at Hobarton to obtain corrections for the ship's attraction.

June 22. At anchor	Direct. . .	-70 14.3	W.	Direct. . .	-69 54.9	E.
	Def. N. . .	-69 52.5	W.	Def. N. . .	-69 21.9	E.
	Direct. . .	-69 59.0	W.S.W.	Direct. . .	-70 14.1	E.N.E.
	Def. N. . .	-69 38.4	W.S.W.	Def. N. . .	-69 51.5	E.N.E.
	Direct. . .	-69 24.5	S.W.	Direct. . .	-70 21.4	N.E.
	Def. N. . .	-68 49.9	S.W.	Def. N. . .	-70 12.0	N.E.
	Direct. . .	-68 57.0	S.S.W.	Direct. . .	-70 31.6	N.N.E.
	Def. N. . .	-68 38.2	S.S.W.	Def. N. . .	-70 16.9	N.N.E.
	Direct. . .	-68 37.5	S.	Direct. . .	-70 48.2	N.
	Def. N. . .	-68 30.9	S.	Def. N. . .	-70 28.2	N.
	Direct. . .	-68 40.0	S.S.E.	Direct. . .	-71 01.8	N.N.W.
	Def. N. . .	-68 14.3	S.S.E.	Def. N. . .	-70 42.3	N.N.W.
	Direct. . .	-68 52.2	S.E.	Direct. . .	-70 59.6	N.W.
	Def. N. . .	-68 26.4	S.E.	Def. N. . .	-70 13.9	N.W.
	Direct. . .	-69 22.6	E.S.E.	Direct. . .	-70 47.6	W.N.W.
	Def. N. . .	-68 59.1	E.S.E.	Def. N. . .	-70 32.5	W.N.W.

† Observed on shore; face west.

Direct.	-70 39.9	Mag. N.S. . .	-70 54.4	Mag. S.	-70 39.9
Direct.	-70 40.2	Mag. N.	-70 54.4	Def. N.	-71 25.9
Def. S.	-70 40.0				

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
July 12.	-37° 28'	151° 30'	Direct.	-66° 45.1	N.E. $\frac{1}{2}$ N.	+63	-35	-66 22 -66 22	Ship steering steadily.
			Def. N.	-66 40.0	N.E. $\frac{1}{2}$ N.	+63	-81		
			Def. S.	-66 19.1	N.E. $\frac{1}{2}$ N.	+63	-35		
13.	-36 21	151 39	Direct.	-66 49.7	N.E. $\frac{1}{2}$ N.	+63	-35	-66 11 -66 11	Ship unsteady.
			Direct.	-66 24.5	N.N.W. $\frac{1}{4}$ W.	+69	-35		
			Def. N.	-66 35.9	N.N.W. $\frac{1}{4}$ W.	+69	-81		
14.	-34 06	151 19	Direct.	-66 29.1	N.N.W. $\frac{1}{4}$ W.	+69	-35	-62 58 -62 58	Steering steadily.
			Direct.	-63 25.9	N.	+67	-35		
			Def. N.	-63 08.4	N.	+67	-81		
19.	Garden Island, Sydney.	-33 51 151 17	Def. S.	-63 11.9	N.	+67	-35	-62 59 -62 59	
			Direct.	-63 29.6	N.	+67	-35		
			Direct.	-62 29.3*		-35		
30.	At anchor.		Def. N.	-61 36.7		-81	-63 00 -63 16	
			Def. S.	-62 29.8		-35		
			Mag. N.	-62 15.2		-35		
Aug. 4.			Mag. S.	-62 17.4		-35	-62 57 -63 16	
			Mag. N.S.	-62 14.0		-35		
			Direct.	-62 28.8		-35		
5.	Running out of harbour.		Direct.	-62 36.6	w. by s.	+12	-35	-62 49 -62 56	Head swell on the 5th, steering badly.
			Direct.	-63 06.1	w.	+25	-35		
			Direct.	-63 03.3	w. $\frac{1}{2}$ s.	+18	-35		
5.			Direct.	-62 06.4	s.w. by w.	-16	-35	-62 30 -62 40	
			Direct.	-62 16.0	s.w. $\frac{1}{2}$ w.	-25	-35		
			Direct.	-62 52.9	E. by N. $\frac{1}{2}$ N.	+39	-35		
6.	-34 01	153 17	Def. N.	-62 14.1	E. by N. $\frac{1}{2}$ N.	+39	-81	-62 30 -62 30	Steering badly.
			Def. S.	-62 25.4	E. by N. $\frac{1}{2}$ N.	+39	-35		
			Mag. N.	-62 34.4	E. by N. $\frac{1}{2}$ N.	+39	-35		
7.	-33 56	156 38	Mag. S.	-62 44.6	E. by N. $\frac{1}{2}$ N.	+39	-35	-61 46 -61 46	Steering wildly.
			Direct.	-62 43.5	E. by N. $\frac{1}{2}$ N.	+39	-35		
			Direct.	-62 31.3	E. by N.	+35	-25		
8.	-33 31	160 20	Def. N.	-62 06.1	E. by N.	+35	-81	-61 04 -61 04	Steering tolerably.
			Def. S.	-62 28.2	E. by N.	+35	-35		
			Direct.	-62 27.2	E. by N.	+35	-35		
9.	-33 42	164 05	Direct.	-62 23.7	E. by N.	+35	-35	-60 52 -60 52	Steering badly.
			Def. N.	-62 02.6	E. by N.	+35	-81		
			Def. S.	-62 02.8	E. by N.	+35	-35		
			Direct.	-62 24.1	E. by N.	+35	-35	-60 52 -60 52	
			Direct.	-61 40.6	E. by N.	+35	-35		
			Def. N.	-61 09.9	E. by N.	+35	-81		
			Def. S.	-61 40.7	E. by N.	+35	-35	-60 52 -60 52	
			Direct.	-61 47.6	E. by N.	+35	-35		
			Def. N.	-61 17.4	E. by N.	+35	-35		
			Def. S.	-60 38.1	E. by N.	+35	-81	-60 52 -60 52	
			Direct.	-60 22.1	E. by N.	+35	-35		
			Direct.	-61 14.2	E. by N.	+35	-35		
			Def. N.	-60 40.6	E.	+26	-35	-60 52 -60 52	
			Def. S.	-60 17.2	E.	+26	-81		
			Direct.	-60 30.8	E.	+26	-35		
			Def. S.	-60 37.7	E.	+26	-35		
			Direct.						
			Direct.						

* Observed on shore; face west. { Direct. -62 52.9 | Mag. N. -63 00.8 | Mag. N. and S. -63 03.7
 { Def. N. -63 00.7 | Mag. S. -62 57.0 | Direct. -62 52.3
 { Def. S. -62 52.4

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Aug. 10.	-33 47	166 39	Direct.	-59 59.9	E. by N. 1/2 N.	+39	-35	-60 02	Long swell, motion quick, steering steadily.
			Def. N.	-59 56.7	E. by N. 1/2 N.	+39	-81		
			Def. S.	-59 38.1	E. by N. 1/2 N.	+39	-35		
	-33 42	166 36	Direct.	-60 02.2	E. by N. 1/2 N.	+39	-35	-59 55	
			Direct.	-59 42.3	E.	+26	-35		
			Def. N.	-59 00.3	E.	+26	-81		
			Def. S.	-59 42.7	E.	+26	-35	-59 49	
			Mag. N.	-59 21.1	E.	+26	-35		
			Mag. S.	-59 39.9	E.	+26	-35		
11.	-33 34	167 37	Direct.	-60 02.2	E. by N.	+36	-35	-59 49	
			Direct.	-60 13.9	N.E. by E.	+50	-35		
			Def. N.	-59 18.4	N.E. by E.	+50	-81		
			Def. S.	-60 03.5	N.E. by E.	+50	-35	-59 58	
			Mag. N.	-60 04.1	N.E. by E.	+50	-35		
			Mag. S.	-60 01.4	N.E. by E.	+50	-35		
			Mag. N.S.	-59 54.0	N.E. by E.	+50	-35	-60 07	
			Direct.	-60 09.5	N.E. by E.	+50	-35		
	-33 31	167 41	Direct.	-59 53.1	E.	+26	-35		
12.	-33 00	169 20	Def. N.	-59 17.2	E.	+26	-81	-58 43	
			Direct.	-58 59.8	E.N.E.	+43	-35		
			Def. N.	-58 22.6	E.N.E.	+43	-81		
			Def. S.	-58 56.9	E.N.E.	+43	-35	-58 43	
			Mag. N.	-58 36.5	E.N.E.	+43	-35		
			Mag. S.	-58 23.1	E.N.E.	+43	-35		
			Direct.	-58 56.7	E.N.E.	+43	-35	-58 43	
			Direct.	-59 10.4	N.E.	+52	-35		
			Mag. N.S.	-58 40.5	N.E.	+52	-35		
13.	-32 12	170 27	Direct.	-59 09.1	N.E.	+52	-35	-57 13	
			Direct.	-56 21.9	S.E. by E.	-10	-35		
			Def. N.	-56 00.5	S.E. by E.	-10	-81		
			Def. S.	-56 18.1	S.E. by E.	-10	-35	-57 28	
14.	-32 11	171 20	Direct.	-56 24.6	S.E. by E.	-10	-35		
			Direct.	-56 58.5	S.E. by E.	-10	-35		
			Def. N.	-56 11.3	S.E. by E.	-10	-81	-57 36	
			Def. S.	-56 40.0	S.E. by E.	-10	-35		
			Mag. N.	-56 46.1	S.E. by E.	-10	-35		
			Mag. N.S.	-56 55.9	S.E. by E.	-10	-35	-58 17	
			Mag. S.	-56 49.8	S.E. by E.	-10	-35		
			Direct.	-56 51.0	S.E. by E.	-10	-35		
15.	-33 55	171 59	Direct.	-57 39.5	E. by S.	+14	-35	-58 24	
			Def. N.	-57 06.2	E. by S.	+14	-81		
			Direct.	-58 22.1	E. 1/2 N.	+32	-35		
			Def. N.	-57 57.4	E. 1/2 N.	+32	-81	-58 14	
			Direct.	-58 20.8	E. 1/2 N.	+32	-35		
			Direct.	-57 57.7	E.S.E.	+4	-35		
	-33 58	172 06	Def. N.	-57 32.5	E.S.E.	+4	-81	-58 14	
			Def. S.	-57 22.1	E.S.E.	+4	-35		
			Mag. N.	-57 24.9	E.S.E.	+4	-35		
			Mag. N.S.	-57 30.0	E.S.E.	+4	-35	-58 48	
			Mag. S.	-57 22.9	E.S.E.	+4	-35		
			Direct.	-58 00.5	E.S.E.	+4	-35		
16.	-34 15	172 50	Direct.	-59 25.6	N.W. 1/2 N.	+51	-35	-58 48	
			Def. N.	-59 00.3	N.W. 1/2 N.	+51	-81		
			Def. S.	-58 46.2	N.W. 1/2 N.	+51	-35		
			Mag. N.	-59 01.4	N.W. 1/2 N.	+51	-35	-58 48	
			Mag. N.S.	-58 55.8	N.W. 1/2 N.	+51	-35		

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Aug. 16.	—34 15	172 50	Mag. S.	—58 08.6	N.W. $\frac{1}{2}$ N.	+51	—35	—58 48 } —58 48	Head sea, steering badly, ship unsteady.
			Direct.	—59 24.6	N.W. $\frac{1}{2}$ N.	+51	—35		
			Direct.	—58 26.9	E. by S. $\frac{1}{2}$ S.	+7	—35		
			Mag. N.S.	—58 04.7	E. by S. $\frac{1}{2}$ S.	+7	—35		
			Direct.	—58 23.1	E. by S. $\frac{1}{2}$ S.	+7	—35	—58 46 }	
17.	—34 24	173 43	Direct.	—58 33.2	E. by S. $\frac{1}{2}$ S.	+7	—35		
			Def. N.	—58 21.7	E. by S. $\frac{1}{2}$ S.	+7	—81		
			Def. S.	—58 23.3	E. by S. $\frac{1}{2}$ S.	+7	—35		
			Mag. N.	—58 25.9	E. by S. $\frac{1}{2}$ S.	+7	—35	—59 00 } —59 00	Strong wind, a good deal of motion.
			Mag. N.S.	—58 25.5	E. by S. $\frac{1}{2}$ S.	+7	—35		
			Mag. S.	—58 21.4	E. by S. $\frac{1}{2}$ S.	+7	—35		
			Direct.	—58 26.8	E. by S. $\frac{1}{2}$ S.	+7	—35		
18.	Running into the Bay of Islands.		Direct.	—58 20.6	S.W.	—30	—35	—59 36 } —59 36	Heavy sea, steering wildly.
			Def. N.	—58 08.4	S.W.	—30	—81		
			Direct.	—58 19.2	S.W.	—30	—35		
			Direct.	—59 00.4			—35		
Oct. 21.	Bay of Islands, New Zealand.		Def. N.	—57 57.5			—81	—59 18	Magnetic observatory.
	—35 16	174 00	Def. S.	—59 05.1			—35	—59 40	
			Mag. N.	—58 41.0			—35	—59 16	
			Mag. N.S.	—58 43.6			—35	—59 19	
			Mag. S.	—58 38.4			—35	—59 13	
			Direct.	—59 01.0	Observed on shore.		—35	—59 36	
			Direct.	—59 00.8			—35	—59 36	
			Def. N.	—57 58.4			—81	—59 19	
			Def. S.	—58 59.2			—35	—59 34	
			Mag. N.	—58 38.7			—35	—59 14	
			Mag. N.S.	—58 40.3			—35	—59 15	
			Mag. S.	—58 37.1			—35	—59 12	
			Direct.	—59 02.2*			—35	—59 37	
Nov. 23.	Running out of Bay of Islands, about one mile from Piercy Island.		Direct.	—57 50.2	S.E. by E.	—17	—35	—58 42	Very steady.
			Direct.	—58 34.3	E. by S.	+11	—35	—58 58	
			Def. N.	—57 57.1	E. by S.	+11	—81	—59 07	
			Def. S.	—58 40.9	E. by S.	+11	—35	—59 05	
			Direct.	—58 34.2	E. by S.	+11	—35	—58 58	Ship unsteady.
24.	—36 20	177 27	Direct.	—59 13.5	E.S.E.	—5	—35	—59 53	
			Def. N.	—58 23.2	E.S.E.	—5	—81	—59 49	
			Def. S.	—58 53.7	E.S.E.	—5	—35	—59 34	
			Mag. N.	—58 39.2	E.S.E.	—5	—35	—59 19	
			Mag. N.S.	—58 37.0	E.S.E.	—5	—35	—59 17	
			Mag. S.	—58 37.3	E.S.E.	—5	—35	—59 17	
			Direct.	—59 14.7	E.S.E.	—5	—35	—59 55	
			Direct.	—59 41.1	S.E. by S.	—40	—35	—60 56	Head sea, table unsteady.
25.	—38 00	179 34	Def. N.	—58 31.6	S.E. by S.	—40	—81	—60 33	
			Def. S.	—58 54.4	S.E. by S.	—40	—35	—60 09	
			Mag. N.	—58 54.0	S.E. by S.	—40	—35	—60 09	
			Mag. N.S.	—59 02.5	S.E. by S.	—40	—35	—60 17	
			Mag. S.	—58 55.4	S.E. by S.	—40	—35	—60 10	
			Direct.	—59 37.6	S.E. by S.	—40	—35	—60 53	
	—38 27	179 59	Direct.	—60 11.8	S.E. by E. $\frac{1}{2}$ E.	—12	—35	—60 59	

* Observed on shore;
face west.

Direct. . .	Oct. 21.	—59 47.6	Oct. 29.	—59 54.6
Def. N. . .	Oct. 21.	—60 13.9	Oct. 29.	—60 10.7
Def. S. . .	Oct. 21.	—60 00.5	Oct. 29.	—60 06.3
Mag. N. . .	Oct. 21.	—60 10.3	Oct. 29.	—60 13.1
Mag. N.S.	Oct. 21.	—60 13.7	Oct. 29.	—60 01.2
Mag. S. . .	Oct. 21.	—60 07.4	Oct. 29.	—60 12.8
Direct. . .	Oct. 21.	—59 48.6	Oct. 29.	—59 58.5

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Nov. 25.	-38 27	179 59	Def. N.	-59 06.2	S.E. by E. $\frac{1}{2}$ E.	-12	-81	-60 39	Head sea, table unsteady.
			Def. S.	-60 03.3	S.E. by E. $\frac{1}{2}$ E.	-12	-35	-60 50	
			Mag. N.	-59 51.3	S.E. by E. $\frac{1}{2}$ E.	-12	-35	-60 38	
			Mag. N.S.	-59 46.0	S.E. by E. $\frac{1}{2}$ E.	-12	-35	-60 33	
			Mag. S.	-60 00.6	S.E. by E. $\frac{1}{2}$ E.	-12	-35	-60 48	
26.	-38 57 -38 48	181 18 182 05	Direct.	-60 12.9	S.E. by E. $\frac{1}{2}$ E.	-12	-35	-61 00	Heavy sea, much motion, observations not satisfactory.
			Direct.	-60 00.6	E.S.E.	-5	-35	-60 41	
			Direct.	-61 08.6	E.S.E.	-5	-35	-61 49	
			Def. N.	-60 00.6	E.S.E.	-5	-81	-61 27	
			Def. S.	-60 37.7	E.S.E.	-5	-35	-61 18	
			Direct.	-60 11.9	S.E.	-31	-35	-61 18	Tolerably steady.
			Def. N.	-59 07.5	S.E.	-31	-81	-61 00	
			Def. S.	-59 48.8	S.E.	-31	-35	-60 55	
			Mag. N.	-59 36.8	S.E.	-31	-35	-60 43	
			Mag. N.S.	-59 48.5	S.E.	-31	-35	-60 54	
			Mag. S.	-59 38.9	S.E.	-31	-35	-60 45	-61 21.
			Direct.	-60 08.7	S.E.	-31	-35	-61 15	
			Direct.	-61 14.4	E.S.E.	-5	-35	-61 54	
			Def. N.	-60 13.3	E.S.E.	-5	-81	-61 39	
			Def. S.	-60 46.2	E.S.E.	-5	-35	-61 26	
27.			Mag. N.	-60 42.2	E.S.E.	-5	-35	-61 22	Head swell with considerable motion.
			Mag. N.S.	-60 51.5	E.S.E.	-5	-35	-61 31	
			Mag. N.	-60 06.7	E.S.E.	-5	-35	-61 47	
			Direct.	-61 13.9	E.S.E.	-5	-35	-61 54	
			Direct.	-60 24.6	S.E. by E.	-20	-35	-61 20	
			Def. N.	-59 12.0	S.E. by E.	-20	-81	-60 53	Tolerably steady, steering well.
			Def. S.	-60 30.1	S.E. by E.	-20	-35	-61 25	
			Mag. N.	-59 54.5	S.E. by E.	-20	-35	-60 50	
			Mag. N.S.	-59 55.1	S.E. by E.	-20	-35	-60 50	
			Mag. S.	-60 15.2	S.E. by E.	-20	-35	-61 10	
			Direct.	-60 31.5	S.E. by E.	-20	-35	-61 27	Slight motion.
			Direct.	-59 41.2	S. by E. $\frac{1}{2}$ E.	-56	-35	-61 12	
			Direct.	-59 41.8	S. $\frac{1}{2}$ E.	-61	-35	-61 18	
			Direct.	-59 51.6	S. by E.	-60	-35	-61 27	
			Def. N.	-59 13.4	S. by E.	-60	-81	-61 34	
28.			Def. S.	-59 59.5	S. by E.	-60	-35	-61 34	Table steady.
			Mag. N.	-59 23.9	S. by E.	-60	-35	-60 59	
			Mag. N.S.	-59 30.9	S. by E.	-60	-35	-61 06	
			Mag. S.	-59 44.6	S. by E.	-60	-35	-61 20	
			Direct.	-59 55.0	S. by E.	-60	-35	-61 30	
			Direct.	-61 14.0	E.S.E.	-5	-35	-61 54	-61 15
			Direct.	-60 47.6	S.E.	-33	-35	-61 56	
			Def. N.	-59 58.5	S.E.	-33	-81	-61 53	
			Def. S.	-60 57.6	S.E.	-33	-35	-62 06	
			Mag. N.	-60 28.1	S.E.	-33	-35	-61 36	
			Mag. N.S.	-60 29.6	S.E.	-33	-35	-61 38	-61 56
			Mag. S.	-60 46.0	S.E.	-33	-35	-61 54	
			Direct.	-60 47.3	S.E.	-33	-35	-61 55	
			Direct.	-60 51.2	S.S.E. $\frac{1}{2}$ E.	-48	-35	-62 14	
			Def. N.	-59 43.5	S.S.E. $\frac{1}{2}$ E.	-48	-81	-61 53	
			Def. S.	-60 55.4	S.S.E. $\frac{1}{2}$ E.	-48	-35	-62 18	Slight motion, steering well.
			Mag. N.	-60 13.9	S.S.E. $\frac{1}{2}$ E.	-48	-35	-61 37	
			Mag. N.S.	-60 30.0	S.S.E. $\frac{1}{2}$ E.	-48	-35	-61 53	
			Mag. S.	-60 30.1	S.S.E. $\frac{1}{2}$ E.	-48	-35	-61 53	
			Direct.	-60 54.0	S.S.E. $\frac{1}{2}$ E.	-48	-35	-62 17	

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Nov. 29.	—41 34	183 40	Direct.	—61 27.5	s. by E.	—60	—35	—63 03	Slight motion, steering well.
			Def. N.	—60 27.5	s. by E.	—60	—81	—62 49	
			Def. S.	—61 31.3	s. by E.	—60	—35	—63 06	
			Mag. N.	—61 37.1	s. by E.	—60	—35	—63 12	
			Mag. N.S.	—61 03.5	s. by E.	—60	—35	—62 39	
			Mag. S.	—60 58.9	s. by E.	—60	—35	—62 34	—62 57
			Direct.	—61 44.5	s. by E.	—60	—35	—63 19	
	—42 40	183 46	Direct.	—62 23.7	s.	—64	—35	—64 03	
			Def. N.	—61 02.1	s.	—64	—81	—63 27	
			Def. S.	—62 08.6	s.	—64	—35	—63 48	
			Mag. N.	—61 54.9	s.	—64	—35	—63 34	—63 46
			Mag. N.S.	—62 03.6	s.	—64	—35	—63 43	
			Mag. S.	—62 01.2	s.	—64	—35	—63 40	
			Direct.	—62 29.6	s.	—64	—35	—64 09	
30.	—43 33	183 10	Direct.	—63 26.2	s. $\frac{1}{2}$ w.	—63	—35	—65 04	
			Def. N.	—62 29.3	s. $\frac{1}{2}$ w.	—63	—81	—64 53	
			Def. S.	—63 58.6	s. $\frac{1}{2}$ w.	—63	—35	—65 37	
			Mag. N.	—63 16.8	s. $\frac{1}{2}$ w.	—63	—35	—64 55	
			Mag. N.S.	—62 58.2	s. $\frac{1}{2}$ w.	—63	—35	—64 36	
			Mag. S.	—63 46.3	s. $\frac{1}{2}$ w.	—63	—35	—65 24	—65 22
			Direct.	—63 26.2	s. $\frac{1}{2}$ w.	—63	—35	—65 04	
	—43 50	183 00	Direct.	—63 43.0	s. by w.	—62	—35	—65 20	
	—44 15		Direct.	—64 07.3	s. by w.	—62	—35	—65 44	
			Def. N.	—63 29.4	s. by w.	—62	—81	—65 52	
			Def. S.	—63 59.7	s. by w.	—62	—35	—65 37	Cross sea, motion slight.
			Mag. N.	—63 51.9	s. by w.	—62	—35	—65 29	
			Mag. N.S.	—63 52.9	s. by w.	—62	—35	—65 30	
			Mag. S.	—63 58.1	s. by w.	—62	—35	—65 35	
			Direct.	—64 11.4	s. by w.	—62	—35	—65 48	
Dec. 1.	—45 30	183 12	Direct.	—65 46.1	s.e. by E.	—24	—35	—66 45	—66 43
			Def. N.	—65 01.6	s.e. by E.	—24	—81	—66 47	
			Def. S.	—65 19.5	s.e. by E.	—24	—35	—66 19	
			Mag. N.	—65 14.3	s.e. by E.	—24	—35	—66 13	
			Mag. N.S.	—65 31.7	s.e. by E.	—24	—35	—66 31	
			Mag. S.	—66 00.8	s.e. by E.	—24	—35	—67 00	Much pitching, steering well.
			Direct.	—65 40.0	s.e. by E.	—24	—35	—66 39	
	—45 48	183 25	Direct.	—65 43.9	s.e. $\frac{1}{2}$ E.	—31	—35	—66 50	
			Def. N.	—64 55.1	s.e. $\frac{1}{2}$ E.	—31	—81	—66 47	
			Def. S.	—65 36.8	s.e. $\frac{1}{2}$ E.	—31	—35	—66 43	
			Mag. N.	—65 54.2	s.e. $\frac{1}{2}$ E.	—31	—35	—67 00	—67 32
			Mag. N.S.	—65 40.5	s.e. $\frac{1}{2}$ E.	—31	—35	—66 47	
			Mag. S.	—65 49.2	s.e. $\frac{1}{2}$ E.	—31	—35	—66 55	
			Direct.	—65 47.4	s.e. $\frac{1}{2}$ E.	—31	—35	—66 53	
2.	—47 13	184 30	Direct.	—66 30.4	s.e. by E. $\frac{1}{2}$ E.	—18	—35	—67 23	
			Def. N.	—65 41.8	s.e. by E. $\frac{1}{2}$ E.	—18	—81	—67 21	Ship pitching, but steering well.
			Def. S.	—66 43.2	s.e. by E. $\frac{1}{2}$ E.	—18	—35	—67 36	
			Mag. N.	—66 31.4	s.e. by E. $\frac{1}{2}$ E.	—18	—35	—67 24	
			Mag. N.S.	—66 30.3	s.e. by E. $\frac{1}{2}$ E.	—18	—35	—67 23	
			Mag. S.	—66 37.0	s.e. by E. $\frac{1}{2}$ E.	—18	—35	—67 30	
			Direct.	—66 34.6	s.e. by E. $\frac{1}{2}$ E.	—18	—35	—67 28	—67 32
	—47 39	184 55	Direct.	—66 54.4	s.e. by E.	—26	—35	—67 55	
			Def. N.	—65 36.6	s.e. by E.	—26	—81	—67 24	
			Def. S.	—66 40.1	s.e. by E.	—26	—35	—67 41	
			Mag. N.	—66 21.5	s.e. by E.	—26	—35	—67 23	
			Mag. N.S.	—66 35.4	s.e. by E.	—26	—35	—67 36	Very steady.
			Mag. S.	—66 34.7	s.e. by E.	—26	—35	—67 36	
			Direct.	—66 47.4	s.e. by E.	—26	—35	—67 48	

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 3.	—48 18	185 54	Direct.	—67 34.4	S.E. by E.	—27	—35	—68 36	° ' }
			Def. N.	—66 19.7	S.E. by E.	—27	—81	—68 08	
			Def. S.	—67 23.9	S.E. by E.	—27	—35	—68 26	
			Mag. N.	—67 17.7	S.E. by E.	—27	—35	—68 20	
			Mag. N.S.	—67 21.9	S.E. by E.	—27	—35	—68 24	
			Mag. S.	—67 17.1	S.E. by E.	—27	—35	—68 19	
			Direct.	—67 38.6	S.E. by E.	—27	—35	—68 41	
			Direct.	—67 46.6	E.S.E.	—11	—35	—68 33	
			Direct.	—68 01.5	S.E. by E. $\frac{1}{2}$ E.	—19	—35	—68 56	
			Def. N.	—67 07.3	S.E. by E. $\frac{1}{2}$ E.	—19	—81	—68 47	
	—48 48 —49 05	186 38 186 54	Def. S.	—67 55.0	S.E. by E. $\frac{1}{2}$ E.	—19	—35	—68 49	—68 40 } Very steady.
			Mag. N.	—67 49.5	S.E. by E. $\frac{1}{2}$ E.	—19	—35	—68 44	
			Mag. N.S.	—67 44.7	S.E. by E. $\frac{1}{2}$ E.	—19	—35	—68 39	
			Mag. S.	—67 53.8	S.E. by E. $\frac{1}{2}$ E.	—19	—35	—68 48	
			Direct.	—68 54.3	S.E. by E. $\frac{1}{2}$ E.	—19	—35	—69 48	
4.	—49 24	187 23	Direct.	—68 53.5	N.E. by E.	+54	—35	—68 35	
			Direct.	—68 33.0	E. $\frac{1}{2}$ N.	+26	—35	—68 42	
			Direct.	—68 29.8	E.	+20	—35	—68 45	
			Direct.	—68 42.3	E.N.E.	+45	—35	—68 32	
			Direct.	—68 28.7	W.S.W.	—12	—35	—69 16	
			Direct.	—68 45.7	W.	+20	—35	—69 01	
			Direct.	—68 52.2	E.	+20	—35	—69 07	
			Def. N.	—67 28.0	E.	+20	—81	—68 29	
			Direct.	—68 48.0	E. by S.	+4	—35	—69 19	
			Def. N.	—67 29.5	E. by S.	+4	—81	—68 47	
	—49 23	188 54	Def. S.	—68 52.0	E. by S.	+4	—35	—69 23	—68 59 } Swell from northward. Table steady.
			Mag. N.	—68 29.0	E. by S.	+4	—35	—69 00	
			Mag. N.S.	—68 28.1	E. by S.	+4	—35	—68 59	
			Mag. S.	—68 42.7	E. by S.	+4	—35	—69 14	
			Direct.	—69 01.0	E. by S.	+4	—35	—69 32	
			Direct.	—68 43.9	E. by S.	+4	—35	—69 15	
			Def. N.	—67 31.6	E. by S.	+4	—81	—68 49	
			Def. S.	—68 42.2	E. by S.	+4	—35	—69 13	
			Mag. N.	—68 42.6	E. by S.	+4	—35	—69 14	
			Mag. N.S.	—68 40.1	E. by S.	+4	—35	—69 11	
5.	—49 38	189 44	Mag. S.	—68 30.6	E. by S.	+4	—35	—69 02	
			Direct.	—68 44.2	E. by S.	+4	—35	—69 15	
			Direct.	—68 15.9	E. by S.	+4	—35	—68 47	
			Def. N.	—67 25.5	E. by S.	+4	—81	—68 43	
			Def. S.	—68 06.1	E. by S.	+4	—35	—68 37	
			Mag. N.	—67 57.8	E. by S.	+4	—35	—68 29	
			Mag. N.S.	—68 01.6	E. by S.	+4	—35	—68 33	
			Mag. S.	—68 22.7	E. by S.	+4	—35	—68 54	
			Direct.	—68 14.3	E. by S.	+4	—35	—68 45	
	—49 50	190 46	Direct.	—68 12.9	E. by S.	+4	—35	—68 44	
			Def. N.	—67 22.6	E. by S.	+4	—81	—68 40	
			Def. S.	—68 09.6	E. by S.	+4	—35	—68 41	
			Mag. N.	—68 07.4	E. by S.	+4	—35	—68 38	
			Mag. N.S.	—68 05.2	E. by S.	+4	—35	—68 36	
			Mag. S.	—68 21.5	E. by S.	+4	—35	—68 53	
			Direct.	—68 16.3	E. by S.	+4	—35	—68 47	
			Direct.	—68 09.8	E. by S.	+4	—35	—68 41	
			Direct.	—68 17.0	E. by S.	+4	—35	—68 48	
	—50 02 —50 08	191 21 191 39	Def. N.	—67 22.2	E. by S.	+4	—81	—68 39	—68 43 } Swell from northward. Table steady.
			Def. S.	—68 16.8	E. by S.	+4	—35	—68 48	
			Mag. N.	—68 09.2	E. by S.	+4	—35	—68 40	
			Mag. N.S.	—68 08.4	E. by S.	+4	—35	—68 39	
			Mag. S.	—68 18.2	E. by S.	+4	—35	—68 49	

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 7.	-50 32	191 52	Direct.	-68 24.2	S.E. by E.	-27	-35	-69 26	Table steady.
			Def. N.	-67 47.4	S.E. by E.	-27	-81	-69 35	
			Def. S.	-68 18.1	S.E. by E.	-27	-35	-69 20	
			Mag. N.	-68 02.0	S.E. by E.	-27	-35	-69 04	
			Mag. N.S.	-67 50.3	S.E. by E.	-27	-35	-68 52	
			Mag. S.	-68 07.9	S.E. by E.	-27	-35	-69 10	
	-50 45	192 19	Direct.	-68 28.1	S.E. by E.	-27	-35	-69 30	
			Direct.	-68 31.2	S.E. $\frac{1}{2}$ E.	-35	-35	-69 41	
			Def. N.	-67 31.3	S.E. $\frac{1}{2}$ E.	-35	-81	-69 27	
			Def. S.	-68 08.4	S.E. $\frac{1}{2}$ E.	-35	-35	-69 18	
			Mag. N.	-68 39.3	S.E. $\frac{1}{2}$ E.	-35	-35	-69 49	
			Mag. N.S.	-68 30.9	S.E. $\frac{1}{2}$ E.	-35	-35	-69 41	
8.	-51 37	194 00	Mag. S.	-68 13.2	S.E. $\frac{1}{2}$ E.	-35	-35	-69 23	
			Direct.	-68 30.3	S.E. $\frac{1}{2}$ E.	-35	-35	-69 40	
			Direct.	-69 18.9	E. by S.	+ 4	-35	-69 50	
			Def. N.	-68 23.8	E. by S.	+ 4	-81	-69 41	
			Def. S.	-69 20.4	E. by S.	+ 4	-35	-69 51	
			Mag. N.	-69 19.6	E. by S.	+ 4	-35	-69 51	
	-52 00	194 53	Mag. N.S.	-69 13.8	E. by S.	+ 4	-35	-69 45	
			Mag. S.	-69 31.4	E. by S.	+ 4	-35	-70 02	
			Direct.	-69 22.4	E. by S.	+ 4	-35	-69 53	
			Direct.	-69 24.6	E. by S.	+ 4	-35	-69 56	
			Direct.	-69 29.8	E. by S.	+ 4	-35	-70 01	
			Def. N.	-68 30.1	E. by S.	+ 4	-81	-69 47	
9.	-52 14	197 49	Def. S.	-69 17.1	E. by S.	+ 4	-35	-69 48	
			Mag. N.	-69 08.9	E. by S.	+ 4	-35	-69 40	
			Mag. N.S.	-69 11.7	E. by S.	+ 4	-35	-69 43	
			Mag. S.	-69 29.7	E. by S.	+ 4	-35	-70 01	
			Direct.	-69 27.0	E. by S.	+ 4	-35	-69 58	
			Direct.	-69 41.0	E. by S.	+ 4	-35	-70 12	
	-52 32	198 31	Def. N.	-68 37.6	E. by S.	+ 4	-81	-69 55	Motion quick, steering wild. Strong wind, heavy sea.
			Def. S.	-69 29.3	E. by S.	+ 4	-35	-70 00	
			Mag. N.	-69 38.3	E. by S.	+ 4	-35	-70 09	
			Mag. N.S.	-69 56.9	E. by S.	+ 4	-35	-70 28	
			Mag. S.	-69 35.8	E. by S.	+ 4	-35	-70 07	
			Direct.	-69 42.6	E. by S.	+ 4	-35	-70 14	
10.	-53 01	202 16	Direct.	-69 41.2	E. by S.	+ 4	-35	-70 12	
			Direct.	-69 47.1	E. by S.	+ 4	-35	-70 18	
			Mag. N.S.	-69 19.7	E. by S.	+ 4	-35	-69 51	
			Direct.	-69 56.5	E. by S.	+ 4	-35	-70 28	
			Direct.	-69 53.3	E. $\frac{1}{2}$ N.	+26	-35	-70 02	
			Def. N.	-68 59.6	E. $\frac{1}{2}$ N.	+26	-81	-69 55	
11.	-52 51	203 56	Def. S.	-69 59.1	E. $\frac{1}{2}$ N.	+26	-35	-70 08	Head sea, table not very steady.
			Mag. N.	-69 36.5	E. $\frac{1}{2}$ N.	+26	-35	-69 45	
			Mag. N.S.	-69 30.2	E. $\frac{1}{2}$ N.	+26	-35	-69 39	
			Mag. S.	-69 55.8	E. $\frac{1}{2}$ N.	+26	-35	-70 05	
			Direct.	-70 04.7	E. $\frac{1}{2}$ N.	+26	-35	-70 14	
			Direct.	-70 00.9	E. $\frac{1}{2}$ S.	+12	-35	-70 24	
12.	-52 53	205 07	Direct.	-69 14.2	E.S.E.	-12	-35	-70 01	
			Def. N.	-67 53.9	E.S.E.	-12	-81	-69 27	
			Def. S.	-68 55.7	E.S.E.	-12	-35	-69 43	
			Mag. N.	-68 45.1	E.S.E.	-12	-35	-69 32	
			Mag. N.S.	-68 19.8	E.S.E.	-12	-35	-69 07	
			Mag. S.	-68 53.5	E.S.E.	-12	-35	-69 41	
	-53 12	205 40	Direct.	-69 16.4	E.S.E.	-12	-35	-70 03	A head swell, steering well.
			Direct.	-69 19.3	E.S.E.	-12	-35	-70 06	

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 12.	—53 31	206 14	Direct.	—69 18.8	E.S.E.	—12	—35	—70 06	Table steady, steering wild.
			Def. N.	—68 07.1	E.S.E.	—12	—81	—69 40	
			Def. S.	—69 05.5	E.S.E.	—12	—35	—69 53	A slight motion, steering well.
			Mag. N.	—69 07.0	E.S.E.	—12	—35	—69 54	
			Mag. N.S.	—69 01.4	E.S.E.	—12	—35	—69 51	
			Mag. S.	—69 58.3	E.S.E.	—12	—35	—70 45	
			Direct.	—69 19.5	E.S.E.	—12	—35	—70 06	
			Direct.	—69 18.1	E.S.E.	—12	—35	—70 05	
13.	—54 19	208 24	Def. N.	—68 59.2	E.S.E.	—12	—81	—70 32	
			Def. S.	—69 02.6	E.S.E.	—12	—35	—69 50	
			Mag. N.	—69 16.0	E.S.E.	—12	—35	—70 03	
			Mag. N.S.	—69 16.0	E.S.E.	—12	—35	—70 03	
			Mag. S.	—69 14.0	E.S.E.	—12	—35	—70 01	Table steady, steering wildly.
			Direct.	—69 16.6	E.S.E.	—12	—35	—70 04	
	—54 53	209 24	Direct.	—69 32.9	E.S.E.	—12	—35	—70 20	
			Def. N.	—68 59.0	E.S.E.	—12	—81	—70 32	
			Def. S.	—69 28.8	E.S.E.	—12	—35	—70 16	
			Mag. N.	—69 13.4	E.S.E.	—12	—35	—70 00	
			Mag. N.S.	—69 24.6	E.S.E.	—12	—35	—70 12	
			Mag. S.	—70 00.3	E.S.E.	—12	—35	—70 47	
			Direct.	—69 32.6	E.S.E.	—12	—35	—70 20	
			Direct.	—69 39.5	E.S.E.	—12	—35	—70 27	
			Def. N.	—68 55.8	E.S.E.	—12	—81	—70 29	A heavy sea, ship steering badly.
			Direct.	—68 52.9	S.E. by S.	—55	—35	—70 23	
			Def. N.	—68 11.4	S.E. by S.	—55	—81	—70 27	A swell from the N.W.
			Def. S.	—68 27.0	S.E. by S.	—55	—35	—69 57	
			Mag. N.	—68 59.1	S.E. by S.	—55	—35	—70 29	Ship tolerably steady.
			Mag. N.S.	—68 46.1	S.E. by S.	—55	—35	—70 16	
			Mag. S.	—68 34.0	S.E. by S.	—55	—35	—70 04	
			Direct.	—68 52.1	S.E. by S.	—55	—35	—70 22	
14.	—56 14	211 43	Direct.	—70 08.2	S.E. by S.	—57	—35	—71 40	
			Def. N.	—69 12.9	S.E. by S.	—57	—81	—71 31	
			Def. S.	—70 10.1	S.E. by S.	—57	—35	—71 42	
			Mag. N.	—70 03.2	S.E. by S.	—57	—35	—71 35	
			Mag. N.S.	—70 06.2	S.E. by S.	—57	—35	—71 38	
			Mag. S.	—70 22.0	S.E. by S.	—57	—35	—71 54	
			Direct.	—70 16.1	S.E. by S.	—57	—35	—71 48	
			Direct.	—70 17.8	S.E. by S.	—57	—35	—71 50	
			Def. N.	—69 11.7	S.E. by S.	—57	—81	—71 30	Ship steady.
			Def. S.	—70 12.1	S.E. by S.	—57	—35	—71 44	
			Mag. N.	—70 04.2	S.E. by S.	—57	—35	—71 36	
			Mag. N.S.	—70 00.2	S.E. by S.	—57	—35	—71 32	
			Mag. S.	—70 22.1	S.E. by S.	—57	—35	—71 54	
			Direct.	—70 17.2	S.E. by S.	—57	—35	—71 49	
	—56 30	211 50	Direct.	—70 19.5	S.E. by S.	—57	—35	—71 52	
			Def. N.	—69 29.1	S.E. by S.	—57	—81	—71 47	
			Def. S.	—70 12.7	S.E. by S.	—57	—35	—71 45	
			Mag. N.	—70 05.2	S.E. by S.	—57	—35	—71 37	
			Mag. N.S.	—69 59.7	S.E. by S.	—57	—35	—71 32	
			Mag. S.	—70 35.2	S.E. by S.	—57	—35	—72 07	
			Direct.	—70 22.9	S.E. by S.	—57	—35	—71 55	Ship steady.
			Direct.	—70 42.4	s.	—77	—35	—72 34	
15.	—56 53	212 06	Direct.	—70 50.5	s. by E.	—75	—35	—72 40	
			Direct.	—70 27.5	S.S.E.	—69	—35	—72 12	
			Direct.	—70 30.8	S.E. by S.	—57	—35	—72 03	
			Def. N.	—69 33.8	S.E. by S.	—57	—81	—71 52	

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 15.	—56 53	212 06	Def. S.	—70 26.1	S.E. by S.	—57	—35	—71 58	Ship very steady.
			Mag. N.	—70 12.5	S.E. by S.	—57	—35	—71 45	
			Mag. N.S.	—70 09.6	S.E. by S.	—57	—35	—71 42	
			Mag. S.	—70 34.0	S.E. by S.	—57	—35	—72 06	
			Direct.	—70 30.6	S.E. by S.	—57	—35	—72 03	
			Direct.	—70 37.3	S.S.E.	—69	—35	—72 21	
	—57 16	212 17	Def. N.	—70 00.6	S.S.E.	—69	—81	—72 31	
			Def. S.	—70 54.6	S.S.E.	—69	—35	—72 39	
			Mag. N.	—70 49.7	S.S.E.	—69	—35	—72 34	
			Mag. N.S.	—70 25.1	S.S.E.	—69	—35	—72 09	
			Mag. S.	—70 46.1	S.S.E.	—69	—35	—72 30	
			Direct.	—70 41.5	S.S.E.	—69	—35	—72 26	
16.	—57 44	212 59	Direct.	—71 03.3	S.S.E.	—70	—35	—72 48	Ship steady, steering well.
			Def. N.	—70 29.6	S.S.E.	—70	—81	—73 01	
			Def. S.	—71 08.2	S.S.E.	—70	—35	—72 53	
			Mag. N.	—71 09.6	S.S.E.	—70	—35	—72 55	
			Mag. N.S.	—71 02.8	S.S.E.	—70	—35	—72 48	
			Mag. S.	—71 15.7	S.S.E.	—70	—35	—73 01	
	—58 28	213 08	Direct.	—71 11.9	S.S.E.	—70	—35	—72 57	
			Direct.	—71 56.4	S.S.E.	—70	—35	—73 41	
			Def. N.	—71 20.8	S.S.E.	—70	—81	—73 52	
			Def. S.	—71 52.3	S.S.E.	—70	—35	—73 37	
			Mag. N.	—71 39.7	S.S.E.	—70	—35	—73 25	
			Mag. N.S.	—71 23.9	S.S.E.	—70	—35	—73 09	
17.	—58 44	213 11	Mag. S.	—71 59.3	S.S.E.	—70	—35	—73 44	Ship steady, steering well.
			Direct.	—72 04.4	S.S.E.	—70	—35	—73 49	
			Direct.	—72 16.2	S.S.E.	—70	—35	—74 01	
			Def. N.	—71 24.5	S.S.E.	—70	—81	—73 56	
			Def. S.	—72 22.6	S.S.E.	—70	—35	—74 08	
			Mag. N.	—71 57.1	S.S.E.	—70	—35	—73 42	
	—60 48	213 51	Mag. N.S.	—71 47.8	S.S.E.	—70	—35	—73 33	
			Mag. S.	—72 01.3	S.S.E.	—70	—35	—73 46	
			Direct.	—72 16.1	S.S.E.	—70	—35	—74 01	
			Direct.	—73 24.1	S.S.E.	—73	—35	—75 12	
			Def. N.	—72 33.2	S.S.E.	—73	—81	—75 07	
			Def. S.	—73 29.4	S.S.E.	—73	—35	—75 17	
18.	—61 37	213 54	Mag. N.	—73 01.5	S.S.E.	—73	—35	—74 49	Slight motion, steering well.
			Mag. N.S.	—73 04.2	S.S.E.	—73	—35	—74 52	
			Mag. S.	—73 31.1	S.S.E.	—73	—35	—75 19	
			Direct.	—73 28.8	S.S.E.	—73	—35	—75 17	
			Direct.	—74 10.9	S. $\frac{1}{2}$ E.	—81	—35	—76 07	
			Def. N.	—73 06.9	S. $\frac{1}{2}$ E.	—81	—81	—75 49	
	—62 34	212 34	Def. S.	—73 59.8	S. $\frac{1}{2}$ E.	—81	—35	—75 56	
			Mag. N.	—73 52.8	S. $\frac{1}{2}$ E.	—81	—35	—75 49	
			Mag. N.S.	—73 39.5	S. $\frac{1}{2}$ E.	—81	—35	—75 36	
			Mag. S.	—74 08.6	S. $\frac{1}{2}$ E.	—81	—35	—76 05	
			Direct.	—74 13.1	S. $\frac{1}{2}$ E.	—81	—35	—76 09	
			Direct.	—74 51.6	S. by E.	—79	—35	—76 46	
18.	—62 51	212 50	Def. N.	—73 48.3	S. by E.	—79	—81	—76 28	Ship steady, sailing amongst loose ice.
			Def. S.	—74 43.7	S. by E.	—79	—35	—76 38	
			Mag. N.	—74 23.1	S. by E.	—79	—35	—76 17	
			Mag. N.S.	—74 23.9	S. by E.	—79	—35	—76 18	
			Mag. S.	—74 38.9	S. by E.	—79	—35	—76 33	
			Direct.	—74 46.1	S. by E.	—79	—35	—76 40	
			Direct.	—75 20.5	S. by W.	—79	—35	—77 14	

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 19.	-63 06	210 55	Direct.	-75 52.3	s.s.w.	-74	-35	-77 41	Ship steady, sailing amongst loose ice.
			Direct.	-75 45.3	s. by w.	-80	-35	-77 40	
			Def. N.	-74 56.9	s. by w.	-80	-81	-77 38	
			Def. S.	-75 35.6	s. by w.	-80	-35	-77 31	
			Mag. N.	-75 24.5	s. by w.	-80	-35	-77 20	
			Mag. N.S.	-75 21.2	s. by w.	-80	-35	-77 16	
	-63 21	209 55	Mag. S.	-75 37.8	s. by w.	-80	-35	-77 33	
			Direct.	-75 51.8	s. by w.	-80	-35	-77 47	
			Direct.	-76 08.3	s.w. by s.	-62	-35	-77 45	
			Direct.	-76 00.0	s.s.w. $\frac{1}{2}$ w.	-68	-35	-77 43	
			Direct.	-77 00.8	w. by s. $\frac{3}{4}$ s.	-12	-35	-77 48	
			Direct.	-76 36.2	s.w. by w. $\frac{1}{4}$ w.	-25	-35	-77 36	
20.	-63 36	208 20	Direct.	-76 13.7	s.s.w.	-74	-35	-78 03	Ship steady, steering amongst loose ice.
			Def. N.	-75 10.8	s.s.w.	-74	-81	-77 46	
			Def. S.	-76 04.8	s.s.w.	-74	-35	-77 54	
			Mag. N.	-75 45.5	s.s.w.	-74	-35	-77 35	
			Mag. N.S.	-75 44.8	s.s.w.	-74	-35	-77 34	
			Mag. S.	-76 08.0	s.s.w.	-74	-35	-77 57	
	-63 53	208 32	Direct.	-76 01.3	s. by w.	-80	-35	-77 56	
			Direct.	-76 24.9	s.w. by s.	-62	-35	-78 02	
			Direct.	-76 00.4	s.	-82	-35	-77 57	
			Direct.	-76 45.2	s.w.	-49	-35	-78 09	
			Direct.	-76 24.3	s.w. by s.	-62	-35	-78 01	
			Direct.	-76 45.5	s.w.	-49	-35	-78 10	
21.	-63 53	208 32	Direct.	-76 06.9	s.	-82	-35	-78 04	Ship steady, steering amongst loose ice.
			Def. N.	-75 01.3	s.	-82	-81	-77 44	
			Def. S.	-75 53.4	s.	-82	-35	-77 50	
			Mag. N.	-75 44.5	s.	-82	-35	-77 42	
			Mag. N.S.	-75 36.8	s.	-82	-35	-77 34	
			Mag. S.	-75 57.7	s.	-82	-35	-77 55	
	-64 11	206 35	Direct.	-76 08.9	s.	-82	-35	-78 06	
			Direct.	-76 15.3	s. by w.	-80	-35	-78 10	
			Direct.	-76 32.9	s.s.w.	-75	-35	-78 23	
			Def. N.	-75 31.5	s.s.w.	-75	-81	-78 08	
			Def. S.	-76 29.6	s.s.w.	-75	-35	-78 20	
			Mag. N.	-76 10.0	s.s.w.	-75	-35	-78 00	
22.	-64 51	206 19	Mag. N.S.	-76 01.2	s.s.w.	-75	-35	-77 51	Ship steady, sailing amongst loose ice.
			Mag. S.	-76 00.8	s.s.w.	-75	-35	-77 51	
			Direct.	-76 43.1	s. $\frac{1}{2}$ E.	-82	-35	-78 40	
			Direct.	-76 32.7	s. by E.	-81	-35	-78 29	
			Direct.	-76 41.8	s. by E. $\frac{1}{2}$ E.	-78	-35	-78 35	
			Direct.	-77 03.2	s. $\frac{3}{4}$ E.	-82	-35	-79 00	
	-65 19	205 08	Direct.	-77 06.4	s. by w.	-81	-35	-79 02	
			Def. N.	-76 06.6	s. by w.	-81	-81	-78 49	
			Def. S.	-77 02.2	s. by w.	-81	-35	-78 58	
			Direct.	-77 04.7	s. by w.	-81	-35	-79 01	
			Direct.	-77 29.4	s. $\frac{1}{2}$ w.	-83	-35	-79 27	
			Def. N.	-76 37.6	s. $\frac{1}{2}$ w.	-83	-81	-79 22	
	-65 34	205 00	Def. S.	-77 20.3	s. $\frac{1}{2}$ w.	-83	-35	-79 18	Sailing amongst loose ice, very steady.
			Mag. N.	-77 08.4	s. $\frac{1}{2}$ w.	-83	-35	-79 06	
			Mag. N.S.	-76 59.9	s. $\frac{1}{2}$ w.	-83	-35	-78 58	
			Mag. S.	-77 30.4	s. $\frac{1}{2}$ w.	-83	-35	-79 28	
			Direct.	-77 28.6	s. $\frac{1}{2}$ w.	-83	-35	-79 27	
			Direct.	-77 26.4	s.	-84	-35	-79 25	
			Direct.	-77 27.8	s.	-84	-35	-79 27	
			Def. N.	-76 20.5	s.	-84	-81	-79 05	

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 22.	—65 34	205 00	Def. S.	—77 14.7	S.	—84	—35	—79 14	Sailing amongst loose ice, very steady.
			Mag. N.	—77 04.0	S.	—84	—35	—79 03	
			Mag. N.S.	—76 53.3	S.	—84	—35	—78 52	
			Mag. S.	—77 23.6	S.	—84	—35	—79 23	
23.	—65 47	204 19	Direct.	—77 30.4	S. $\frac{3}{4}$ W.	—82	—35	—79 27	Sailing amongst loose ice, very steady.
			Direct.	—79 54.8	N.E.	+69	—35	—79 21	
			Direct.	—79 45.9	N.E. $\frac{1}{2}$ E.	+64	—35	—79 17	
			Direct.	—79 30.8	N.E. by E.	+59	—35	—79 07	
			Direct.	—77 34.8	S.	—84	—35	—79 34	
			Def. N.	—76 44.1	S.	—84	—81	—79 29	
			Direct.	—79 12.3	E. by N.	+32	—35	—79 15	
			Def. S.	—79 04.9	E. by N.	+32	—35	—79 08	
			Mag. N.S.	—78 44.5	E. by N.	+32	—35	—78 48	
			Mag. S.	—77 15.9*	E. by N.	+32	—35	—77 19	
			Direct.	—78 10.8	S.W. $\frac{1}{4}$ S.	—55	—35	—79 41	Sailing amongst loose ice, very steady.
			Direct.	—77 46.2	S. by W.	—82	—35	—79 43	
			Def. N.	—77 23.0	S. by W.	—82	—81	—80 06	
			Direct.	—77 45.1	S. $\frac{1}{4}$ W.	—83	—35	—79 43	
			Direct.	—77 44.6	S. $\frac{3}{4}$ W.	—82	—35	—79 42	
			Direct.	—77 57.6	S.S.W.	—76	—35	—79 49	
			Direct.	—77 34.4	S.	—84	—35	—79 33	
			Direct.	—79 51.1	N.E. $\frac{1}{2}$ E.	+63	—35	—79 23	
			Direct.	—79 57.6	N.E.	+69	—35	—79 24	
			Direct.	—79 32.1	N.E. by E. $\frac{1}{2}$ E.	+52	—35	—79 15	
24.	—65 50	204 08	Direct.	—78 18.6	S.E. by E. $\frac{1}{2}$ E.	—27	—35	—79 21	Sailing amongst loose ice, very steady.
			Direct.	—78 14.3	S.E. by E.	—36	—35	—79 25	
			Direct.	—78 23.0	E.S.E.	—17	—35	—79 15	
			Direct.	—80 26.0	N.	+86	—35	—79 35	
			Direct.	—80 03.9	N.E. by N.	+75	—35	—79 24	
			Direct.	—80 11.6	N.N.E.	+81	—35	—79 26	
			Direct.	—80 19.4	N. by E.	+85	—35	—79 29	
			Direct.	—80 31.9	N. by W.	+85	—35	—79 42	
			Direct.	—80 28.8	N. by W.	+85	—35	—79 39	
			Def. N.	—79 26.9	N. by W.	+85	—81	—79 23	Ship fast to a piece of ice.
			Mag. S.	—80 21.4	N. by W.	+85	—35	—79 31	
			Mag. N.	—80 08.5	N. by W.	+85	—35	—79 19	
			Mag. N.S.	—80 00.0	N. by W.	+85	—35	—79 10	
			Direct.	—80 01.8	N.E.	+69	—35	—79 28	
			Mag. S.	—79 50.6	N.E.	+69	—35	—79 17	
			Direct.	—80 29.6	N.N.W.	+81	—35	—79 44	
25.	—66 01	204 00	Direct.	—80 29.2	N.W.	+69	—35	—79 55	Sailing amongst ice, very steady.
			Direct.	—79 01.3	E.	+16	—35	—79 19	
			Direct.	—79 09.2	E. by N.	+32	—35	—79 12	
			Direct.	—78 56.5	E. $\frac{3}{4}$ S.	+4	—35	—79 28	
			Direct.	—80 31.4	N.W. $\frac{1}{4}$ N.	+70	—35	—79 56	
26.	—65 57	204 27	Direct.	—78 39.0	E. by S. $\frac{3}{4}$ S.	—12	—35	—79 26	Sailing amongst ice, very steady.
			Direct.	—80 39.4	N. by W.	+85	—35	—79 49	
			Direct.	—80 31.5	N.W. $\frac{3}{4}$ W.	+61	—35	—80 06	
			Direct.	—78 21.3	S.E.	—51	—35	—79 47	
27.	—66 08	203 50	Direct.	—78 39.0	E.S.E.	—18	—35	—79 32	Sailing amongst ice, very steady.
			Direct.	—78 44.5	E.S.E.	—18	—35	—79 37	
			Direct.	—79 00.2	E. by S.	—1	—35	—79 36	
			Def. N.	—77 37.7	E.S.E.	—18	—81	—79 17	
			Def. S.	—78 30.0	E.S.E.	—18	—35	—79 23	
			Direct.	—80 38.3	N.W. by N.	+75	—35	—79 58	

* The result is omitted in the mean, as it differs so widely from all others of the same period.

Observations of Inclination. (Continued.)

1841.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Dec. 27.	-66° 08'	203° 50'	Mag. N.	-80° 16.1	N.W. by N.	+75	-35	-79° 36'	Sailing amongst ice, very steady.
			Mag. N.S.	-79 58.1	N.W. by N.	+75	-35	-79 18	
			Mag. S.	-80 34.0	N.W. by N.	+75	-35	-79 54	
			Direct.	-78 03.0	s. by E.	-83	-35	-80 01	
			Direct.	-78 21.3	s.E.	-52	-35	-79 48	Sailing amongst ice, very steady.
			Direct.	-80 00.0	w. by N.	+32	-35	-80 03	
			Def. N.	-78 52.8	w. by N.	+32	-81	-79 42	
			Direct.	-80 50.2	N. $\frac{1}{2}$ W.	+85	-35	-80 00	
			Direct.	-78 29.2	s.W. by s.	-65	-35	-80 09	Sailing amongst ice, very steady.
			Direct.	-79 22.8	E.	+16	-35	-79 42	
			Direct.	-80 44.3	N.W. $\frac{1}{2}$ W.	+64	-35	-80 15	
			Direct.	-80 47.6	N.W.	+69	-35	-80 14	
30.	-66° 11'	202° 54'	Direct.	-79 26.8	E. $\frac{1}{2}$ N.	+24	-35	-79 38	Sailing amongst ice, very steady.
			Direct.	-79 24.7	E. by s.	0	-35	-80 00	
			Direct.	-81 13.2	N. W. by N.	+75	-35	-80 33	
			Direct.	-79 45.3	E.	+16	-35	-80 04	
			Direct.	-79 59.8	E. by N.	+32	-35	-80 03	Fast to a piece of ice: Erebus fast to the same piece distant fifty yards. Terror's head to North*.
			Direct.	-80 09.2	E.N.E.	+46	-35	-79 58	
			Direct.	-80 14.0	N.E. by E. $\frac{1}{2}$ E.	+52	-35	-79 57	
			Direct.	-81 15.6	N. by W.	+85	-35	-80 26	
			Direct.	-81 17.6	N. $\frac{1}{2}$ W.	+85	-35	-80 28	Erebus bearing E.
			Direct.	-81 15.5	N.	+86	-35	-80 25	
			Direct.	-81 10.2	N. $\frac{1}{2}$ E	+85	-35	-80 20	
			Direct.	-81 11.8	N. by E.	+85	-35	-80 22	
1842. Jan. 1.	-66° 36'	203° 29'	Direct.	-80 28.6	w. $\frac{1}{2}$ N.	+24	-35	-80 40	Ditto; Erebus N.
			Direct.	-81 14.8	N.W. $\frac{1}{2}$ W.	+64	-35	-80 46	Ditto; Erebus N.E.
			Def. N.	-80 22.2	N.W. $\frac{1}{2}$ W.	+64	-81	-80 39	
			Def. S.	-81 06.3	N.W. $\frac{1}{2}$ W.	+64	-35	-80 37	
			Mag. N.	-81 03.7	N.W. $\frac{1}{2}$ W.	+64	-35	-80 34	
			Mag. N.S.	-80 50.7	N.W. $\frac{1}{2}$ W.	+64	-35	-80 22	Ditto; Erebus E.
			Mag. S.	-81 01.3	N.W. $\frac{1}{2}$ W.	+64	-35	-80 32	
			Direct.	-81 15.4	N.W. $\frac{1}{2}$ W.	+64	-35	-80 46	
			Direct.	-81 12.4	N. $\frac{1}{2}$ W.	+85	-35	-80 22	
			Direct.	-78 46.1	s.E.	-52	-35	-80 13	Running amongst loose ice, very steady.
			Direct.	-78 26.1	s. by w.	-83	-35	-80 24	
			Direct.	-78 29.6	s. by w. $\frac{1}{2}$ W.	-80	-35	-80 25	
			Direct.	-79 36.7	E. $\frac{1}{2}$ S.	+8	-35	-80 04	
5.	-66° 14'	203° 17'	Direct.	-77 46.2	s. $\frac{3}{4}$ W.	-83	-35	-79 44	Running amongst loose ice, very steady.
			Direct.	-80 15.8	N. $\frac{3}{4}$ E.	+85	-35	-79 26	
			Direct.	-80 31.9	N.W.	+69	-35	-79 58	
			Def. N.	-79 32.1	N.W.	+69	-81	-79 44	
			Def. S.	-80 26.2	N.W.	+69	-35	-79 52	Running amongst loose ice, very steady.
			Mag. N.	-80 15.7	N.W.	+69	-35	-79 42	
			Mag. N.S.	-80 05.8	N.W.	+69	-35	-79 32	
			Mag. S.	-80 34.5	N.W.	+69	-35	-80 01	
			Direct.	-80 37.9	N.W.	+69	-35	-80 04	Running amongst loose ice, very steady.
			Direct.	-79 53.0	s.	-85	-35	-79 53	
			Direct.	-78 00.9	s. by E.	-83	-35	-79 59	
			Direct.	-78 15.2	s. by w. $\frac{1}{2}$ W.	-80	-35	-80 10	
8.	-66° 05'	204° 02'	Direct.	-80 44.1	N.	+86	-35	-79 53	Running amongst loose ice, very steady.
			Def. N.	-79 45.4	N.	+86	-81	-79 40	
			Def. S.	-80 41.6	N.	+86	-35	-79 51	
			Mag. N.	-80 27.8	N.	+86	-35	-79 37	

* These observations are omitted in the general table of results, and in the map: the proximity of the two ships appears however to have produced scarcely any sensible effect on the inclination needle.

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Jan. 8.	-66 05	204 02	Mag. N.S.	-80 20.7	N.	+86	-35	-79 30	Running amongst loose ice, very steady.
			Mag. S.	-80 46.2	N.	+86	-35	-79 55	
			Direct.	-80 45.4	N.	+86	-35	-79 54	
			Direct.	-78 00.6	s. by E.	-83	-35	-79 59	
			Direct.	-78 25.8	s.w. by s.	-65	-35	-80 06	
			Direct.	-80 40.4	N. by w.	+85	-35	-79 50	
			Direct.	-80 43.1	N.	+86	-35	-79 52	
			Direct.	-79 10.0	E. $\frac{1}{2}$ S.	+8	-35	-79 37	
			Direct.	-77 56.0	S.	-85	-35	-79 56	
			Direct.	-78 58.2	E. by S.	-1	-35	-79 34	
9.	-66 01	204 04	Direct.	-79 22.2	E. $\frac{1}{4}$ N.	+20	-35	-79 37	Running amongst loose ice, very steady.
			Direct.	-78 46.0	s.w. by w.	-36	-35	-79 57	
			Direct.	-78 33.8	s.w. $\frac{1}{2}$ w.	-44	-35	-79 53	
			Def. N.	-77 34.8	s.w. $\frac{1}{2}$ w.	-44	-81	-79 40	
			Direct.	-78 36.3	s.w.	-52	-35	-80 03	
			Direct.	-79 00.8	w.s.w.	-18	-35	-79 54	
			Def. S.	-79 10.9	w.s.w.	-18	-35	-80 04	
			Mag. N.	-78 28.8	s.w. by w.	-36	-35	-79 40	
			Mag. N.S.	-78 24.4	s.w. by w.	-36	-35	-79 35	
			Mag. S.	-78 48.6	s.w. by w.	-36	-35	-80 00	
10.	-65 57	203 56	Direct.	-78 45.2	s.w. by w.	-36	-35	-79 56	Running amongst loose ice, very steady.
			Direct.	-79 03.7	w.s.w.	-18	-35	-79 57	
			Direct.	-79 30.4	w. by s.	-1	-35	-80 06	
			Def. N.	-78 23.7	w. by s.	-1	-81	-79 46	
			Def. S.	-79 14.9	w. by s.	-1	-35	-79 51	
			Mag. N.	-79 17.4	w. by s.	-1	-35	-79 53	
			Direct.	-79 15.1	E.	+16	-35	-79 34	
			Mag. S.	-79 17.6	E.	+16	-35	-79 37	
			Mag. N.S.	-78 55.2	E.	+16	-35	-79 14	
			Direct.	-79 15.7	E.	+16	-35	-79 35	
11.	-65 58	203 37	Direct.	-78 29.0	s.e. by E. $\frac{1}{2}$ E.	-27	-35	-79 31	Running amongst loose ice, very steady.
			Direct.	-79 41.5	w. $\frac{1}{4}$ S.	+12	-35	-80 05	
			Direct.	-79 23.8	w. by s. $\frac{1}{2}$ S.	-8	-35	-80 07	
			Direct.	-78 44.5	s.w. by w.	-36	-35	-79 55	
			Direct.	-78 46.3	s.w. by w.	-36	-35	-79 57	
			Direct.	-77 58.3	s. by E.	-83	-35	-79 56	
			Direct.	-77 53.2	S.	-85	-35	-79 53	
			Def. N.	-76 51.8	S.	-85	-81	-79 58	
			Def. S.	-77 56.7	S.	-85	-35	-79 57	
			Mag. N.	-77 31.0	S.	-85	-35	-79 31	
12.	-65 45	203 23	Mag. N.S.	-77 35.4	S.	-85	-35	-79 35	Very steady, working about in a hole of water.
			Mag. S.	-77 49.3	S.	-85	-35	-79 49	
			Direct.	-78 30.4	s.w.	-52	-35	-79 57	
			Direct.	-78 20.6	s.w. by s.	-65	-35	-80 01	
			Direct.	-78 44.4	s.w. by w.	-36	-35	-79 55	
			Direct.	-78 13.7	s. by w.	-82	-35	-80 11	
			Direct.	-77 50.3	S.	-84	-35	-79 49	
			Direct.	-80 22.0	N.N.E.	+81	-35	-79 36	
			Direct.	-80 46.2	N.	+86	-35	-79 55	
			Direct.	-80 38.4	N. $\frac{1}{2}$ E.	+85	-35	-79 48	
13.	-66 06	202 10	Def. N.	-79 44.5	N. $\frac{1}{2}$ E.	+85	-81	-79 41	Very steady, working about in a hole of water.
			Def. S.	-80 39.1	N. $\frac{1}{2}$ E.	+85	-35	-79 49	
			Mag. N.	-80 22.8	N. $\frac{1}{2}$ E.	+85	-35	-79 33	
			Mag. N.S.	-80 20.0	N. $\frac{1}{2}$ E.	+85	-35	-79 30	
			Mag. S.	-80 37.4	N. $\frac{1}{2}$ E.	+85	-35	-79 47	
			Direct.	-80 39.8	N. $\frac{1}{2}$ E.	+85	-35	-79 50	
			Direct.	-78 07.0	S.S.E.	-77	-35	-79 59	
			Direct.	-77 58.2	S.	-85	-35	-79 58	
			Direct.	-77 58.2	S.	-85	-35	-79 58	
			Direct.	-77 58.2	S.	-85	-35	-79 58	

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Jan. 14.	-66 08	201 46	Direct.	-77 58.8	s.	-85	-35	-79 59	-79 35
			Direct.	-78 09.0	s. by E.	-83	-35	-80 07	
			Direct.	-80 23.5	N.N.E.	+81	-35	-79 38	
			Direct.	-80 20.4	N.E.	+69	-35	-79 46	
			Direct.	-79 51.7	N.E. by E.	+59	-35	-79 28	
			Def. N.	-79 01.7	N.E. by E.	+59	-81	-79 24	
			Def. S.	-80 00.4	N.E. by E.	+59	-35	-79 36	
			Mag. N.	-79 39.7	N.E. by E.	+59	-35	-79 16	
			Mag. N.S.	-79 28.8	N.E. by E.	+59	-35	-79 05	
			Mag. S.	-80 17.5	N.N.E.	+81	-35	-79 32	
15.	-65 59	202 22	Direct.	-80 22.0	N.N.E.	+81	-35	-79 36	Very steady, working about in a hole of water.
			Direct.	-78 45.5	E.S.E.	-18	-35	-79 39	
			Direct.	-79 19.4	E.	+16	-35	-79 38	
16.	-65 47	202 08	Direct.	-78 31.4	S.W. by S.	-65	-35	-80 11	
			Direct.	-78 45.9	E.S.E.	-18	-35	-79 39	
			Direct.	-79 23.8	E.	+16	-35	-79 43	
			Def. N.	-78 32.3	E.	+16	-81	-79 37	
			Def. S.	-79 13.2	E.	+16	-35	-79 32	
			Mag. N.	-79 06.4	E.	+16	-35	-79 25	
			Mag. N.S.	-79 00.0	E.	+16	-35	-79 19	
			Mag. S.	-79 19.3	E.	+16	-35	-79 38	
			Direct.	-79 23.4	E.	+16	-35	-79 42	
			Direct.	-79 25.3	E.	+16	-35	-79 44	
17.	-65 47	201 56	Direct.	-80 05.9	N.E.	+69	-35	-79 32	Fast to a piece of ice.
19.	-66 11	200 45	Direct.	-80 55.9	N.	+86	-35	-80 05	
20.	-67 37	200 12	Direct.	-80 50.3	N. by E. $\frac{3}{4}$ E.	+82	-35	-80 03	Ship steady.
			Direct.	-78 47.2	S.S.W. $\frac{1}{2}$ W.	-71	-35	-80 33	
			Direct.	-79 51.6	W. by S.	-1	-35	-80 28	Long swell, ship striking heavily against pieces of ice.
			Direct.	-80 25.6	W. by N.	+32	-35	-80 29	
21.	-66 43	202 50	Direct.	-80 03.1	W.	+16	-35	-80 22	
			Direct.	-80 47.6	N. by E.	+85	-35	-79 58	
			Direct.	-80 59.8	N. by E. $\frac{1}{2}$ E.	+83	-35	-80 12	
			Direct.	-78 26.8	S. by W.	-83	-35	-80 25	
			Direct.	-78 44.7	S.S.W.	-77	-35	-80 37	
			Direct.	-78 38.3	S. by W.	-83	-35	-80 36	
			Direct.	-78 35.4	S.	-85	-35	-80 35	
			Direct.	-80 12.8	E. by N.	+32	-35	-80 16	Swell from W.N.W.
			Def. N.	-79 15.3	E. by N.	+32	-81	-80 04	
			Def. S.	-80 14.2	E. by N.	+32	-35	-80 17	Both ships made fast to a piece of ice; Erebus N. by W., distant 20 fathoms.
26.	-67 12	203 12	Mag. N.	-80 07.4	E. by N.	+32	-35	-80 10	
			Mag. N.S.	-79 55.1	E. by N.	+32	-35	-79 58	
			Direct.	-80 03.0	E.	+16	-35	-80 22	
			Direct.	-78 54.4	S.E. by E.	-36	-35	-80 05	
			Mag. N.S.	-78 23.2	S.E. by E.	-36	-35	-79 34	
			Mag. S.	-78 46.7	S.E. by E.	-36	-35	-79 58	
			Direct.	-79 28.2	E.S.E.	-18	-35	-80 21	
			Direct.	-80 38.8	E. by N.	+32	-35	-80 42	
			Def. N.	-79 40.5	E. by N.	+32	-81	-80 30	
			Def. S.	-81 31.3	N.	+86	-35	-80 40	
28.	-67 46	204 17	Direct.	-80 46.1	E.N.E.	+46	-35	-80 35	Swell from W.S.W. Table steady.
			Direct.	-81 45.8	N. by E.	+85	-35	-80 56	
			Def. N.	-81 02.7	N. by E.	+85	-81	-81 07	
			Direct.	-81 31.0	N.N.E.	+81	-35	-80 45	
			Def. N.	-80 43.8	N.N.E.	+81	-81	-80 44	
			Mag. N.	-81 24.4	N.N.E.	+81	-35	-80 38	
								-80 43	

* Omitted in the Map, in consequence of the vicinity of the other ship.

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Jan. 28.	-67 46	204 17	Mag. N.S.	-81 16.6	N.N.E.	+81	-35	-80 31	Table steady.
			Mag. S.	-81 25.2	N.N.E.	+81	-35	-80 39	
			Direct.	-79 06.5	S. $\frac{3}{4}$ W.	-84	-35	-81 06	
			Def. N.	-78 00.0	S. $\frac{3}{4}$ W.	-84	-81	-80 45	
			Def. S.	-78 38.0	S. $\frac{3}{4}$ W.	-84	-35	-80 37	
			Mag. N.	-78 36.0	S. $\frac{3}{4}$ W.	-84	-35	-80 35	
			Mag. N.S.	-78 32.1	S. $\frac{3}{4}$ W.	-84	-35	-80 31	
			Mag. S.	-78 45.8	S. $\frac{3}{4}$ W.	-84	-35	-80 45	
			Direct.	-79 04.5	S. $\frac{3}{4}$ W.	-84	-35	-81 04	
			Direct.	-81 39.3	N.	+86	-35	-80 48	
			Direct.	-81 42.2	N. by W. $\frac{3}{4}$ W.	+83	-35	-80 54	
			Direct.	-81 47.6	N. by W. $\frac{1}{2}$ W.	+84	-35	-81 00	
	-67 48	204 18	Direct.	-78 47.4	S. $\frac{1}{2}$ E.	-84	-35	-80 46	-80 48
			Direct.	-78 50.6	S. $\frac{1}{2}$ E.	-84	-35	-80 50	
			Direct.	-79 45.4	S.W. by W.	-36	-35	-80 56	
			Direct.	-80 40.8	W.	+16	-35	-81 00	
			Direct.	-81 31.5	N.W. by W.	+59	-35	-81 08	
			Direct.	-80 15.3	E.	+16	-35	-80 34	
			Direct.	-80 01.3	E. by S.	-1	-35	-80 37	
			Direct.	-79 46.6	E.S.E.	-18	-35	-80 40	
			Direct.	-80 31.9	E. by N.	+32	-35	-80 35	
			Direct.	-80 38.5	E.N.E.	+46	-35	-80 28	
			Direct.	-79 10.2	S. by W.	-83	-35	-81 08	
			Def. N.	-78 06.9	S. by W.	-83	-81	-80 51	
29.	-67 24	204 05	Def. S.	-78 44.1	E.N.E.	+46	-35	* }	Very steady.
			Mag. N.	-78 38.6	E.N.E.	+46	-35		
			Mag. N.S.	-78 33.9	E.N.E.	+46	-35		
			Direct.	-78 59.8	S.S.W.	-77	-35	-80 52	
			Def. N.	-78 07.9	S.S.W.	-77	-81	-80 46	
			Def. S.	-78 55.8	S.S.W.	-77	-35	-80 48	
			Mag. N.	-78 36.9	S.S.W.	-77	-35	-80 29	
			Mag. N.S.	-78 29.0	S.S.W.	-77	-35	-80 21	
			Mag. S.	-79 07.7	S.S.W.	-77	-35	-81 00	
			Direct.	-79 23.3	S.W.	-52	-35	-80 50	
			Def. N.	-78 09.4	S.W.	-52	-81	-80 22	
			Direct.	-79 15.3	S.W. by S.	-65	-35	-80 55	
Feb. 1.	-67 12	201 34	Def. N.	-78 23.5	S.W. by S.	-65	-81	-80 50	-80 44
			Direct.	-80 15.5	W. by S.	-1	-35	-80 52	
			Def. N.	-79 14.5	W. by S.	-1	-81	-80 37	
			Direct.	-80 06.5	E.	+17	-35	-80 25	
			Def. N.	-79 05.2	E.	+17	-81	-80 09	
			Direct.	-79 29.1	E.S.E.	-18	-35	-80 22	
			Direct.	-80 25.9	W.	+17	-35	-80 44	
			Direct.	-79 51.9	W.S.W.	-18	-35	-80 45	
			Direct.	-78 58.6	S.S.W.	-77	-35	-80 51	
			Def. N.	-77 59.0	S.S.W.	-77	-81	-80 31	
			Def. S.	-78 53.6	S.S.W.	-77	-35	-80 46	
			Mag. N.	-78 32.1	S.S.W.	-77	-35	-80 24	
	-67 16		Mag. N.S.	-78 30.2	S.S.W.	-77	-35	-80 22	-80 35
			Mag. S.	-78 49.0	S.S.W.	-77	-35	-80 41	
			Direct.	-79 00.8	S.S.W.	-77	-35	-80 53	
			Direct.	-81 30.0	N. $\frac{3}{4}$ W.	+86	-35	-80 39	
			Def. N.	-80 37.0	N. $\frac{3}{4}$ W.	+86	-81	-80 32	
			Direct.	-79 08.1	S.W.	-52	-35	-80 35	
			Def. N.	-78 11.1	S.W.	-52	-81	-80 24	

* Omitted in the mean; apparently the degree should have been written 80 instead of 78.

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Feb. 2.	-67° 56'	199 48	Direct.	-79° 28.6	s. by w.	-83	-35	-81° 27'	
			Def. N.	-78 37.8	s. by w.	-83	-81	-81 22	
			Def. S.	-79 15.1	s. by w.	-83	-35	-81 13	
			Mag. N.	-78 53.6	s. by w.	-83	-35	-80 52	
			Mag. N.S.	-79 07.5	s. by w.	-83	-35	-81 06	
			Mag. S.	-79 26.9	s. by w.	-83	-35	-81 25	
3.	-68 21	200 06	Direct.	-79 27.4	s. by w.	-83	-35	-81 25	Table steady.
			Direct.	-79 34.2	s.s.w.	-77	-35	-81 26	
			Def. N.	-78 31.9	s.s.w.	-77	-81	-81 10	
			Def. S.	-79 26.7	s.s.w.	-77	-35	-81 19	
			Mag. N.	-79 24.2	s.s.w.	-77	-35	-81 16	
			Mag. N.S.	-79 23.4	s.s.w.	-77	-35	-81 15	
			Mag. S.	-79 28.6	s.s.w.	-77	-35	-81 21	
			Direct.	-79 36.1	s.s.w.	-77	-35	-81 28	
4.	-68 45	199 41	Direct.	-79 32.5	s.	-85	-35	-81 33	
			Def. N.	-78 50.3	s.	-85	-81	-81 36	
			Def. S.	-79 36.6	s.	-85	-35	-81 37	
			Mag. N.	-79 17.2	s.	-85	-35	-81 17	
			Mag. N.S.	-79 12.4	s.	-85	-35	-81 12	
			Mag. S.	-79 43.4	s.	-85	-35	-81 43	
			Direct.	-79 32.1	s. by E.	-83	-35	-81 30	-81 33
			Def. N.	-78 50.4	s. by E.	-83	-81	-81 34	
			Def. S.	-79 25.8	s. by E.	-83	-35	-81 24	
			Direct.	-82 31.4	N.N.W.	+82	-35	-81 44	
	-68 49	199 26	Def. N.	-81 48.7	N.N.W.	+82	-81	-81 48	Fresh breeze, steady.
			Direct.	-81 51.5	s.w.	-52	-35	-83 19	
5.	-68 52	198 24	Def. N.	-79 59.5	s.w.	-52	-81	-82 13	
			Def. S.	-80 58.7	s.w.	-52	-35	-82 26	
			Mag. N.	-80 48.0	s.w.	-52	-35	-82 15	
			Mag. N.S.	-80 36.8	s.w.	-52	-35	-82 04	
			Mag. S.	-81 04.1	s.w.	-52	-35	-82 31	-82 30
			Direct.	-81 21.6	s.w. $\frac{1}{2}$ w.	-44	-35	-82 41	
			Direct.	-81 20.0	s.w. by w.	-36	-35	-82 31	
			Direct.	-81 09.2	s. by w.	-84	-35	-83 08	
6.	-69 55	192 17	Def. N.	-80 15.1	s. by w.	-84	-81	-83 00	
			Def. S.	-81 04.2	s. by w.	-84	-35	-83 03	
			Mag. N.	-80 52.3	s. by w.	-84	-35	-82 51	
			Mag. N.S.	-80 39.1	s. by w.	-84	-35	-82 38	
			Mag. S.	-81 09.2	s. by w.	-84	-35	-83 08	-83 00
			Direct.	-81 12.8	s. by w.	-84	-35	-83 12	
			Direct.	-80 56.9	s.	-86	-35	-82 58	
			Def. N.	-80 00.2	s.	-86	-81	-82 47	
			Direct.	-81 12.6	s. by w.	-84	-35	-83 12	
			Direct.	-81 35.1	s.s.w.	-78	-35	-83 28	
7.	-70 05	191 03	Def. N.	-80 38.2	s.s.w.	-78	-81	-83 17	
			Direct.	-81 56.4	s.w.	-52	-35	-83 23	
			Direct.	-81 35.3	s. by w. $\frac{3}{4}$ w.	-80	-35	-83 30	
			Def. S.	-81 20.0	s.s.w.	-78	-35	-83 13	
			Mag. N.	-81 24.7	s.s.w.	-78	-35	-83 18	-83 20
			Mag. N.S.	-81 15.6	s.s.w.	-78	-35	-83 09	
			Mag. S.	-81 23.9	s.s.w.	-78	-35	-83 17	
			Direct.	-81 29.6	s. by w. $\frac{1}{2}$ w.	-81	-35	-83 26	
8.	-70 08	186 39	Direct.	-81 56.9	s.w.	-52	-35	-83 24	
			Def. N.	-81 16.7	s.w.	-52	-81	-83 30	
			Direct.	-82 12.3	s.w. by w.	-36	-35	-83 23	
			Def. N.	-81 34.1	s.w. by w.	-36	-83	-83 31	

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Feb. 8.	-70 08	186 39	Def. S.	-82 09.9	s.w. by w.	-36	-35	-83 21	Table steady.
			Mag. N.	-82 10.1	s.w. by w.	-36	-35	-83 21	
			Mag. N.S.	-82 03.7	s.w. by w.	-36	-35	-83 15	
			Mag. S.	-82 10.3	s.w. by w.	-36	-35	-83 21	
	-70 17	186 04	Direct.	-82 15.9	s.w. by w.	-36	-35	-83 27	
			Direct.	-81 19.7	s.	-87	-35	-83 22	
			Direct.	-81 16.1	s.	-87	-35	-83 18	
			Def. N.	-80 37.6	s.	-87	-81	-83 26	
			Def. S.	-81 38.5	s.	-87	-35	-83 41	
			Mag. N.	-81 11.6	s.	-87	-35	-83 14	
			Mag. N.S.	-81 04.5	s.	-87	-35	-83 07	
			Mag. S.	-81 33.4	s.	-87	-35	-83 35	
			Direct.	-81 20.6	s.	-87	-35	-83 23	
			Direct.	-83 51.8	w. by N.	+32	-35	-83 55	
			Def. N.	-83 09.4	w. by N.	+32	-81	-83 58	
			Def. S.	-83 55.8	w. by N.	+32	-35	-83 59	
9.	-70 32	185 38	Mag. N.S.	-83 36.2	w. by N.	+32	-35	-83 39	
			Direct.	-82 08.5	w. by N.	+32	-35	-82 12	
			Def. N.	-81 14.8	w. by N.	+32	-81	-82 04	
			Direct.	-82 02.7	S.E. $\frac{1}{2}$ s.	-59	-35	-83 37	
			Def. S.	-82 01.0	S.E. $\frac{1}{2}$ s.	-59	-35	-83 35	
			Mag. N.S.	-82 03.5	S.E. $\frac{1}{2}$ s.	-59	-35	-83 38	
			Direct.	-82 12.6	S.E. by s.	-66	-35	-83 54	
			Direct.	-83 33.0	w. by s.	-1	-35	-84 09	
			Def. N.	-82 37.3	w. by s.	-1	-81	-83 59	
			Def. S.	-83 31.5	w. by s.	-1	-35	-84 07	
			Mag. N.	-83 25.9	w. by s.	-1	-35	-84 02	
			Mag. N.S.	-83 11.0	w. by s.	-1	-35	-83 47	
10.	-69 56	184 43	Mag. S.	-83 33.1	w. by s.	-1	-35	-84 09	Heavy swell, unsteady.
			Direct.	-83 34.2	w. by s.	-1	-35	-84 10	
			Direct.	-83 46.2	w.	+17	-35	-84 04	
			Direct.	-83 21.8	W.S.W.	-18	-35	-84 15	
			Def. N.	-82 21.1	W.S.W.	-18	-81	-84 00	
			Def. S.	-83 04.0	W.S.W.	-18	-35	-83 57	
			Mag. N.	-83 25.7	W.S.W.	-18	-35	-84 19	
			Mag. N.S.	-82 58.0	W.S.W.	-18	-35	-83 51	
			Mag. S.	-83 20.5	W.S.W.	-18	-35	-84 14	
			Direct.	-82 45.0	s.w. by s.	-66	-35	-84 26	
			Direct.	-82 46.6	S.E. by s.	-66	-35	-84 28	
			Def. N.	-81 48.5	S.E. by s.	-66	-81	-84 16	
11.	-69 51	183 02	Def. S.	-82 39.3	S.E. by s.	-66	-35	-84 20	Strong wind, westerly swell, ship unsteady.
			Mag. N.	-82 24.9	S.E. by s.	-66	-35	-84 06	
			Mag. N.S.	-82 21.1	S.E. by s.	-66	-35	-84 02	
			Mag. S.	-82 34.9	S.E. by s.	-66	-35	-84 16	
			Direct.	-82 45.2	S.E. by s.	-66	-35	-84 26	
			Direct.	-83 08.2	S.E. by s.	-66	-35	-84 49	
			Direct.	-83 16.8	S.E. by s.	-66	-35	-84 58	
			Def. N.	-82 21.1	S.E. by s.	-66	-81	-84 48	
			Def. S.	-83 18.6	S.E. by s.	-66	-35	-85 00	
			Mag. N.	-83 06.9	S.E. by s.	-66	-35	-84 48	
			Mag. N.S.	-82 55.3	S.E. by s.	-66	-35	-84 36	
			Mag. S.	-83 17.7	S.E. by s.	-66	-35	-84 59	
12.	-70 03	181 44	Direct.	-83 20.2	S.E. by s.	-66	-35	-85 01	Cross sea, table very unsteady.
			Direct.	-83 37.9	S.E. by s.	-66	-35	-85 19	
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	
13.	-71 02	180 58	Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	Table very unsteady, a cross sea.
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	
	-72 07	181 50	Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	A swell from N.W., ship unsteady, steering badly.
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	
			Direct.	-83 40.5	S.E. by s.	-66	-35	-85 22	

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Feb. 14.	-72 55	181 33	Direct.	-83 58.2	S.E. by E.	-36	-35	-85 09	A swell from the W.N.W., unsteady.
			Def. N.	-83 21.7	S.E. by E.	-36	-81	-85 19	
			Def. S.	-84 07.0	S.E. by E.	-36	-35	-85 18	
			Mag. N.	-84 01.7	S.E. by E.	-36	-35	-85 13	
			Mag. N.S.	-83 29.5	S.E. by E.	-36	-35	-84 40	
	-73 23	181 11	Mag. S.	-83 58.4	S.E. by E.	-36	-35	-85 09	Strong breeze, unsteady. Heavy sea, very unsteady.
			Direct.	-84 00.6	S.E. by E.	-36	-35	-85 12	
			Direct.	-84 16.8	S.E.	-52	-35	-85 44	
			Direct.	-84 51.4	S.E. by S.	-66	-35	-86 32	
			Direct.	-85 13.4	S.S.E.	-79	-35	-87 07	
15.	-74 20	177 55	Def. N.	-84 17.5	S.S.E.	-79	-81	-86 58	Table steady.
16.	-74 51	174 02	Def. S.	-85 10.6	S.S.E.	-79	-35	-87 05	
			Mag. N.	-85 08.8	S.S.E.	-79	-35	-87 03	
			Mag. N.S.	-84 53.3	S.S.E.	-79	-35	-86 47	
			Mag. S.	-85 12.0	S.S.E.	-79	-35	-87 06	
			Direct.	-85 15.6	S.S.E.	-79	-35	-87 10	
			Direct.	-85 49.1	S.E.	-52	-35	-87 16	
			Direct.	-86 56.1	E. 1/2 S.	+ 7	-35	-87 24	
			Direct.	-86 33.0	E. by S.	- 2	-35	-87 10	
			Def. N.	-85 35.9	E. by S.	- 2	-81	-86 59	
			Def. S.	-86 39.6	E. by S.	- 2	-35	-87 17	
17.	-75 05	173 10	Mag. N.S.	-86 13.2	E. by S.	- 2	-35	-86 50	N.W. swell, slight motion.
			Direct.	-87 15.8	E.N.E.	+46	-35	-87 05	
			Direct.	-87 12.6	E. by N. 1/2 N.	+39	-35	-87 09	
			Def. N.	-86 31.1	E. by N. 1/2 N.	+39	-81	-87 13	
			Def. S.	-87 05.2	E. by N. 1/2 N.	+39	-35	-87 01	
			Mag. N.	-86 50.8	E. by N. 1/2 N.	+39	-35	-86 47	
			Mag. N.S.	-86 39.4	E. by N. 1/2 N.	+39	-35	-86 35	
			Mag. S.	-87 33.9	E. by N. 1/2 N.	+39	-35	-87 30	
			Direct.	-87 08.0	E. by N. 1/2 N.	+39	-35	-87 04	
			Direct.	-87 06.3	E.N.E.	+46	-35	-86 55	
18.	-77 02	181 37	Def. N.	-86 16.8	E.N.E.	+46	-81	-86 52	Very unsteady, steering badly.
			Def. S.	-87 21.3	E.N.E.	+46	-35	-87 10	
			Mag. N.	-87 14.9	E.N.E.	+46	-35	-87 04	
			Mag. N.S.	-86 45.6	E.N.E.	+46	-35	-86 35	
			Mag. S.	-87 15.2	E.N.E.	+46	-35	-87 04	
			Direct.	-87 37.4	N.E. 1/2 E.	+64	-35	-87 08	
			Direct.	-86 56.5	N.E. by E. 1/2 E.	+52	-35	-86 39	
			Direct.	-87 27.6	N. by E.	+88	-35	-86 35	
			Def. N.	-86 54.2	N. by E.	+88	-81	-86 47	
			Def. S.	-87 45.2	N. by E.	+88	-35	-86 52	
19.	-77 09	181 22	Mag. N.	-87 16.6	N. by E.	+88	-35	-86 24	Cross sea, table unsteady.
			Mag. N.S.	-87 15.1	N. by E.	+88	-35	-86 22	
			Mag. S.	-86 53.6	N. by E.	+88	-35	-86 01	
			Direct.	-87 29.1	N. by E.	+88	-35	-86 36	
			Direct.	-87 01.3	N.E. 1/2 N.	+72	-35	-86 24	
			Direct.	-86 44.6	N.E.	+69	-35	-86 11	
			Def. N.	-86 04.7	N.E.	+69	-81	-86 17	
			Def. S.	-86 42.3	N.E.	+69	-35	-86 08	
			Mag. N.	-86 26.7	N.E.	+69	-35	-85 53	
			Mag. N.S.	-86 23.0	N.E.	+69	-35	-85 49	
20.	-76 20	190 26	Mag. S.	-86 48.5	N.E.	+69	-35	-86 15	Strong gale, heavy sea, a great deal of motion.
			Direct.	-86 39.1	N.E.	+69	-35	-86 05	
			Direct.	-85 56.9	N.E. by E.	+59	-35	-85 33	
			Direct.	-84 13.7	S.W.	-52	-35	-85 41	
			Direct.	-85 56.9	N.E. by E.	+59	-35	-85 33	
			Direct.	-84 13.7	S.W.	-52	-35	-85 41	
			Direct.	-85 56.9	N.E. by E.	+59	-35	-85 33	
			Direct.	-84 13.7	S.W.	-52	-35	-85 41	
			Direct.	-85 56.9	N.E. by E.	+59	-35	-85 33	
			Direct.	-84 13.7	S.W.	-52	-35	-85 41	
21.	-76 14	192 29	Direct.	-85 56.9	N.E. by E.	+59	-35	-85 33	Strong gale, heavy sea, a great deal of motion.
			Direct.	-84 13.7	S.W.	-52	-35	-85 41	

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Feb. 22.	-76° 24'	184° 54'	Direct.	-83° 41'5"	S.E. by S.	-66	-35	-85° 23'	A head sea, ship unsteady.
			Def. N.	-82° 56'0"	S.E. by S.	-66	-81	-85° 23'	
			Def. S.	-83° 37'0"	S.E. by S.	-66	-35	-85° 18'	
			Mag. N.	-83° 19'8"	S.E. by S.	-66	-35	-85° 01'	
			Mag. N.S.	-82° 59'8"	S.E. by S.	-66	-35	-84° 41'	
			Mag. S.	-83° 29'9"	S.E. by S.	-66	-35	-85° 11'	
	-76° 46'	193° 48'	Direct.	-83° 45'2"	S.E. by S.	-66	-35	-85° 26'	Light swell, gentle motion.
			Direct.	-84° 19'4"	E.S.E.	-18	-35	-85° 12'	
			Direct.	-84° 37'4"	E. by S.	-1	-35	-85° 13'	
			Def. N.	-83° 51'4"	E. by S.	-1	-81	-85° 13'	
			Def. S.	-84° 50'8"	E. by S.	-1	-35	-85° 27'	
			Mag. N.	-84° 31'6"	E. by S.	-1	-35	-85° 08'	
	-77° 13'	193° 52'	Mag. N.S.	-84° 17'0"	E. by S.	-1	-35	-84° 53'	Table very steady.
			Mag. S.	-84° 27'8"	E. by S.	-1	-35	-85° 04'	
			Direct.	-85° 02'7"	E.	+17	-35	-85° 21'	
			Direct.	-84° 14'6"	S.W. by W. ½ W.	-27	-35	-85° 17'	
			Direct.	-85° 13'0"	N.E. by E.	+59	-35	-84° 49'	
			Def. N.	-84° 34'3"	N.E. by E.	+59	-81	-84° 56'	
23.	-77° 48'	197° 23'	Def. S.	-85° 21'1"	N.E. by E.	+59	-35	-84° 57'	Swell from N.E., steady.
			Direct.	-85° 05'7"	E.N.E.	+46	-35	-84° 55'	
			Mag. N.	-84° 21'4"	E.N.E.	+46	-35	-84° 10'	
			Mag. N.S.	-84° 41'7"	E.N.E.	+46	-35	-84° 31'	
			Mag. S.	-85° 00'2"	E.N.E.	+46	-35	-84° 49'	
			Direct.	-85° 05'5"	E.N.E.	+46	-35	-84° 55'	
	-77° 14'	199° 29'	Direct.	-84° 00'0"	S.W. by S.	-66	-35	-85° 41'	Swell from the E.N.E., steady.
			Def. N.	-83° 17'5"	S.W. by S.	-66	-81	-85° 45'	
			Def. S.	-83° 57'7"	S.W. by S.	-66	-35	-85° 39'	
			Mag. N.	-83° 42'9"	S.W. by S.	-66	-35	-85° 24'	
			Mag. N.S.	-83° 32'3"	S.W. by S.	-66	-35	-85° 13'	
			Mag. S.	-84° 11'7"	S.W. by S.	-66	-35	-85° 53'	
25.	-77° 00'	198° 50'	Direct.	-85° 13'3"	w.	+17	-35	-85° 31'	Strong breeze, motion great.
			Direct.	-84° 25'8"	S.W. by W.	-36	-35	-85° 37'	
			Direct.	-85° 30'9"	w.	+17	-35	-85° 49'	
			Def. N.	-84° 33'1"	w.	+17	-81	-85° 37'	
			Def. S.	-85° 28'4"	w.	+17	-35	-85° 46'	
			Mag. N.	-85° 15'5"	w.	+17	-35	-85° 34'	
	-75° 20'	194° 36'	Mag. N.S.	-84° 59'3"	w.	+17	-35	-85° 17'	Swell from the eastward, motion slight.
			Mag. S.	-85° 22'7"	w.	+17	-35	-85° 41'	
			Direct.	-85° 38'6"	w.	+17	-35	-85° 57'	
			Direct.	-84° 34'6"	S.W. by S.	-66	-35	-86° 16'	
			Direct.	-86° 03'9"	W.N.W.	+46	-35	-85° 53'	
			Direct.	-85° 37'4"	N.W. by W.	+60	-35	-85° 12'	
26.	-73° 10'	189° 21'	Def. N.	-84° 44'0"	N.W. by W.	+60	-81	-85° 05'	Table steady.
			Def. S.	-85° 36'9"	N.W. by W.	+60	-35	-85° 12'	
			Mag. N.	-85° 19'6"	N.W. by W.	+60	-35	-84° 55'	
			Mag. N.S.	-85° 37'8"	N.W. by W.	+60	-35	-85° 13'	
			Mag. S.	-85° 30'6"	N.W. by W.	+60	-35	-85° 06'	
			Direct.	-85° 35'6"	N.W. by W.	+60	-35	-85° 11'	
	-72° 03'	187° 40'	Direct.	-83° 30'8"	S.W.	-52	-35	-84° 58'	Swell from the eastward, motion slight.
			Def. N.	-82° 37'6"	S.W.	-52	-81	-84° 51'	
			Def. S.	-83° 36'5"	S.W.	-52	-35	-85° 04'	
			Mag. N.	-83° 07'6"	S.W.	-52	-35	-84° 35'	
			Direct.	-84° 56'8"	W. by N. ½ N.	+39	-35	-84° 53'	
			Mag. N.S.	-84° 25'5"	W. by N. ½ N.	+39	-35	-84° 22'	
27.	-71° 43'	187° 15'	Mag. S.	-83° 43'4"	S.W.	-52	-35	-85° 10'	Table steady.
			Direct.	-83° 52'3"	W.S.W.	-18	-35	-84° 45'	
			Direct.	-84° 56'8"	W.S.W.	-18	-35	-85° 50'	

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Feb. 28.	-71° 20'	184° 30'	Direct.	-84° 01.9	w. by s.	-1	-35	-84° 38'	-84° 37' Table steady.
			Def. N.	-82° 59.6	w. by s.	-1	-81	-84° 22'	
			Def. S.	-83° 56.9	w. by s.	-1	-35	-84° 33'	
			Mag. N.	-83° 37.9	w. by s.	-1	-35	-84° 14'	
			Mag. N.S.	-83° 23.9	w. by s.	-1	-35	-84° 00'	
	-70° 55'	183° 56'	Mag. S.	-84° 00.7	w. by s.	-1	-35	-84° 37'	
			Direct.	-83° 35.3	s.w. by w.	-36	-35	-84° 46'	
			Direct.	-84° 32.0	w. ½ s.	+8	-35	-84° 59'	
			Direct.	-84° 36.8	w.	+17	-35	-84° 55'	
			Direct.	-85° 31.6	N.W. ½ w.	+64	-35	-85° 03'	
Mar. 1.	-70° 49'	183° 46'	Direct.	-85° 00.0	W.N.W.	+54	-35	-84° 41'	-84° 30' Swell from the eastward, table steady.
			Def. N.	-84° 06.3	W.N.W.	+54	-81	-84° 33'	
			Def. S.	-84° 54.4	W.N.W.	+54	-35	-84° 35'	
			Mag. N.	-84° 44.4	W.N.W.	+54	-35	-84° 25'	
			Mag. N.S.	-84° 35.4	W.N.W.	+54	-35	-84° 16'	
	-69° 54'	179° 55'	Mag. S.	-84° 44.7	W.N.W.	+54	-35	-84° 26'	
			Direct.	-84° 54.2	W.N.W.	+54	-35	-84° 35'	
			Direct.	-84° 28.0	w. by N.	+37	-35	-84° 26'	
			Direct.	-83° 45.8	N.N.E.	+99	-35	-82° 42'	
			Def. N.	-82° 29.8	N.N.E.	+99	-81	-82° 12'	
2.	-68° 09'	183° 10'	Def. S.	-83° 33.2	N.N.E.	+99	-35	-82° 29'	-82° 26' Table steady.
			Mag. N.	-83° 31.2	N.N.E.	+99	-35	-82° 27'	
			Mag. N.S.	-83° 17.5	N.N.E.	+99	-35	-82° 14'	
			Mag. S.	-83° 26.9	N.N.E.	+99	-35	-82° 23'	
			Direct.	-83° 40.9	N.N.E.	+99	-35	-82° 37'	
	-67° 35'	185° 18'	Direct.	-82° 27.4	N.E. by E.	+71	-35	-81° 51'	-81° 33' Cross sea, unsteady.
			Direct.	-82° 53.4	N.E.	+83	-35	-82° 05'	
			Direct.	-82° 21.8	N.E. by E.	+71	-35	-81° 46'	
			Def. N.	-81° 31.3	N.E. by E.	+71	-81	-81° 41'	
			Def. S.	-82° 16.9	N.E. by E.	+71	-35	-81° 41'	
3.	-67° 27'	185° 32'	Mag. N.	-82° 04.0	N.E. by E.	+71	-35	-81° 28'	-81° 33' Cross sea, unsteady.
			Mag. N.S.	-81° 58.7	N.E. by E.	+71	-35	-81° 23'	
			Mag. S.	-82° 02.7	N.E. by E.	+71	-35	-81° 27'	
			Direct.	-82° 28.2	N.E. ½ E.	+76	-35	-81° 52'	
			Direct.	-82° 12.6	w.	+18	-35	-82° 30'	
	-67° 40'	187° 40'	Direct.	-82° 18.4	N. by w.	+103	-35	-81° 10'	-81° 03' Heavy sea, very unsteady.
			Def. N.	-81° 14.9	N. by w.	+103	-81	-80° 53'	
			Def. S.	-82° 28.2	N. by w.	+103	-35	-81° 20'	
			Mag. N.	-82° 07.0	N. by w.	+103	-81	-80° 59'	
			Mag. S.	-82° 22.0	N. by w.	+103	-35	-81° 14'	
4.	-67° 09'	188° 02'	Direct.	-82° 13.3	N.	+104	-35	-81° 04'	-81° 03' Heavy sea, very unsteady.
			Def. N.	-81° 40.1	N.	+104	-81	-81° 17'	
			Def. S.	-81° 45.6	N.	+104	-35	-80° 37'	
			Mag. N.	-82° 19.7	N.	+104	-35	-81° 11'	
			Mag. N.S.	-82° 01.2	N.	+104	-35	-80° 52'	
	-65° 28'	191° 24'	Mag. S.	-82° 16.6	N.	+104	-35	-81° 08'	-79° 42' South-westerly swell, unsteady.
			Direct.	-82° 20.0	N.	+104	-35	-81° 11'	
			Direct.	-81° 09.3	N. by E.	+102	-35	-80° 02'	
			Def. N.	-80° 06.6	N. by E.	+102	-81	-79° 46'	
			Def. S.	-80° 50.1	N. by E.	+102	-35	-79° 43'	
5.	-65° 04'	192° 00'	Mag. N.	-80° 47.0	N. by E.	+102	-35	-79° 40'	-79° 42' South-westerly swell, unsteady.
			Mag. N.S.	-80° 34.9	N. by E.	+102	-35	-79° 28'	
			Mag. S.	-81° 00.6	N. by E.	+102	-35	-79° 54'	
			Direct.	-81° 03.5	N. by E.	+102	-35	-79° 57'	
			Direct.	-80° 44.2	N. by E.	+102	-35	-79° 37'	
	-64° 49'	192° 21'	Direct.	-80° 28.9	N. by E. ½ E.	+99	-35	-79° 25'	
			Direct.	-80° 30.4	N. by E. ½ E.	+99	-35	-79° 26'	

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Mar. 7.	—63 30	194 15	Direct.	—79 46.4	N. by E.	+100	—35	—78 41	—78 30 Steady.
			Def. N.	—78 34.4	N. by E.	+100	—81	—78 15	
			Def. S.	—79 29.2	N. by E.	+100	—35	—78 24	
			Mag. N.	—79 26.0	N. by E.	+100	—35	—78 21	
			Mag. N.S.	—79 24.0	N. by E.	+100	—35	—78 19	
			Mag. S.	—79 50.3	N. by E.	+100	—35	—78 45	
	8. —62 17	195 55	Direct.	—79 49.3	N. by E.	+100	—35	—78 44	—77 30 Steady.
			Direct.	—78 44.7	N. by E.	+100	—35	—77 40	
			Def. N.	—77 54.4	N. by E.	+100	—81	—77 35	
			Def. S.	—78 25.8	N. by E.	+100	—35	—77 21	
			Mag. N.	—78 27.8	N. by E.	+100	—35	—77 23	
			Mag. N.S.	—78 20.3	N. by E.	+100	—35	—77 15	
9.	—61 06	198 08	Mag. S.	—78 42.8	N. by E.	+100	—35	—77 38	—76 32 Steady.
			Direct.	—78 40.3	N. by E.	+100	—35	—77 35	
			Direct.	—77 41.6	N.E. $\frac{1}{2}$ N.	+85	—35	—76 52	
			Def. N.	—76 24.7	N.E. $\frac{1}{2}$ N.	+85	—81	—76 22	
			Def. S.	—77 25.9	N.E. $\frac{1}{2}$ N.	+85	—35	—76 36	
			Mag. N.	—77 16.4	N.E. by N.	+88	—35	—76 23	
	10. —60 57	199 03	Direct.	—77 38.4	N.E. by N.	+88	—35	—76 45	—75 08 Table unsteady.
			Mag. N.S.	—77 11.9	N.E. by N.	+88	—35	—76 19	
			Mag. S.	—77 16.9	N.E. by N.	+88	—35	—76 24	
			Direct.	—77 28.6	N.E. by N.	+88	—35	—76 36	
			Direct.	—77 16.7	N.E.	+81	—35	—76 31	
			Direct.	—75 32.7	E.N.E.	+53	—35	—75 15	
11.	—60 15	208 06	Def. N.	—74 41.0	E.N.E.	+53	—81	—75 19	—74 21 Strong gale, heavy sea, ship unsteady.
			Def. S.	—75 33.6	E.N.E.	+53	—35	—75 16	
			Mag. N.	—75 14.2	E.N.E.	+53	—35	—74 56	
			Mag. N.S.	—75 08.5	E.N.E.	+53	—35	—74 51	
			Mag. S.	—75 27.1	E.N.E.	+53	—35	—75 09	
			Direct.	—75 30.9	E.N.E.	+53	—35	—75 13	
	12. —60 16	211 45	Direct.	—74 20.6	E. by N.	+37	—35	—74 19	—74 14 Heavy swell, ship unsteady.
			Def. N.	—73 57.2	E. by N.	+37	—81	—74 41	
			Def. S.	—74 16.0	E. by N.	+37	—35	—74 14	
			Mag. N.	—74 32.4	E. by N.	+37	—35	—74 30	
			Mag. N.S.	—74 16.0	E. by N.	+37	—35	—74 14	
			Mag. S.	—74 20.9	E. by N.	+37	—35	—74 19	
13.	—60 18	212 39	Direct.	—74 28.5	E. by N.	+37	—35	—74 27	—73 36 Heavy swell, steering very wildly.
			Direct.	—74 07.4	E. by N.	+37	—35	—74 05	
			Def. N.	—73 31.1	E. by N.	+37	—81	—74 15	
			Def. S.	—74 20.5	E. by N.	+37	—35	—74 18	
			Mag. N.	—74 08.9	E. by N.	+37	—35	—74 07	
			Mag. N.S.	—74 28.0	E. by N.	+37	—35	—74 26	
	—59 53	216 28	Mag. S.	—74 33.4	E. by N.	+37	—35	—74 31	—73 48 Heavy swell from W.S.W., very unsteady, steering very badly.
			Direct.	—74 11.5	E. by N.	+37	—35	—74 09	
			Direct.	—73 59.8	E. by N.	+37	—35	—73 58	
			Direct.	—74 15.6	N.E. $\frac{1}{2}$ E.	+74	—35	—73 37	
			Def. N.	—73 29.3	N.E. $\frac{1}{2}$ E.	+74	—81	—73 36	
			Def. S.	—74 15.9	N.E. $\frac{1}{2}$ E.	+74	—35	—73 37	
14.	—59 22	218 14	Mag. N.	—74 09.7	N.E. $\frac{1}{2}$ E.	+74	—35	—73 31	—73 36 Heavy swell from W.S.W., very unsteady, steering very badly.
			Mag. N.S.	—74 15.3	N.E. $\frac{1}{2}$ E.	+74	—35	—73 36	
			Mag. S.	—74 16.5	N.E. $\frac{1}{2}$ E.	+74	—35	—73 37	
			Direct.	—74 18.2	N.E. $\frac{1}{2}$ E.	+74	—35	—73 39	
			Direct.	—75 02.4	N.E. by E.	+69	—35	—74 28	
			Def. N.	—74 26.8	N.E. by E.	+69	—81	—74 39	
			Def. S.	—75 01.0	N.E. by E.	+69	—35	—74 27	—73 48 Heavy swell from W.S.W., very unsteady, steering very badly.
			Mag. N.	—74 50.0	N.E. by E.	+69	—35	—74 16	

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Mar. 14.	-59 22	218 14	Mag. N.S.	-74 58.0	N.E. by E.	+69	-35	-74 24	Heavy swell from W.S.W., very unsteady, steering very badly.
			Mag. S.	-75 01.0	N.E. by E.	+69	-35	-74 27	
			Direct.	-75 09.6	N.E. by E.	+69	-35	-74 36	
			Direct.	-75 07.1	N.E. by E.	+69	-35	-74 33	
15.	-58 49	221 25	Direct.	-75 13.7	N.E. by E.	+69	-35	-74 40	
			Direct.	-73 06.6	E.N.E.	+53	-35	-72 49	
			Def. N.	-72 15.7	E.N.E.	+53	-81	-72 44	
			Def. S.	-73 21.2	E.N.E.	+53	-35	-73 03	
			Mag. N.	-73 08.4	E.N.E.	+53	-35	-72 50	
			Mag. N.S.	-73 13.1	E.N.E.	+53	-35	-72 55	
			Mag. S.	-73 07.7	E.N.E.	+53	-35	-72 50	
			Direct.	-73 10.8	E.N.E.	+53	-35	-72 53	
16.	-58 48 -58 59 -59 01	222 22 227 30 227 43	Direct.	-74 05.2	E. by N.	+37	-35	-74 03	
			Direct.	-73 24.8	E.	+21	-35	-73 39	
			Direct.	-73 21.9	E.	+21	-35	-73 36	
			Def. N.	-72 33.3	E.	+21	-81	-73 30	
			Def. S.	-73 14.1	E.	+21	-35	-73 28	
			Mag. N.	-73 00.4	E.	+21	-35	-73 14	
			Mag. N.S.	-73 09.6	E.	+21	-35	-73 24	
			Mag. S.	-73 07.0	E.	+21	-35	-73 21	
17.	-59 32	231 46	Direct.	-73 26.6	E.	+21	-35	-73 41	
			Direct.	-72 41.3	E.	+21	-35	-72 55	
18.	-60 05	235 56	Direct.	-72 19.5	E. by S.	+2	-35	-72 53	Heavy sea from W.S.W., very unsteady, steering very badly.
			Def. N.	-71 10.6	E. by S.	+2	-81	-72 30	
			Def. S.	-72 24.0	E. by S.	+2	-35	-72 57	
			Mag. N.	-72 29.7	E. by S.	+2	-35	-73 03	
			Mag. N.S.	-72 04.7	E. by S.	+2	-35	-72 38	
			Mag. S.	-72 52.0	E. by S.	+2	-35	-73 25	
			Direct.	-73 01.1	E. by N.	+37	-35	-72 59	
			Direct.	-72 59.1	E.	+21	-35	-73 13	
			Def. N.	-71 56.0	E.	+21	-81	-72 56	
			Def. S.	-73 02.3	E.	+21	-35	-73 16	
			Mag. N.	-73 09.9	E.	+21	-35	-73 24	
			Mag. N.S.	-72 59.8	E.	+21	-35	-73 14	
	-60 17 -60 24	236 38 237 29	Mag. S.	-72 54.8	E.	+21	-35	-73 13	Table more steady, and steering very well.
			Direct.	-73 01.8	E.	+21	-35	-73 16	
			Direct.	-73 08.6	E. by N.	+37	-35	-73 06	
			Def. N.	-72 17.2	E. by N.	+37	-81	-73 01	
			Def. S.	-73 09.0	E. by N.	+37	-35	-73 07	
			Mag. N.	-73 09.7	E. by N.	+37	-35	-73 08	
			Mag. N.S.	-73 06.2	E. by N.	+37	-35	-73 04	
			Mag. S.	-73 07.2	E. by N.	+37	-35	-73 05	
			Direct.	-73 07.1	E. by N.	+37	-35	-73 05	
			Direct.	-71 59.1	E.N.E.	+53	-35	-71 41	
			Direct.	-72 17.9	N.E.	+78	-35	-71 35	
			Direct.	-71 23.1	E. by N.	+37	-35	-71 21	
19. 20. 21.	-60 00 -59 18 -59 05	240 57 245 29 247 17	Def. N.	-70 26.9	E. by N.	+37	-81	-71 11	Strong gale, heavy sea, steering badly.
			Def. S.	-71 26.8	E. by N.	+37	-35	-71 25	
			Mag. N.	-71 32.0	E. by N.	+37	-35	-71 30	
			Mag. N.S.	-71 20.1	E. by N.	+37	-35	-71 18	
			Mag. S.	-71 22.7	E. by N.	+37	-35	-71 21	
			Direct.	-71 20.9	E. by N.	+37	-35	-71 19	
			Direct.	-71 53.4	N.E. ½ E.	+73	-35	-71 15	
			Direct.	-71 53.4	N.E. ½ E.	+73	-35	-71 15	
	--59 00	248 49	Direct.	-71 53.4	N.E. ½ E.	+73	-35	-71 15	Head sea, table unsteady.

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.		
						Ship's attraction.	Index.				
Mar. 22.	58° 26'	251° 42'	Direct.	-71° 06.1	E. by N.	+37	-35	-71° 04'	-70 55	Cross sea, unsteady.	
			Def. N.	-70 01.3	E. by N.	+37	-81	-70 45			
			Def. S.	-70 45.2	E. by N.	+37	-35	-70 43			
			Mag. N.	-71 03.3	E. by N.	+37	-35	-71 01			
			Mag. N.S.	-70 44.0	E. by N.	+37	-35	-70 42			
	23.	58 33	254 45	Mag. S.	-71 07.8	E. by N.	+37	-35	-71 06	-70 16	Slight motion.
				Direct.	-71 02.9	E. by N.	+37	-35	-71 01		
				Direct.	-70 24.7	E. ½ N.	+30	-35	-70 30		
				Def. N.	-69 05.4	E. ½ N.	+30	-81	-69 56		
				Def. S.	-69 57.5	E. ½ N.	+30	-35	-70 03		
24.	58 40	257 32	Mag. N.	-70 02.7	E. ½ N.	+30	-35	-70 08	-69 50	Slight motion.	
			Mag. N.S.	-70 21.7	E. ½ N.	+30	-35	-70 27			
			Mag. S.	-70 10.1	E. ½ N.	+30	-35	-70 15			
			Direct.	-70 31.2	E. ½ N.	+30	-35	-70 36			
			Direct.	-70 01.8	E. by N.	+37	-35	-70 00			
	58 49	258 13	Def. N.	-69 09.1	E. by N.	+37	-81	-69 53	-68 00	Heavy sea, steering badly, a little motion.	
			Def. S.	-69 43.7	E. by N.	+37	-35	-69 42			
			Mag. N.	-69 47.0	E. by N.	+37	-35	-69 45			
			Mag. N.S.	-69 37.4	E. by N.	+37	-35	-69 35			
			Mag. S.	-70 03.0	E. by N.	+37	-35	-70 01			
25.	58 53	258 55	Direct.	-70 01.8	E. by N.	+37	-35	-70 00	-66 53	A swell from the W.S.W., ship unsteady.	
			Direct.	-69 52.9	E.	+22	-35	-70 06			
			Direct.	-69 51.1	E. by N.	+37	-35	-69 49			
			Direct.	-69 24.2	E. by N.	+37	-35	-69 32			
			Direct.	-69 17.9	E.N.E.	+53	-35	-69 00			
	26.	58 59	267 50	Direct.	-68 19.8	E. by N. ½ N.	+44	-35	-68 11	-68 00	Heavy sea, steering badly, a little motion.
				Def. N.	-67 03.0	E. by N. ½ N.	+44	-81	-67 40		
				Def. S.	-68 05.4	E. by N. ½ N.	+44	-35	-67 56		
				Mag. N.	-67 44.2	E. by N. ½ N.	+44	-35	-67 35		
				Mag. N.S.	-67 52.6	E. by N. ½ N.	+44	-35	-67 44		
27.	59 01	272 06	Mag. S.	-67 52.5	E. by N. ½ N.	+44	-35	-67 44	-66 53	A swell from the W.S.W., ship unsteady.	
			Direct.	-68 15.6	E. by N. ½ N.	+44	-35	-68 07			
			Direct.	-67 19.3	E.N.E.	+52	-35	-67 02			
			Def. N.	-66 46.0	E.N.E.	+52	-81	-67 15			
			Def. S.	-67 09.6	E.N.E.	+52	-35	-66 53			
	28.	58 54	276 18	Mag. N.	-66 53.0	E.N.E.	+52	-35	-66 36	-66 10	Swell from the W.S.W., ship unsteady.
				Mag. N.S.	-66 59.0	E.N.E.	+52	-35	-66 42		
				Mag. S.	-67 05.8	E.N.E.	+52	-35	-66 49		
				Direct.	-67 17.8	E.N.E.	+52	-35	-67 01		
				Direct.	-67 04.7	E.N.E.	+52	-35	-66 48		
29.	58 25	279 44	Direct.	-66 51.5	N.E. by E.	+64	-35	-66 23	-64 44	Swell from S.W., slight motion.	
			Def. N.	-65 48.2	N.E. by E.	+64	-81	-66 05			
			Def. S.	-66 53.4	N.E. by E.	+64	-35	-66 24			
			Mag. N.	-66 15.2	N.E. by E.	+64	-35	-65 46			
			Mag. N.S.	-66 18.7	N.E. by E.	+64	-35	-65 50			
	29.	58 25	279 44	Mag. S.	-66 51.6	N.E. by E.	+64	-35	-66 23	-64 44	Swell from S.W., slight motion.
				Direct.	-66 51.8	N.E. by E.	+64	-35	-66 23		
				Direct.	-65 05.3	N.E. by E.	+62	-35	-64 38		
				Direct.	-65 27.9	N.E. by E.	+62	-35	-65 01		
				Def. N.	-64 13.0	N.E. by E.	+62	-81	-64 32		
29.	58 25	279 44	Def. S.	-65 20.9	N.E. by E.	+62	-35	-64 54	-64 44	Swell from S.W., slight motion.	
			Mag. N.	-65 03.0	N.E. by E.	+62	-35	-64 36			
			Mag. N.S.	-65 01.6	N.E. by E.	+62	-35	-64 35			
			Mag. S.	-65 08.8	N.E. by E.	+62	-35	-64 42			
			Direct.	-65 22.6	N.E. by E.	+62	-35	-64 56			

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Mar. 30.	—58 31	281 33	Direct.	—64 15.6	E.N.E.	+51	—35	—64 00	} —63 48 Swell from S.W., slight motion.
			Direct.	—64 25.0	N.E. by E.	+62	—35	—63 58	
			Def. N.	—63 11.3	N.E. by E.	+62	—81	—63 30	
			Def. S.	—64 11.8	N.E. by E.	+62	—35	—63 45	
			Mag. N.	—64 05.6	N.E. by E.	+62	—35	—63 39	
			Mag. N.S.	—64 09.8	N.E. by E.	+62	—35	—63 43	
			Mag. S.	—64 27.0	N.E. by E.	+62	—35	—64 00	
			Direct.	—64 17.7	N.E. by E.	+62	—35	—63 51	
			Direct.	—64 14.9	N.E. by E.	+62	—35	—63 48	
			Direct.	—63 42.0	N.E.	+69	—35	—63 08	
			Def. N.	—62 50.6	N.E.	+69	—81	—63 03	
			Def. S.	—63 49.8	N.E.	+69	—35	—63 16	
			Mag. N.	—63 22.5	N.E.	+69	—35	—62 49	
			Mag. N.S.	—63 17.2	N.E.	+69	—35	—62 43	
April 1.	—58 30	282 07	Mag. S.	—63 24.6	N.E.	+69	—35	—62 51	} —63 00 Swell from S.W., slight motion.
			Direct.	—63 44.5	N.E.	+69	—35	—63 11	
			Direct.	—62 26.9	N.E. by N.	+71	—35	—61 51	
			Def. N.	—61 16.8	N.E. by N.	+71	—81	—61 27	
			Def. S.	—62 04.7	N.E. by N.	+71	—35	—61 29	
			Mag. N.	—62 04.4	N.E. by N.	+71	—35	—61 28	
			Mag. N.S.	—62 12.7	N.E. by N.	+71	—35	—61 37	
			Mag. S.	—62 12.4	N.E. by N.	+71	—35	—61 36	
			Direct.	—62 17.0	N.E. by N.	+71	—35	—61 41	
			Direct.	—58 55.8	S.E.	—33	—35	—60 04	
			Def. N.	—57 57.1	S.E.	—33	—81	—59 51	
			Def. S.	—58 43.2	S.E.	—33	—35	—59 51	
			Mag. N.	—58 49.5	S.E.	—33	—35	—59 58	
			Mag. N.S.	—58 29.2	S.E.	—33	—35	—59 37	
2.	—57 26	291 32	Mag. S.	—58 23.7	S.E.	—33	—35	—59 32	} —59 52 Heavy sea, ship unsteady.
			Direct.	—58 59.8	S.E.	—33	—35	—60 08	
			Direct.	—58 22.4	S.S.E.	—62	—35	—59 59	
			Direct.	—59 50.8	N.E.	+65	—35	—59 21	
			Def. N.	—58 33.4	N.E.	+65	—81	—58 49	
			Def. S.	—59 43.5	N.E.	+65	—35	—59 13	
			Mag. N.	—59 19.3	N.E.	+65	—35	—58 49	
			Mag. N.S.	—59 26.3	N.E.	+65	—35	—58 56	
			Mag. S.	—59 21.8	N.E.	+65	—35	—58 52	
			Direct.	—59 45.5	N.E.	+65	—35	—59 16	
			Direct.	—57 27.0	N. by E.	+66	—35	—56 56	
			Def. N.	—56 43.5	N. by E.	+66	—81	—56 58	
			Def. S.	—57 23.2	N. by E.	+66	—35	—56 52	
			Mag. N.	—57 10.4	N. by E.	+66	—35	—56 39	
3.	—56 37	294 34	Mag. N.S.	—57 13.4	N. by E.	+66	—35	—56 42	} —56 48 Heavy sea, strong breeze, steering badly.
			Mag. S.	—57 11.0	N. by E.	+66	—35	—56 40	
			Direct.	—57 19.0	N. by E.	+66	—35	—56 48	
			Direct.	—54 40.0	N.N.E.	+58	—35	—54 17	
			Def. N.	—53 51.3	N.N.E.	+58	—81	—54 14	
			Def. S.	—54 43.4	N.N.E.	+58	—35	—54 20	
			Mag. N.	—54 31.9	N.N.E.	+58	—35	—54 09	
			Mag. N.S.	—54 22.3	N.N.E.	+58	—35	—53 59	
			Mag. S.	—54 15.0	N.N.E.	+58	—35	—53 42	
			Direct.	—54 32.3	N.N.E.	+58	—35	—54 09	
			Direct.	—53 51.0	N.N.E.	+58	—35	—53 28	
			Direct.	—53 08.3	N. by E.	+57	—35	—52 46	
			Def. N.	—52 26.4	N. by E.	+57	—81	—52 50	
			Def. S.	—53 07.9	N. by E.	+57	—35	—52 46	
4.	—54 48	297 21							} —53 25 Ship steady.
5.	—52 35	300 33							
5.	—52 28	300 42							

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
April 5.	—52° 28'	300° 42'	Mag. N.	—52° 50.2	N. by E.	+57	—35	—52° 28'	Ship steady.
			Mag. N.S.	—53 05.2	N. by E.	+57	—35	—52 43	
			Mag. S.	—53 00.8	N. by E.	+57	—35	—52 39	
			Direct.	—53 08.4	N. by E.	+57	—35	—52 46	
6.	—51 42	301 36	Direct.	—52 29.0	N.N.W. $\frac{1}{2}$ W.	+54	—35	—52 10	Strong breeze, slight motion.
			Def. N.	—51 20.0	N.N.W. $\frac{1}{2}$ W.	+54	—81	—51 47	
			Def. S.	—52 35.9	N.N.W. $\frac{1}{2}$ W.	+54	—35	—52 17	
			Mag. N.	—52 16.3	N.N.W. $\frac{1}{2}$ W.	+54	—35	—51 57	
			Mag. N.S.	—52 20.7	N.N.W. $\frac{1}{2}$ W.	+54	—35	—52 02	
			Mag. S.	—52 25.4	N.N.W. $\frac{1}{2}$ W.	+54	—35	—52 06	
			Direct.	—52 24.5	N.N.W. $\frac{1}{2}$ W.	+54	—35	—52 06	
9.	Port Louis, Falkland Islands.		Direct.	—51 32.8	W. $\frac{1}{2}$ N.	+32	—35	—51 36	Single anchor.
			Def. N.	—50 51.4	W. $\frac{1}{2}$ N.	+32	—81	—51 40	
			Def. S.	—52 09.8	W. $\frac{1}{2}$ N.	+32	—35	—52 13	
11.	—51 32	301 53	Direct.	—51 36.7*			—35	—52 12	
			Def. N.	—50 33.0			—81	—51 54	Single anchor.
			Def. S.	—52 08.6			—35	—52 44	
			Mag. N.	—51 33.1			—35	—52 08	
			Mag. N.S.	—51 34.1			—35	—52 09	
			Mag. S.	—51 42.3			—35	—52 17	
July 25.			Direct.	—51 34.4†			—35	—52 09	
			Def. N.	—51 03.7			—81	—52 25	
			Def. S.	—51 58.7			—35	—52 34	
			Mag. N.	—51 32.8			—35	—52 08	
			Mag. N.S.	—51 33.8			—35	—52 09	
			Mag. S.	—51 43.3			—35	—52 18	
			Direct.	—51 31.6‡			—35	—52 07	
			Def. N.	—51 00.8			—81	—52 22	
			Def. S.	—51 58.3			—35	—52 33	
			Mag. N.	—51 31.7			—35	—52 07	
			Mag. N.S.	—51 31.4			—35	—52 06	
			Mag. S.	—51 37.5			—35	—52 13	
			Direct.	—51 31.5			—35	—52 07	
			Direct.	—51 32.2§			—35	—52 07	
			Def. N.	—50 59.9			—81	—52 21	
			Def. S.	—51 58.3			—35	—52 33	
			Mag. N.	—51 31.9			—35	—52 07	
			Mag. N.S.	—51 32.3			—35	—52 07	
			Mag. S.	—51 44.3			—35	—52 19	

* Observed on shore;
face west.

‡ Observed on shore;
face west.

† Observed on shore;
face west.

§ Observed on shore;
face west.

Direct. .. —52° 49.6
Def. N. .. —53 05.3
Def. S. .. —52 48.3
Mag. N... —53 00.8
Mag. N.S. —53 09.7
Mag. S... —53 12.1

Direct. .. —52 39.5
Def. N. .. —53 30.8
Def. S. .. —52 57.9
Mag. N... —53 05.7
Mag. N.S. —53 01.8
Mag. S... —53 12.7
Direct. .. —52 38.6

Direct. .. —52° 48.7
Def. N. .. —53 42.2
Def. S. .. —52 48.4
Mag. N... —53 00.4
Mag. N.S. —53 06.2
Mag. S... —53 05.4

Direct. .. —52 41.5
Def. N. .. —53 46.8
Def. S. .. —52 56.4
Mag. N... —53 04.0
Mag. N.S. —53 02.4
Mag. S... —53 07.6

Observations of Inclination. (Continued.)

1842.	Lat.	Long.	Method employed.	Observed Inclination. Face east.	Direction of ship's head.	Corrections.		True Inclination.	Remarks.
						Ship's attraction.	Index.		
Aug. 15.	Berkeley Sound, Falkland Islands.		Direct.	-51° 31.4	E. $\frac{1}{2}$ S.	+22	-35	-51° 44	
			Def. N.	-51 00.8	E. $\frac{1}{2}$ S.	+22	-81	-52 00	
			Direct.	-51 45.5	E.	+28	-35	-51 52	
			Def. N.	-51 21.2	E.	+28	-81	-52 14	
			Direct.	-51 29.1	E.S.E.	+4	-35	-52 00	
			Def. N.	-51 06.2	E.S.E.	+4	-81	-52 23	
			Direct.	-50 44.9	S.E.	-22	-35	-51 58	
			Def. N.	-50 23.4	S.E.	-22	-81	-52 06	
			Direct.	-50 28.8	S.S.E.	-45	-35	-51 49	
			Def. N.	-49 52.3	S.S.E.	-45	-81	-51 58	
			Direct.	-50 11.7	S.	-52	-35	-51 39	
			Def. N.	-49 38.9	S.	-52	-81	-51 52	
			Direct.	-50 43.1	S.S.W.	-45	-35	-52 03	
			Def. N.	-50 03.0	S.S.W.	-45	-81	-52 09	
			Direct.	-50 48.4	S.W.	-22	-35	-51 45	
			Def. N.	-50 21.3	S.W.	-22	-81	-52 04	
			Direct.	-51 11.2	W.S.W.	+4	-35	-51 42	
			Def. N.	-50 25.0	W.S.W.	+4	-81	-51 42	
			Direct.	-51 31.3	W.	+28	-35	-51 38	
			Def. N.	-50 58.3	W.	+28	-81	-51 51	
			Direct.	-51 59.2	W.N.W.	+44	-35	-51 50	
			Def. N.	-51 22.5	W.N.W.	+44	-81	-52 00	
			Direct.	-52 05.8	N.W.	+52	-35	-51 49	
			Def. N.	-51 27.5	N.W.	+52	-81	-51 57	
			Direct.	-52 13.7	N.N.W.	+54	-35	-51 55	
			Def. N.	-51 14.7	N.N.W.	+54	-81	-51 42	
			Direct.	-52 25.2	N.	+54	-35	-52 06	
			Def. N.	-51 11.7	N.	+54	-81	-51 39	
			Direct.	-52 13.6	N.N.E.	+54	-35	-51 55	
			Def. N.	-51 33.5	N.N.E.	+54	-81	-52 01	
			Direct.	-52 13.0	N.E.	+52	-35	-51 56	
			Def. N.	-51 25.6	N.E.	+52	-81	-51 55	
			Direct.	-52 16.5	E.N.E.	+44	-35	-52 08	
			Def. N.	-51 29.7	E.N.E.	+44	-81	-52 07	

Observations of the INTENSITY of the Magnetic Force made in Her Majesty's Ship
Erebus, with Needle R. F. 5, between April 17, 1841, and August 23, 1842.

Observers Captain Sir JAMES CLARK ROSS and Lieutenant ALEXANDER SMITH, R.N.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Apr. 19.	Magnetic Observatory, Hobarton. —42 52 147 24		Def. S.	56 28.6	64	Observed on shore.	1.820 1.820	Deflector employed R. F. 4.
			Def. N.	53 02.6	63					
			wt. 6 grs.	42 55.7	61					
			wt. 5 grs.	34 23.5	60					
			wt. 4 grs.	26 47.7	60					
			wt. 3 grs.	19 37.2	60					
20.	At anchor in the river Derwent.	To obtain corrections for the ship's attraction.	wt. 2 grs.	13 02.8*	60	N. N.N.E. N.E. E.N.E. E. E.S.E. S.E. S.S.E. S S.S.W. S.W. W.S.W. W. W.N.W. N.W. N.N.W. N. S.E. ½ E. S.E. ½ E. N.N.E. N.N.E. N.N.W. N.N.W. N. N. by w. N. by w. N. by w. N.E. N.E. N.W. by N. N. N. Observed on shore.	1.809 1.806 1.815 1.820 1.821 1.825 1.846 1.851 1.854 1.849 1.847 1.832 1.825 1.830 1.817 1.818 1.815 1.858 1.854 1.823 1.807 1.790 1.785 1.786 1.773 1.732 1.742 1.722 1.715 1.676 1.679 1.698 1.694 1.698 1.680 1.683 1.687 1.703 1.696 1.692	+0.024 +0.022 +0.018 +0.013 +0.004 -0.006 -0.016 -0.023 -0.026 -0.023 -0.016 -0.006 +0.004 +0.013 +0.018 +0.022 +0.024 -0.014 +0.022 +0.022 +0.024 +0.022 +0.022 +0.024 +0.027 +0.031 1.832 1.828 1.833 1.833 1.825 1.819 1.830 1.828 1.822 1.826 1.831 1.826 1.829 1.843 1.835 1.840 1.839 1.842 1.842 1.837 1.837 1.809 1.809 1.804 1.804 1.756 } 1.755 1.754 } 1.742 } 1.720 1.708 } 1.685 1.685	} 1.830 A heavy head swell. A head swell. <

* Observed on shore; face west.

wt. 6 grs. . . 43 07.5	Ther. 58
wt. 5 grs. . . 34 51.5	Ther. 58
wt. 4 grs. . . 27 02.7	Ther. 58
wt. 3 grs. . . 19 55.5	Ther. 60
wt. 2 grs. . . 13 14.5	Ther. 60

† Observed on shore; face west.

wt. 6 grs. . . 47 32.4	Ther. 63	Intensity. 1.688
wt. 5 grs. . . 37 38.9	Ther. 63	1.704
wt. 4 grs. . . 29 32.1	Ther. 64	1.680
wt. 3 grs. . . 21 51.4	Ther. 63	1.667
wt. 2 grs. . . 14 32.6	Ther. 64	1.662

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
July 15.	—33° 51'	151 17	Def. S.	59° 11' 5	64	w.	1.696	+007	1.703	1.705
Aug. 1.	At anchor.		Def. S.	58 21.4	61	s.	1.733	—032	1.701	
			Def. S.	58 15.6	61	S.S.W.	1.737	—028	1.709	
3.			Def. S.	59 29.0	63	N.E.	1.684	+025	1.709	
5.	Running out of harbour.		Def. S.	59 09.4	63	E. by N.	1.698	+011	1.709	
			Def. N.	55 46.8	63	E. by N.	1.686	+011	1.697	1.694
6.	—32 52	154 07	Def. S.	59 25.6	63	E. by N.	1.686	+011	1.694	
			Def. N.	55 52.6	63	E. by N.	1.681			1.667
7.	—33 51	157 18	Def. S.	60 05.3	60	E. by N.	1.660	+011	1.667	
			Def. N.	56 30.2	61	E. by N.	1.652			1.655
8.	—33 27	160 43	Def. S.	60 18.0	63	E. by N.	1.651	+011	1.655	
			Def. N.	56 53.1	64	E. by N.	1.638			1.642
9.	—33 38	163 42	Def. S.	60 24.0	60	E.	1.647	+007	1.642	
			Def. N.	57 14.4	61	E.	1.623			1.625
10.	—33 41	166 23	Def. S.	61 22.7	63	N.E.	1.609	+025	1.625	
			Def. N.	58 01.2	61	N.E.	1.591			1.617
11.	—33 22	167 40	Def. S.	61 19.8	65	E. by N.	1.611	+012	1.617	
			Def. N.	57 49.4	67	E. by N.	1.599			1.607
12.	—32 58	169 20	Def. S.	61 40.0	56	E.N.E.	1.598	+017	1.607	
			Def. N.	58 14.8	56	E.N.E.	1.582			1.583
13.	—32 12	170 27	Def. S.	62 24.2	56	S.E. by E.	1.572	—012	1.562	
			Def. N.	58 24.4	55	S.E. by E.	1.576			1.594
15.	—33 55	171 54	Def. S.	61 35.7	60	E. $\frac{1}{2}$ S.	1.590	+004	1.593	
			Def. N.	53 05.6	60	E. $\frac{1}{2}$ S.	1.588			1.607
17.	—34 29	173 36	Def. S.	61 20.0	62	E.S.E.	1.611	—006	1.594	
			Def. N.	58 02.7	62	E.S.E.	1.590			1.602
20.	At anchor.		Def. S.	61 57.7	66	N.W. $\frac{1}{2}$ N.	1.587	+025	1.612	
			Def. S.	60 42.9	63	S.	1.634	—032	1.602	The results with the face west are included in the mean.
23.	Bay of Islands, New Zealand.		Def. S.	61 41.1	58		1.599			
	—35 16	174 00	Def. N.	58 00.0	56		1.592			
			wt. 6 grs.	50 38.1	58		1.604			
			wt. 5 grs.	40 10.5	58		1.594			
			wt. 4 grs.	30 55.0	59		1.597			
			wt. 3 grs.	22 47.5	59		1.578			
			wt. 2 grs.	14 59.3*	59		1.590			
Oct. 27.	—35 16	174 00	Def. S.	61 45.2	67	Observed on shore.	1.595	1.594	
			Def. N.	57 47.1	70		1.600			
			wt. 6 grs.	50 35.0	71		1.608			The results with the face west are included in the mean.
			wt. 5 grs.	39 59.3	70		1.603			
			wt. 4 grs.	30 30.6	70		1.619			
			wt. 3 grs.	22 45.0	70		1.583			
			wt. 2 grs.	14 43.2	68		1.620			
			Def. S.	61 54.4	65		1.590			
			Def. N.	58 09.1†	65		1.586			
Nov. 23.	—35 15	174 39	Def. S.	61 00.9	63	E.S.E.	1.623	—006	1.611	
			Def. N.	57 29.1	63	E.S.E.	1.611			
24.	—36 27	177 34	Def. S.	61 26.7	65	E.S.E.	1.607	—006	1.612	
			Def. N.	57 12.7	64	E.S.E.	1.625			

* Observed on shore; face west.

wt. 6 grs.. 51 26.0	Ther. 61	Intensity. 1.591
wt. 5 grs.. 40 52.0	Ther. 60	Intensity. 1.590
wt. 4 grs.. 30 26.9	Ther. 59	Intensity. 1.633
wt. 3 grs.. 23 17.9	Ther. 59	Intensity. 1.568
wt. 2 grs.. 15 23.3	Ther. 60	Intensity. 1.571

† Observed on shore; face west.

wt. 6 grs.. 51 38.7	Ther. 65	Intensity. 1.588
wt. 5 grs.. 40 51.0	Ther. 65	Intensity. 1.591
wt. 4 grs.. 31 29.2	Ther. 65	Intensity. 1.586
wt. 3 grs.. 23 17.2	Ther. 64	Intensity. 1.570
wt. 2 grs.. 15 11.1	Ther. 64	Intensity. 1.593

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.	
Nov. 25.	—38 17	179 31	Def. S	60 44.4	62	S.E. by S.	1.633	—020	1.614 1.614	Very much motion.	
			Def. N.	56 57.2	62	S.E. by S.	1.634				
26.	—39 01	182 12	Def. S.	62 02.7	59	E. by S.	1.585	—000	1.605		1.615
			Def. N.	57 12.9	57	E. by S.	1.625				
27.	—39 18	182 58	Def. S.	60 16.0	64	S.	1.652	—028	1.625		
			Def. N.	56 29.9	62	S.	1.654				
28.	—40 47	183 03	Def. S.	59 58.5	62	S.E. by E.	1.664	—010	1.659 1.659		
			Def. N.	56 03.4	65	S.E. by E.	1.674				
29.	—41 49	183 41	Def. S.	59 05.1	65	S. by E.	1.701	—026	1.671 1.671		
			Def. N.	55 37.2	65	S. by E.	1.693				
30.	—43 32	183 03	Def. S.	58 24.9	60	S. $\frac{1}{2}$ W.	1.732	—027	1.701 1.701		
			Def. N.	54 54.9	59	S. $\frac{1}{2}$ W.	1.724				
Dec. 1.	—45 40	183 20	Def. S.	58 32.2	63	S.E. by E.	1.725	—010	1.715	A head sea.	
			Def. N.	54 58.7	63	S.E. by E.	1.722			A heavy swell.	
2.	—47 19	184 40	Def. S.	57 40.9	57	S.E. by E. $\frac{1}{2}$ E.	1.762	—008	1.745		1.730
			Def. N.	54 30.5	57	S.E. by E. $\frac{1}{2}$ E.	1.744				
3.	—48 43	186 30	Def. S.	57 41.3	51	S.E. by E.	1.762	—009	1.752		
			Def. N.	54 10.1	51	S.E. by E.	1.760				
			wt. 2 grs.	13 28.0	51	E.S.E.	1.765	—005	1.760		1.753
4.	—49 20	187 41	Def. S.	57 45.8	55	E. by S.	1.757				
			Def. N.	54 13.1	55	E. by S.	1.758	—000	1.752		
			wt. 3 grs.	20 30.2	53	E. by S.	1.745				
			wt. 4 grs.	27 58.0	53	E. by S.	1.750	—000	1.759 1.759		
5.	—49 27	189 13	Def. S.	57 32.7	55	E. by S.	1.770				
			Def. N.	54 16.0	55	E. by S.	1.757	—000	1.762		
			wt. 3 grs.	20 18.0	56	E. by S.	1.762				
			wt. 4 grs.	27 32.0	56	E. by S.	1.775	—000	1.775		
			wt. 5 grs.	36 30.1	56	E. by S.	1.729				
6.	—50 00	191 00	Def. S.	57 30.2	51	E. by S.	1.771	—000	1.763		1.766
			Def. N.	54 13.5	51	E. by S.	1.758				
			wt. 3 grs.	20 22.2	51	E. by S.	1.754	—000	1.779		
			wt. 4 grs.	27 16.5	51	E. by S.	1.789				
			wt. 5 grs.	36 07.2	51	E. by S.	1.742	—009	1.774		
7.	—50 48	192 20	Def. S.	57 07.9	51	S.E. by E.	1.787				
			Def. N.	53 45.7	51	S.E. by E.	1.779	—000	1.792 1.792		
8.	—51 34	194 29	Def. S.	57 06.4	52	E. by S.	1.789				
			Def. N.	53 15.7	50	E. by S.	1.804	—000	1.801		Weight 5, unsteady.
			wt. 3 grs.	20 09.1	48	E. by S.	1.771				
			wt. 4 grs.	26 59.7	48	E. by S.	1.804	—000	1.815		Much motion.
			wt. 5 grs.	34 58.0	47	E. by S.	1.791				
9.	—52 21	197 53	Def. S.	56 44.5	45	E. by S.	1.805	—000	1.801		
			Def. N.	53 25.1	44	E. by S.	1.797				
10.	—53 01	202 11	Def. S.	56 21.2	48	E. $\frac{1}{2}$ N.	1.824	+006	1.815	1.808	
			Def. N.	53 27.0	47	E. $\frac{1}{2}$ N.	1.794				
11.	—52 48	203 50	Def. N.	53 13.3	45	E.	1.807	+003	1.809	A head swell.	
			Def. S.	56 45.0	46	E.	1.805				
			wt. 3 grs.	19 57.7	46	E.	1.797	—004	1.810 1.810		
12.	—53 01	205 08	Def. S.	56 37.4	45	E.S.E.	1.811				
			Def. N.	52 57.3	44	E.S.E.	1.818	—004	1.810 1.810		
			wt. 3 grs.	19 46.7	45	E.S.E.	1.802				
			wt. 4 grs.	26 41.5	45	E.S.E.	1.823	—007	1.831 1.831		
			wt. 5 grs.	34 25.7	45	E.S.E.	1.815				
13.	—54 55	209 30	Def. S.	56 08.7	52	S.E. by E. $\frac{1}{2}$ E.	1.833	—007	1.831 1.831		
			Def. N.	52 26.0	51	S.E. by E. $\frac{1}{2}$ E.	1.846				
	—55 08	210 04	Def. S.	56 02.2	49	S.E. by E. $\frac{1}{2}$ E.	1.839	—007	1.831 1.831		
			Def. N.	52 30.7	48	S.E. by E. $\frac{1}{2}$ E.	1.842				
	—55 20	210 28	Def. S.	56 10.0	45	S.E. by E. $\frac{1}{2}$ E.	1.832	—007	1.831 1.831		
			Def. N.	52 38.2	44	S.E. by E. $\frac{1}{2}$ E.	1.836				

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 14.	—56° 20'	211° 52'	Def. S.	55° 38.9	51	S.E. by S.	1.857	—016	1.836	1.836
			Def. N.	52° 01.3	51	S.E. by S.	1.868			
			wt. 3 grs.	19° 37.5	53	S.E. by S.	1.818			
			wt. 4 grs.	26° 08.7	52	S.E. by S.	1.860			
			wt. 5 grs.	33° 36.0	52	S.E. by S.	1.856			
			wt. 6 grs.	42° 36.0	52	S.E. by S.	1.830			
15.	—56° 55'	211° 38'	Def. S.	55° 33.2	43	S.E. by S.	1.863	—017	1.843	1.850
			Def. N.	51° 59.7	43	S.E. by S.	1.868			
			Def. S.	55° 28.0	41	S.S.E.	1.865			
			Def. N.	52° 17.0	40	S.S.E.	1.856			
			Def. S.	55° 29.8	42	F.S.E.	1.864			
			Def. N.	52° 10.0	41	E.S.E.	1.860			
16.	—58° 29'	213° 11'	Def. S.	55° 19.7	42	S.S.E.	1.872	—004	1.858	1.873
			Def. N.	51° 52.9	42	S.S.E.	1.874			
			Def. S.	54° 57.6	41	S.S.E.	1.889			
			Def. N.	52° 04.5	41	S.S.E.	1.865			
			wt. 3 grs.	18° 32.2	38	S.S.E.	1.916			
			wt. 4 grs.	25° 25.0	38	S.S.E.	1.906			
17.	—61° 03'	213° 57'	wt. 5 grs.	32° 31.2	38	S.S.E.	1.907	—017	1.903	1.908
			Def. S.	54° 19.2	39	S.S.E.	1.923			
			Def. N.	51° 06.0	36	S.S.E.	1.918			
			Def. S.	54° 02.4	34	S. by E.	1.939			
			Def. N.	51° 01.2	32	S. by E.	1.922			
			Def. S.	53° 43.6	34	S.	1.953			
18.	—62° 40'	212° 53'	Def. N.	50° 50.0	32	S.	1.931	—019	1.922	1.922
			Def. S.	53° 39.8	39	S.S.W.	1.958			
			Def. N.	50° 26.0	38	S.E.W.	1.954			
			Def. S.	54° 33.8	42	Observed	1.910			
			Def. N.	50° 44.7	45	on ice.	1.936			
			Def. S.	53° 58.3	35	S. by W.	1.941			
20.	—63° 47'	208° 26'	Def. N.	50° 36.8	34	S. by W.	1.944	—018	1.924	1.930
			wt. 3 grs.	18° 22.9	35	S.W. by S.	1.938			
			wt. 4 grs.	25° 05.6	34	S.W. by S.	1.935			
			wt. 5 grs.	32° 11.8	34	S.W. by S.	1.926			
			wt. 6 grs.	40° 03.5	34	S.W. by S.	1.926			
			Def. S.	54° 00.1	32	S.	1.940			
21.	—64° 38'	206° 53'	Def. N.	50° 35.6	31	S.	1.944	—016	1.926	1.933
			Def. S.	53° 34.4	44	S. by W.	1.963			
			Def. N.	50° 23.4	39	S. by W.	1.956			
			wt. 3 grs.	18° 15.6	33	S. $\frac{1}{2}$ E.	1.942			
			wt. 4 grs.	24° 39.8	33	S.	1.959			
			wt. 5 grs.	31° 35.1	33	S. by E.	1.955			
22.	—65° 36'	205° 32'	wt. 6 grs.	39° 11.3	33	S. by E.	1.954	—015	1.939	1.955
			Def. S.	53° 33.1	37	S.	1.964			
			Def. N.	50° 00.6	36	S.	1.977			
			Def. S.	53° 51.4	44	E.N.E.	1.948			
			Def. S.	53° 38.5	37	S. by W.	1.959			
			Def. N.	49° 48.2	36	S. by W.	1.996			
23.	—65° 59'	204° 16'	Def. S.	53° 31.5	39	S.	1.965	—014	1.956	1.957
			Def. N.	50° 05.6	35	S.	1.973			
			Def. S.	53° 21.6	43	S.W. by S.	1.976			
			Def. N.	50° 19.8	43	S.W. by S.	1.959			
			Def. S.	53° 56.5	34	E.	1.943			
			Def. N.	50° 19.4	35	E.	1.959			
24.	—65° 58'	203° 51'	Def. S.	53° 43.3	30	S.E. by E.	1.955	—005	1.954	Fast to a piece of ice.
			Def. N.	50° 16.2	30	S.E. by E.	1.963			
			Def. S.	54° 01.9	30	N.W.	1.939			
			Def. S.	53° 51.7	42	N.E.	1.947			
			Def. S.	53° 51.7	42	N.E.	1.947			
			Def. S.	53° 51.7	42	N.E.	1.947			
25.	—66° 00'	203° 46'	Def. S.	53° 56.5	34	E.	1.943	+002	1.953	1.953
			Def. N.	50° 19.4	35	E.	1.959			
			Def. S.	53° 43.3	30	S.E. by E.	1.955			
			Def. N.	50° 16.2	30	S.E. by E.	1.963			
			Def. S.	54° 01.9	30	N.W.	1.939			
			Def. S.	53° 51.7	42	N.E.	1.947			
26.	—66° 11'	203° 36'	Def. S.	53° 51.7	42	N.E.	1.947	+010	1.953	1.953
			Def. S.	53° 51.7	42	N.E.	1.947			
			Def. S.	53° 51.7	42	N.E.	1.947			
			Def. S.	53° 51.7	42	N.E.	1.947			
			Def. S.	53° 51.7	42	N.E.	1.947			
			Def. S.	53° 51.7	42	N.E.	1.947			

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Jan. 1.	—66 32	203 32	Def. S.	53 23.8	44	S.S.E.	1.972	—0.012	1.966	Fast to a piece of ice, the Terror distant 25 fathoms. (This result is not employed in the Map.)
			Def. N.	49 53.5	44	S.S.E.	1.984			
3.	—66 35	203 25	Def. S.	53 48.9	39	N. by W. $\frac{1}{2}$ W.	1.950	+0.012	1.965	
			Def. N.	50 21.7	37	N. by W. $\frac{1}{2}$ W.	1.957			
6.	—66 06	204 24	Def. S.	53 28.7	41	S.	1.967			
			Def. N.	50 01.7	38	S.	1.976			
			wt. 3 grs.	18 01.8	37	S.	1.964			Sailing through loose ice.
			wt. 4 grs.	24 44.9	37	S.	1.953	—0.014	1.955	
			wt. 5 grs.	30 55.2	36	S.	1.994			
			wt. 6 grs.	38 50.1	36	S.	1.970			
7.	—66 13	204 25	Def. S.	53 38.9	33	S.	1.958			
			Def. N.	50 07.5	32	S.	1.971			
8.	—66 12	204 33	Def. S.	53 50.4	35	N.W.	1.948	+0.010	1.958	
			Def. N.	50 32.2	35	N.W.	1.948			
			Def. S.	53 47.9	34	S.S.E.	1.951	—0.012	1.939	
10.	—65 59	204 12	Def. S.	53 49.5	36	S.W. by W.	1.949	—0.005	1.947	
			Def. N.	50 25.4	30	S.W. by W.	1.955			
			Def. N.	50 15.4	30	E.	1.964			
			wt. 3 grs.	18 09.9	30	E.	1.951			1.957
			wt. 4 grs.	24 37.5	30	E.	1.960	+0.002	1.966	
			wt. 5 grs.	31 12.1	30	E.	1.975			
			wt. 6 grs.	38 45.9	30	E.	1.971			
12.	—65 54	203 32	Def. S.	53 33.4	32	S.W.	1.963	—0.008	1.955	
13.	—66 12	203 05	Def. S.	53 41.3	40	S.S.E.	1.957	—0.012	1.949	
			Def. N.	50 13.9	36	S.S.E.	1.965			1.946
			Def. S.	54 11.3	30	N.N.E.	1.932	+0.012	1.946	
			Def. N.	50 46.1	30	N.N.E.	1.935			
16.	—65 49	202 02	Def. S.	54 03.1	45		1.938			
			Def. N.	50 35.0	45		1.945			
			wt. 2 grs.	12 13.0	50		1.940			Observed on ice.
			wt. 3 grs.	18 32.4	54		1.992			
			wt. 4 grs.	24 49.3	54		1.952			
			wt. 5 grs.	32 02.4	54		1.936			
			wt. 6 grs.	39 31.4	55		1.946			
21.	—66 49	202 40	Def. S.	53 19.1	37	S. by E.	1.975	—0.013	1.961	1.960
			Def. N.	50 05.6	36	S. by E.	1.973			
28.	—67 33	204 01	Def. N.	50 24.8	34	N.	1.955	+0.012	1.967	
29.	—67 32	203 59	Def. S.	53 28.8	31	S.S.W.	1.967	—0.012	1.957	
			Def. N.	50 08.2	30	S.S.W.	1.971			
30.	—67 18	203 39	Def. S.	53 35.7	38	S.W. $\frac{1}{2}$ S.	1.961			
			Def. N.	50 06.7	36	S.W. $\frac{1}{2}$ S.	1.972	—0.009	1.959	
			wt. 3 grs.	18 00.0	34	S.W. $\frac{1}{2}$ S.	1.970			
31.	—67 21	202 15	Def. S.	53 36.7	35	S.W.	1.961			
			Def. N.	50 08.2	32	S.W.	1.971			
			wt. 3 grs.	18 19.6	33	S.W.	1.936	—0.008	1.951	
			wt. 4 grs.	24 44.5	33	S.W.	1.953			1.951
			wt. 5 grs.	31 23.7	35	S.W.	1.965			
			wt. 6 grs.	38 52.0	35	S.W.	1.968			
Feb. 2.	—68 07	200 15	Def. S.	53 23.2	31	S.S.E. $\frac{1}{2}$ E.	1.972	—0.011	1.971	
			Def. N.	49 46.2	31	S.S.E. $\frac{1}{4}$ E.	1.992			
3.	—68 21	200 03	Def. S.	52 54.7	32	S.E. by S.	1.997	—0.010	1.981	1.975 Much motion.
			Def. N.	49 52.6	31	S.E. by S.	1.985			
4.	—68 42	199 44	Def. S.	52 57.1	33	S. $\frac{1}{2}$ E.	1.995			
			Def. N.	49 51.4	30	S. $\frac{1}{2}$ E.	1.987			
			wt. 3 grs.	18 05.7	30	S. $\frac{1}{2}$ E.	1.961	—0.014	1.974	
			wt. 4 grs.	23 55.7	29	S. $\frac{1}{2}$ E.	2.014			
			wt. 5 grs.	31 02.0	30	S. $\frac{1}{2}$ E.	1.985			

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.	
Feb. 5.	—68 59	195 51	Def. S.	53 13.7	33	s.w. by s.	1.981	—004	1.972	1.985 A great deal of motion.	
			Def. N.	50 07.0	32	s.w. by s.	1.972				
6.	—69 48	192 25	Def. S.	52 42.1	36	s. by w.	2.010	—008	1.991		
			Def. N.	49 49.0	34	s. by w.	1.989				
7.	—70 05	191 10	Def. S.	52 46.1	29	s.w.	2.006	—005	2.008		
			Def. N.	49 18.3	29	s.w.	2.020				
			Def. S.	53 21.7	33	s.s.w.	1.973	—007	1.972		
			Def. N.	49 52.7	30	s.s.w.	1.985				
8.	—70 18	186 01	Def. S.	53 05.0	37	s.	1.989	—009	1.977		
			Def. N.	49 46.8	33	s.	1.991				
			wt. 3 grs.	18 21.8	31	s.	1.931				
			wt. 4 grs.	24 06.1	31	s.	2.001				
			wt. 5 grs.	30 40.6	31	s.	2.006				
			wt. 6 grs.	38 05.3	30	s.	2.001				
9.	—70 39	185 31	Def. S.	52 56.5	32	s.e. by s.	1.996	—006	1.987		
			Def. N.	49 47.4	29	s.e. by s.	1.991				
10.	—70 06	181 50	Def. S.	53 09.0	33	w. by s.	1.985	000	1.981	A head swell.	
			Def. N.	50 00.2	31	w. by s.	1.978				
11.	—70 10	181 34	Def. N.	50 03.7	33	s.w.	1.975	—005	1.972	1.983 Much motion.	
12.	—71 00	180 44	Def. S.	52 49.2	33	s.e. by s.	2.003				
			Def. N.	49 45.7	32	s.e. by s.	1.992	—005	1.992	A heavy cross sea.	
13.	—72 46	181 46	Def. S.	52 55.6	34	s.e. by s.	1.997				
			Def. N.	49 45.5	32	s.e. by s.	1.992	—003	1.973	1.973	
			wt. 3 grs.	18 17.2	31	s.e. by s.	1.940				
			wt. 4 grs.	24 23.0	31	s.e. by s.	1.975				
16.	—74 56	173 36	Def. S.	53 16.1	26	s.s.e.	1.979				
			Def. N.	49 49.5	26	s.s.e.	1.988	—003	1.998	2.008 Very unsteady.	
			wt. 3 grs.	17 23.0	26	s.s.e.	2.036				
	—75 10	173 08	Def. S.	52 39.5	36	E.	2.017	+001	2.009		
			Def. N.	49 45.9	30	E.	1.992				
			wt. 3 grs.	17 20.9	27	E.	2.039				
			wt. 4 grs.	23 58.7	27	E.	2.009				
			wt. 5 grs.	30 59.1	28	E.	1.987	+002	2.010		
			wt. 6 grs.	38 02.3	27	E.	2.002				
17.	—76 00	175 15	Def. S.	52 38.3	33	E.N.E.	2.014				
			Def. N.	49 33.5	31	E.N.E.	2.004	+002	2.003		2.005 Ship pitching.
18.	—76 58	181 03	Def. S.	53 00.7	28	E.N.E.	1.993				
			Def. N.	49 29.3	27	E.N.E.	2.009	+004	2.001		
19.	—76 42	184 09	Def. S.	53 06.2	25	N. by E.	1.988				
			Def. N.	49 31.3	25	N. by E.	2.007	+004	1.999		
22.	—76 42	194 48	Def. S.	52 59.0	30	N. by E.	1.993				
			Def. N.	49 41.0	28	N. by E.	1.997				
	—77 05	194 38	Def. S.	53 10.6	36	E. by s.	1.984	+001	1.991	1.993 A swell from the south.	
			Def. N.	49 57.5	33	E. by s.	1.981				
			wt. 3 grs.	18 06.5	29	E. by s.	1.960				
			wt. 4 grs.	23 18.7	29	E. by s.	2.063				
			wt. 5 grs.	31 25.7	29	E. by s.	1.961				
			wt. 6 grs.	38 04.1	29	E. by s.	2.000				
25.	—74 50	193 45	Def. S.	53 14.8	30	w.	1.980	+001	1.983	1.983	
			Def. N.	49 54.3	29	w.	1.984				
26.	—72 46	189 59	Def. S.	53 30.5	37	N.W. by W.	1.966	+002	1.972		
			Def. N.	50 04.5	31	N.W. by W.	1.974				
27.	—72 01	187 35	Def. S.	53 32.7	26	w. by s.	1.964	+000	1.976		
			Def. N.	49 49.1	25	w. by s.	1.989				
28.	—71 08	184 59	Def. S.	53 27.6	31	w.	1.968	+001	1.975		1.993
			Def. N.	49 57.0	26	w.	1.981				
			wt. 3 grs.	17 39.5	25	W.S.W.	2.004	000	2.012		
			wt. 4 grs.	23 52.0	25	W.S.W.	2.020				

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 1.	-69 52	180 00	Def. S.	53 10.7	33	w. by N.	1.983	+0.003	1.980	A swell from the northward.
			Def. N.	50 06.0	31	w. by N.	1.972			
	-69 44	179 53	Def. S.	53 28.1	32	N. by E.	1.968	+0.007	1.976	
			Def. N.	50 09.7	29	N. by E.	1.969			
2.	-68 04	183 25	Def. S.	54 05.0	33	N.N.E.	1.936	+0.008	1.962	A swell from the northward.
			Def. N.	50 06.7	32	N.N.E.	1.972			
			Def. S.	53 46.5	34	N.E. by N.	1.951	+0.008	1.969	
			Def. N.	50 09.3	32	N.E. by N.	1.970			
3.	-67 32	185 09	Def. S.	53 24.5	30	E.N.E.	1.971	+0.005	1.976	A very heavy swell from westward, observations very uncertain.
			Def. N.	50 08.8	31	E.N.E.	1.971			
	-67 16	188 10	Def. N.	50 40.2	35	N. by E.	1.941	+0.010	1.952	
	-65 25	191 48	Def. N.	50 38.3	34	N. by E.	1.943			
6.	-63 30	194 52	Def. S.	54 11.9	40	N. by E.	1.930	+0.010	1.936	A very heavy swell from westward, observations very uncertain.
			Def. N.	50 54.2	35	N. by E.	1.927			
			wt. 3 grs.	18 26.2	33	N. by E.	1.925			
			wt. 4 grs.	25 10.3	33	N. by E.	1.922			
8.	-62 16	196 10	Def. S.	54 52.7	35	N. by E.	1.893	+0.010	1.903	A swell from the northward.
			Def. N.	51 32.2	35	N. by E.	1.893			
9.	-61 14	198 38	Def. S.	54 38.4	43	N.E. by N.	1.907	+0.013	1.914	
			Def. N.	51 23.2	35	N.E. by N.	1.902			
			wt. 3 grs.	19 06.9	33	N.E. by N.	1.859			A swell from the northward.
			wt. 4 grs.	25 25.5	35	N.E. by N.	1.905			
			wt. 5 grs.	32 00.5	34	N.E. by N.	1.933			
	-60 50	200 11	Def. S.	55 00.4	38	E.N.E.	1.888	+0.007	1.895	
			Def. N.	51 37.2	35	E.N.E.	1.888			Cross sea, ship very unsteady.
10.	-60 18	204 11	Def. S.	55 52.5	35	E. by N.	1.844	+0.005	1.869	
			Def. N.	51 56.5	34	E. by N.	1.871			
12.	-60 13	211 34	Def. S.	55 28.0	35	E. by N.	1.862			
			Def. N.	51 47.5	35	E. by N.	1.879			A heavy swell, very unsteady.
14.	-59 24	218 58	Def. S.	55 52.2	37	N.E. by E.	1.846	+0.011	1.863	
			Def. N.	52 20.0	37	N.E. by E.	1.851			
	-59 16	219 30	Def. S.	55 37.4	37	N.E. by E.	1.859			
			Def. N.	52 18.2	37	N.E. by E.	1.853			A heavy swell, very unsteady.
15.	-58 04	222 04	Def. S.	55 54.2	37	E.N.E.	1.844	+0.009	1.864	
			Def. N.	52 16.4	37	E.N.E.	1.844			
			wt. 3 grs.	18 57.0	38	E.N.E.	1.876			
16.	-59 04	228 57	Def. S.	55 28.7	39	E.	1.864	+0.002	1.869	A great deal of motion.
			Def. N.	51 57.5	39	E.	1.870			
17.	-59 39	232 48	Def. S.	55 21.3	39	E. 1/2 S.	1.872	+0.001	1.878	
			Def. N.	51 57.5	39	E. 1/2 S.	1.870			
	-59 45	233 53	Def. S.	55 12.0	40	E. 1/2 S.	1.879			Very unsteady.
			Def. N.	51 41.2	38	E. 1/2 S.	1.885			
18.	-60 16	236 11	Def. S.	54 40.7	36	E. by S.	1.901	+0.000	1.897	
			Def. N.	51 33.2	35	E. by S.	1.893			
			Def. S.	55 00.2	37	E.	1.888	+0.003	1.892	Ship rolling, very unsteady.
	-60 21	237 02	Def. S.	55 12.5	39	E.	1.879			
			Def. N.	51 25.6	39	E.	1.899	+0.009	1.890	
	-60 20	237 50	Def. S.	55 33.4	39	E. by N.	1.862			
			Def. N.	51 25.5	39	E. by N.	1.899	+0.010	1.894	Much motion.
	-60 19	238 00	Def. S.	55 10.2	40	E. by N. 1/2 N.	1.880			
			Def. N.	51 37.9	39	E. by N. 1/2 N.	1.887			
19.	-60 01	241 38	Def. S.	55 58.9	39	E.N.E.	1.841	+0.011	1.851	
			Def. N.	52 25.0	37	E.N.E.	1.846			A swell from the northward.
			Def. S.	56 13.5	42	F.N.E.	1.829	+0.009	1.839	
			Def. N.	52 30.0	40	E.N.E.	1.842			
21.	-59 15	248 12	Def. S.	56 07.0	39	E. by N.	1.836	+0.015	1.841	
			Def. N.	52 51.5	38	E. by N.	1.824			A swell from the northward.
	-58 58	249 24	Def. S.	56 11.2	39	N.E. by E.	1.831			
			Def. N.	52 56.0	38	N.E. by E.	1.820			

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 22.	-58° 29'	252° 22'	Def. S.	56° 30.5	38	E. $\frac{1}{2}$ S.	1.816	+0.002	1.816	A head sea.
			Def. N.	53° 05.6	38	E. $\frac{1}{2}$ S.	1.812			
23.	-58 35	255 10	Def. S.	56° 36.0	34	E. $\frac{1}{2}$ N.	1.812			
			Def. N.	53° 13.2	33	E. $\frac{1}{2}$ N.	1.807	+0.006	1.804	
25.	-58 44	257 49	Def. S.	56° 35.8	36	E. $\frac{1}{2}$ N.	1.812			
			Def. N.	53° 16.7	35	E. $\frac{1}{2}$ N.	1.803			
			wt. 3 grs.	20° 17.0	34	E. $\frac{1}{2}$ N.	1.756	+0.012	1.783	Ship unsteady.
26.	-59 02	268 30	Def. S.	57° 19.2	47	E. by N. $\frac{1}{2}$ N.	1.778			
			Def. N.	54° 05.2	45	E. by N. $\frac{1}{2}$ N.	1.763			
27.	-59 02	272 02	Def. S.	58° 55.6	37	E.N.E.	1.707	+0.014	1.722	
			Def. N.	55° 17.7	35	E.N.E.	1.708			
28.	-58 50	277 12	Def. S.	59° 34.0	40	N.E. by E.	1.681			
			Def. N.	56° 07.7	39	N.E. by E.	1.671	+0.018	1.694	
29.	-58 23	280 03	Def. S.	60° 45.2	44	N.E. $\frac{1}{2}$ E.	1.633			
			Def. N.	57° 03.0	45	N.E. $\frac{1}{2}$ E.	1.631			
30.	-58 29	282 04	Def. S.	60° 30.3	40	N.E. by E. $\frac{1}{2}$ E.	1.643	+0.016	1.651	A heavy swell from the southward.
			Def. N.	57° 08.2	40	N.E. by E. $\frac{1}{2}$ E.	1.627			
31.	-58 29	286 04	Def. N.	58° 34.2	45	N.E. by N.	1.570			
Apr. 1.	-57 22	289 50	Def. S.	63° 22.7	47	N.E. by N.	1.539	+0.025	1.554	
			Def. N.	60° 00.8	47	N.E. by N.	1.519			
2.	-57 10	292 11	Def. S.	63° 27.2	44	S.E.	1.535			
			Def. N.	59° 57.5	44	S.E.	1.520	-0.017	1.510	
3.	-56 40	294 46	Def. S.	65° 38.2	46	N.E.	1.465			
			Def. N.	61° 36.2	45	N.E.	1.469			
4.	-54 50	298 10	Def. N.	64° 10.7	44	N.E.	1.395	+0.023	1.466	1.466
5.	-52 54	300 57	Def. S.	70° 13.4	48	N.N.E.	1.342			
			Def. N.	66° 55.7	45	N.N.E.	1.327			
			wt. 3 grs.	27° 57.7	43	N.N.E.	1.300	+0.025	1.355	1.355
			wt. 4 grs.	37° 33.2	44	N.N.E.	1.340			
			wt. 5 grs.	49° 40.7	44	N.N.E.	1.343			
11.	Port Louis, Falkland Islands.		Def. S.	70° 51.3	47		1.328			
			Def. N.	67° 08.1	47		1.322			
	-51 32	301 53	wt. 2 grs.	18° 31.1	45		1.291			
			wt. 3 grs.	27° 42.7	45		1.311			
			wt. 4 grs.	37° 58.5	43		1.331			
			wt. 5 grs.	48° 55.9	43		1.361			
			wt. 6 grs.	66° 49.8*	43	Observed on shore.	1.345		1.322	The results with the "face west" are included in the mean.
Aug. 19.			wt. 2 grs.	17° 57.1	37		1.330			
			wt. 3 grs.	27° 43.3	37		1.310			
			wt. 4 grs.	37° 40.4	37		1.339			
			wt. 5 grs.	49° 31.4	38		1.347			
			wt. 6 grs.	67° 23.4*	38		1.339			
			Def. S.	71° 32.4	34		1.311			
			Def. N.	67° 12.6	35		1.320			

* Observed on shore ;
face west.

	Temp.	Intensity.
wt. 2 grs.	18° 50.4	42 1.287
wt. 3 grs.	28 30.0	42 1.296
wt. 4 grs.	38 51.0	41 1.315
wt. 5 grs.	51 27.9	41 1.326
wt. 6 grs.	68 40.3	41 1.332
wt. 2 grs.	18 32.9	39 1.306
wt. 3 grs.	28 26.6	40 1.299
wt. 4 grs.	39 05.3	40 1.309
wt. 5 grs.	51 19.2	40 1.329
wt. 6 grs.	69 35.7	40 1.324

Observations of the INTENSITY of the Magnetic Force made in Her Majesty's Ship
Terror, with Needle F. C. B., between April 16, 1841, and August 15, 1842.

Observers Captain FRANCIS RAWDON CROZIER, and Mr. THOMAS MOORE, Mate, R.N.

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.			
Apr. 17.	Hobarton Magnetic Observatory.		Def. S.	33 20.4	60	Observed on shore.	1.820	1.820	A spare needle marked C. was used as a deflector, and the observations with it are those registered as "Deflector S." and "Deflector N." The deflecting magnets belonging to the apparatus were also employed, N alone and N. and S. conjointly. The observations with these are distinguished as "Mag. N." and "Mag. N.S." The temperatures are taken from the register in the Erebus.			
	-42 52 147 24		Mag. N.S.	39 59.2	60								
			Mag. N.	30 04.0	60								
			Def. S.	21 03.1	60								
19.			wt. 1 gr.*	12 11.9	60								
			wt. 1½ gr.	18 29.4	60								
			wt. 2 grs.	25 13.7	60								
			wt. 2½ grs.	31 43.0	60								
			wt. 3 grs.	39 02.3	60								
			wt. 3½ grs.	46 51.3	60								
20.			Def. N.	36 00.6	60								
			Def. S.	33 25.6	60								
			Mag. N.S.	40 11.6	60								
			Mag. N.	30 24.1	60								
June 22.	At anchor in the river Derwent.	To obtain corrections for the ship's attraction.	Def. N.	35 58.5	48	W.	1.821						
			Def. N.	35 49.1	48	W.S.W.	1.831						
			Def. N.	35 34.5	48	S.W.	1.844						
			Def. N.	35 09.6	48	S.S.W.	1.868						
			Def. N.	35 09.3	48	S.	1.868						
			Def. N.	34 58.0	48	S.S.E.	1.879						
			Def. N.	35 00.0	48	S.E.	1.877						
			Def. N.	34 59.9	48	E.S.E.	1.877						
			Def. N.	35 06.4	48	E.	1.871						
			Def. N.	35 13.9	48	E.N.E.	1.863						
			Def. N.	35 18.4	48	N.E.	1.859						
			Def. N.	35 21.6	48	N.N.E.	1.857						
			Def. N.	35 23.0	48	N.	1.855						
			Def. N.	35 23.7	48	N.N.W.	1.854						
			Def. N.	36 04.1	48	N.W.	1.816						
			Def. N.	35 21.4	48	W.N.W.	1.857						
July 7.	Storm Bay.		Def. N.	34 57.0	48	S.E. ¾ E.	1.880				-012	1.860	Very steady.
			Def. S.	32 40.0	48	S.E. ¾ E.	1.864						
8.	-43 03 148 20		Def. N.	35 23.6	52	W. ½ N.	1.854	+006	1.849	Very steady.			
			Def. S.	33 11.5	52	W. ½ N.	1.832						
9.	-42 24 149 30		Def. N.	36 03.7	56	N.N.W.	1.816	+022	1.822	Very steady.			
			Def. S.	33 57.6	56	N.N.W.	1.785						
10.	-40 51 149 28		Def. N.	36 33.8	56	N. by W.	1.787	+025	1.814	Very steady.			
			Def. S.	33 51.3	56	N. by W.	1.792						
11.	-38 17 150 22		Def. N.	36 46.1	56	N. by E.	1.775	+027	1.785	Very steady.			
			Def. S.	34 43.3	56	N. by E.	1.741						
12.	-37 28 151 30		Def. N.	37 09.4	61	N.E. ½ N.	1.752	+023	1.758	Slight motion. Steering very steady.			
			Def. S.	35 06.4	61	N.E. ½ N.	1.718						
13.	-36 21 151 39		Def. N.	37 15.1	58	N.N.W. ½ W.	1.747	+026	1.738	Heavy cross sea, unsteady.			
			Def. N.	38 06.6	60	N.	1.697						
14.	-34 06 151 19		Def. S.	35 42.8	60	N.	1.681	+031		A slight motion. Steering steady.			
			Def. N.	38 05.9	60	N.	1.697						
19.	Garden Island, Port Jackson.		Def. N.	38 05.9	60	Observed on shore.	1.708						
	-33 51 151 17		Def. S.	35 15.7	60								

* Observed on shore; face west.

wt. 1 gr.	11 42.0	Intensity 1.820
wt. 1½ gr.	17 52.6	
wt. 2 grs.	24 15.6	
wt. 2½ grs.	31 00.7	
wt. 3 grs.	38 42.3	
wt. 3½ grs.	46 06.3	

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.	
July 19.	Garden Island, Port Jackson.		Mag. N.S.	41 45.3	60	Observed on shore.	1.705	}	1.699	Including the results with the "face west."	
			Mag. N.	31 47.2	60		1.696				
			Mag. S.	22 06.6	60						
			wt. 1 gr.*	13 08.8	60		1.691				
			wt. 1½ gr.	20 02.0	60		1.685				
			wt. 2 grs.	27 00.7	60		1.708				
			wt. 2½ grs.	34 25.2	60		1.692				
			wt. 3 grs.	42 06.9	60		1.709				
			wt. 3½ grs.	51 13.5	60		1.703				
			Aug. 5.	Running out of harbour.	Def. N.		37 45.1				63
Def. S.	35 36.2	63			E. by N. ½ N.	1.688					
Def. N.	37 36.2	63			E. by N. ½ N.	1.726					
6.	-34 01	153 17	Def. S.	35 34.5	63	E. by N. ½ N.	1.690	}	+011	1.703	
			Def. N.	38 06.3	63	E. by N.	1.698				
	-33 54	153 54	Def. S.	36 11.3	63	E. by N.	1.654	}	+011	1.703	
			Def. N.	37 32.3	63	E. by N.	1.731				
7.	-33 56	156 38	Def. S.	35 38.8	63	E. by N.	1.685	}	+011	1.679	Steering wildly, much motion.
			Def. N.	38 16.4	61	E. by N.	1.688				
8.	-33 31	160 20	Def. S.	36 19.2	61	E. by N.	1.647	}	+011	1.671	A good deal of mo- tion, steering tolerably.
			Def. N.	38 36.0	63	E. by N.	1.669				
9.	-33 42	163 34	Def. S.	36 13.2	63	E. by N.	1.652	}	+011	1.671	
			Def. N.	38 58.3	61	E.	1.648				
		164 05	Def. S.	36 16.0	61	E.	1.650	}	+007	1.658	Much motion, steer- ing badly.
			Def. N.	38 46.2	61	E.	1.659				
10.	-33 47	166 39	Def. S.	36 18.3	61	E.	1.648	}	+014	1.627	Motion violent, steering wild.
			Def. N.	38 57.3	62	E. by N. ½ N.	1.648				
	-33 42	166 36	Def. S.	37 01.9	62	E. by N. ½ N.	1.604	}	+014	1.627	A long swell, motion quick, steering well.
			Def. N.	39 30.7	62	E.	1.616				
			Def. S.	36 57.2	62	E.	1.609	}	+007	1.627	
			Mag. N.	32 50.1	62	E.	1.609				
11.	-33 34	167 37	Mag. S.	23 37.2	62	E.	1.609	}	+007	1.627	
			Def. N.	40 07.5	66	N.E. by E.	1.579				
			Def. S.	40 07.5	66	N.E. by E.	1.579	}	+020	1.600	Light wind, heavy swell, with quick motion.
			Mag. N.	37 58.5	66	N.E. by E.	1.549				
			Mag. N.	33 03.0	66	N.E. by E.	1.592	}	+020	1.600	
			Mag. S.	23 12.0	66	N.E. by E.	1.590				
			Mag. N.S.	43 13.0	66	N.E. by E.	1.590	}	+007	1.607	
			Def. N.	39 46.4	66	E.	1.600				
12.	-32 58	169 20	Def. N.	40 10.5	56	E.N.E.	1.576	}	+018	1.607	Wind fresh, motion quick, steering badly.
			Def. S.	37 19.5	56	E.N.E.	1.586				
			Mag. N.	32 56.3	56	E.N.E.	1.601	}	+018	1.607	A head sea, steer- ing steadily.
			Mag. S.	24 07.8	56	E.N.E.	1.601				
			Mag. N.S.	43 17.9	56	N.E.	1.585	}	+026	1.607	
			Def. N.	39 31.5	55	S.E. by E.	1.615				
13.	-32 12	170 27	Def. S.	37 17.6	55	S.E. by E.	1.588	}	-012	1.589	Strong wind, heavy sea, motion quick, ship steering well.
			Def. N.	38 55.5	55	S.E. by E.	1.650				
14.	-32 11	171 20	Def. S.	36 58.7	55	S.E. by E.	1.607	}	-012	1.589	
			Mag. N.	33 30.8	55	S.E. by E.	1.554				
			Mag. N.S.	43 09.9	55	S.E. by E.	1.595	}	-012	1.589	
			Mag. S.	23 34.3	55	S.E. by E.	1.595				

* Observed on shore;
face west.

	Intensity.
wt. 1 gr. 12 44.1	1.674
wt. 1½ gr. 19 03.3	1.712
wt. 2 grs. 26 01.2	1.705
wt. 2½ grs. 33 17.7	1.709
wt. 3 grs. 41 35.2	1.715
wt. 3½ grs. 51 02.1	1.687

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Aug. 15.	—33 55	171 59	Def. N.	39 35.3	60	E. by S.	1.611	.000	1.601	A head sea, table very unsteady.
			Def. N.	39 46.2	60	E. ½ N.	1.600	+ .010		
	—33 58	172 06	Def. N.	39 09.4	60	E.S.E.	1.637	— .006		
			Def. S.	37 06.3	60	E.S.E.	1.600			
			Mag. N.	33 20.9	60	E.S.E.	1.566			
			Mag. N.S.	43 00.2	60	E.S.E.	1.609			
			Mag. S.	23 21.3	60	E.S.E.				
16.	—34 15	172 50	Def. N.	39 43.1	61	N.W. by N.	1.603	+ .029	1.597	A head sea, wind strong, steering well.
			Def. S.	37 44.5	61	N.W. by N.	1.562			
			Mag. N.	33 10.3	61	N.W. by N.	1.583			
			Mag. N.S.	43 25.9	61	N.W. by N.	1.573			
			Mag. S.	23 38.1	61	N.W. by N.		— .004		
			Mag. N.S.	43 40.5	61	E. by S. ½ S.	1.554			
17.	—34 24	173 43	Def. N.	38 52.7	62	E. by S. ½ S.	1.653	— .004	1.619	Strong wind, good deal of motion,
			Def. S.	36 57.2	62	E. by S. ½ S.	1.609			
			Mag. N.	32 46.0	62	E. by S. ½ S.	1.616			
			Mag. N.S.	42 50.3	62	E. by S. ½ S.	1.622			
			Mag. S.	23 06.2	62	E. by S. ½ S.		— .018		A heavy sea, steering wild,
			Def. N.	38 54.8	64	S.W.	1.631			
18.	?	?	Def. N.	39 40.9	59		1.606	1.608	At the Magnetic Observatory, (The results with "face west" are included in the mean.)	
21.	Bay of Islands,		Def. S.	36 59.8	59		1.606			
	New Zealand.		Mag. N.	32 50.2	59		1.610			
			Mag. N.S.	43 01.9	59		1.606			
			Mag. S.	23 37.6	59					
			wt. 1 gr.*	14 03.2	59		1.584			
			wt. 1½ gr.	21 17.9	59		1.601			
			wt. 2 grs.	28 22.1	59		1.633			
			wt. 2½ grs.	36 50.7	59		1.596			
			wt. 3 grs.	44 58.3	59		1.622			
Oct. 29.			wt. 3½ grs.	55 09.9	59	Observed on shore.	1.618	1.608	
			Def. N.	39 32.8	64		1.613			
			Def. S.	36 57.6	64		1.608			
			Mag. N.	32 51.5	64		1.608			
			Mag. N.S.	42 54.9	64		1.616			
			Mag. S.	23 37.6	64					
			wt. 1 gr.†	13 51.7	64		1.606			
			wt. 1½ gr.	20 53.0	64		1.620			
			wt. 2 grs.	28 22.4	64		1.633			
			wt. 2½ grs.	37 05.6	64		1.587			
			wt. 3 grs.	45 02.2	64		1.621			
			wt. 3½ grs.	55 19.1	64		1.616			
Nov. 23.	Running out of	Bay of Islands, off Arch Point.	Def. N.	39 41.1		E. by S.	1.605	+ .004	1.610	Ship steady, about one mile off shore,
			Def. S.	36 59.1		E. by S.	1.607			
24.	—36 20	177 27	Def. N.	39 11.0		E.S.E.	1.635	+ .001	1.616	Ship not very steady, a sea from S.W.
			Def. S.	36 24.1		E.S.E.	1.642			
			Mag. N.	33 07.5		E.S.E.	1.586			
			Mag. N.S.	43 07.0		E.S.E.	1.599			
			Mag. S.	23 09.3		E.S.E.				

* Observed on shore;
face west.

		Intensity.
wt. 1 gr.	13 24.3	1.592
wt. $1\frac{1}{2}$ gr.	20 30.5	1.595
wt. 2 grs.	27 46.9	1.605
wt. $2\frac{1}{2}$ grs.	35 43.0	1.607
wt. 3 grs.	44 38.7	1.619
wt. $3\frac{1}{2}$ grs.	55 23.7	1.594

† Observed on shore;
face west.

		Intensity.
wt. 1 gr.	13 26.8	1.588
wt. $1\frac{1}{2}$ gr.	20 16.4	1.616
wt. 2 grs.	27 38.8	1.613
wt. $2\frac{1}{2}$ grs.	35 45.1	1.606
wt. 3 grs.	44 47.7	1.616
wt. $3\frac{1}{2}$ grs.	55 26.4	1.594

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.	
Nov. 25.	-38 00	179 34	Def. N.	39 01.2	°	S.E. by S.	1.645	-018	1.634	A head sea, table not very steady.	
			Def. S.	36 28.2		S.E. by S.	1.638				
			Mag. N.	32 25.3		S.E. by S.	1.645				
			Mag. N.S.	42 31.1		S.E. by S.	1.647				
			Mag. S.	23 06.8		S.E. by S.	1.647				
	-38 27	179 59	Def. N.	38 52.4		S.E. by E. $\frac{1}{2}$ E.	1.654	-002		A sea from the S.W., ship unsteady.	
			Def. S.	36 29.4		S.E. by E. $\frac{1}{2}$ E.	1.637				
			Mag. N.	32 22.4		S.E. by E. $\frac{1}{2}$ E.	1.643				
			Mag. N.S.	42 30.0		S.E. by E. $\frac{1}{2}$ E.	1.648				
			Mag. S.	22 37.9		S.E. by E. $\frac{1}{2}$ E.	1.648				
	26.	-38 48	182 05	Def. N.		39 12.6	E.S.E.	1.633	+001	1.640	Ship very steady, steering well.
				Def. S.		36 36.7	E.S.E.	1.629			
Def. N.				39 06.7	S.E.	1.639					
Def. S.				36 32.6	S.E.	1.633					
Mag. N.				32 23.2	S.E.	1.648					
-39 02		182 05	Mag. N.S.	42 20.3	S.E.	1.662	-013	Head sea, much motion.			
			Mag. S.	22 23.4	S.E.	1.662					
			Def. N.	38 54.4	E.S.E.	1.653			+001		
			Def. S.	36 15.2	E.S.E.	1.650					
			Mag. N.	32 30.5	E.S.E.	1.638					
27.		-39 14	182 54	Mag. N.S.	42 19.3	E.S.E.	1.663	-006		A swell from the S.E., ship steady.	
				Mag. S.	22 25.8	E.S.E.	1.663				
	Def. N.			38 52.7	S.E. by E.	1.653					
	Def. S.			36 27.2	S.E. by E.	1.639					
	Mag. N.			32 35.6	S.E. by E.	1.631					
	-39 31	183 00	Mag. N.S.	42 34.9	S.E. by E.	1.641	-024	Steering well, ship steady.			
			Mag. S.	22 45.9	S.E. by E.	1.641					
			Def. N.	38 39.5	S. by E.	1.666					
			Def. S.	35 59.9	S. by E.	1.665					
			Mag. N.	32 11.1	S. by E.	1.663					
	28.	-40 35	183 00	Mag. N.S.	42 13.5	S. by E.	1.666	-019	1.652	Very steady.	
				Mag. S.	22 43.5	S. by E.	1.666				
Def. N.				38 32.3	E.S.E.	1.673					
Def. S.				35 52.8	E.S.E.	1.672					
Mag. N.				32 12.2	E.S.E.	1.662					
-40 50		183 11	Mag. N.S.	41 59.7	E.S.E.	1.686	-019	1.652	Very steady.		
			Mag. S.	22 29.6	E.S.E.	1.686					
			Def. N.	38 27.2	S.S.E. $\frac{1}{2}$ E.	1.678					
			Def. S.	35 35.2	S.S.E. $\frac{1}{2}$ E.	1.689					
			Mag. N.	32 02.5	S.S.E. $\frac{1}{2}$ E.	1.675					
29.		-41 34	183 40	Mag. N.S.	41 46.1	S.S.E. $\frac{1}{2}$ E.	1.706	-023	1.666	Very steady.	
				Mag. S.	22 29.8	S.S.E. $\frac{1}{2}$ E.	1.706				
	Def. N.			38 16.1	S. by E.	1.689					
	Def. S.			35 28.7	S. by E.	1.695					
	Mag. N.			31 55.0	S. by E.	1.686					
	-42 40	183 46	Mag. N.S.	41 32.6	S. by E.	1.720	-025	1.682	Very steady.		
			Mag. S.	22 14.3	S. by E.	1.720					
			wt. 1 gr.	13 24.0	S. by E.	1.660					
			wt. $1\frac{1}{2}$ gr.	20 07.1	S. by E.	1.678					
			wt. 2 grs.	26 39.6	S. by E.	1.729					
				wt. $2\frac{1}{2}$ grs.	35 07.5	S. by E.	1.663	-025	1.682	Very steady.	
				wt. 3 grs.	42 38.1	S. by E.	1.692				
wt. $3\frac{1}{2}$ grs.				52 14.9	S. by E.	1.680					
Def. N.				38 04.4	S.	1.700					
Def. S.				35 21.7	S.	1.702					
Mag. N.				31 38.8	S.	1.708					
Mag. N.S.				41 34.5	S.	1.717					
Mag. S.				22 01.6	S.	1.717					

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.		
Nov. 30.	—43 33	183 10	Def. N.	37 47.0	59	S. $\frac{1}{2}$ W.	1.717	—0.024	1.707	Very steady.		
			Def. S.	35 15.2	59	S. $\frac{1}{2}$ W.	1.709					
			Mag. N.	31 33.3	59	S. $\frac{1}{2}$ W.	1.716					
			Mag. N.S.	41 28.2	59	S. $\frac{1}{2}$ W.	1.727					
			Mag. S.	21 58.1	59	S. $\frac{1}{2}$ W.						
	—44 15	183 02	Def. N.	37 29.0	59	S. by W.	1.734	—0.023			A cross swell, motion slight.	
			Def. S.	34 31.6	59	S. by W.	1.752					
			Mag. N.	31 18.9	59	S. by W.	1.737					
			Mag. N.S.	41 10.5	59	S. by W.	1.747					
			Mag. S.	21 59.4	59	S. by W.						
Dec. 1.	—45 30	183 12	Def. N.	37 08.5	63	S.E. by E.	1.753	—0.007	1.733	Ship pitching considerably, steering very steadily.		
			Def. S.	34 49.3	63	S.E. by E.	1.735					
			Mag. N.	31 29.9	63	S.E. by E.	1.721					
			Mag. N.S.	41 29.2	63	S.E. by E.	1.725					
			Mag. S.	21 42.2	63	S.E. by E.						
	—45 48	183 25	Def. N.	37 11.4	63	S.E. $\frac{1}{2}$ E.	1.750	—0.010			A head sea, table unsteady, ship steering well.	
			Def. S.	34 52.1	63	S.E. $\frac{1}{2}$ E.	1.732					
			Mag. N.	31 06.0	63	S.E. $\frac{1}{2}$ E.	1.753					
			Mag. N.S.	40 59.4	63	S.E. $\frac{1}{2}$ E.	1.762					
			Mag. S.	21 43.6	63	S.E. $\frac{1}{2}$ E.						
2. —47 13	184 30	Def. N.	37 11.8	56	S.E. by E. $\frac{1}{2}$ E.	1.750	—0.002	1.753	Head sea, ship pitching, steering steadily.			
		Def. S.	34 31.8	56	S.E. by E. $\frac{1}{2}$ E.	1.752						
		Mag. N.	31 15.8	56	S.E. by E. $\frac{1}{2}$ E.	1.741						
		Mag. N.S.	41 12.7	56	S.E. by E. $\frac{1}{2}$ E.	1.744						
		Mag. S.	21 07.2	56	S.E. by E. $\frac{1}{2}$ E.							
—47 39	184 55	Def. N.	36 53.8	56	S.E. by E.	1.767	—0.007					
		Def. S.	34 24.0	56	S.E. by E.	1.760						
		Mag. N.	30 55.2	56	S.E. by E.	1.768						
		Mag. N.S.	40 53.0	56	S.E. by E.	1.772						
		Mag. S.	21 09.8	56	S.E. by E.							
3. —48 18	185 54	Def. N.	36 55.9	51	S.E. by E.	1.765	—0.007	1.772	Very steady.			
		Def. S.	34 06.7	51	S.E. by E.	1.776						
		Mag. N.	30 44.1	51	S.E. by E.	1.782						
		Mag. N.S.	40 52.8	51	S.E. by E.	1.772						
		Mag. S.	21 15.0	51	S.E. by E.							
		wt. 1 gr.	12 01.0	51	S.E. by E.	1.844						
		wt. $1\frac{1}{2}$ gr.	18 51.1	51	S.E. by E.	1.784						
		wt. 2 grs.	25 50.7	51	S.E. by E.	1.777						
		wt. $2\frac{1}{2}$ grs.	32 51.6	51	S.E. by E.	1.760						
		wt. 3 grs.	40 23.1	51	S.E. by E.	1.766						
—49 05	186 54	wt. $3\frac{1}{2}$ grs.	48 41.0	51	S.E. by E.	1.765	—0.005	1.772	Very steady.			
		Def. N.	36 51.6	51	S.E. by E. $\frac{1}{2}$ E.	1.769						
		Def. S.	34 06.3	51	S.E. by E. $\frac{1}{2}$ E.	1.777						
		Mag. N.	30 46.1	51	S.E. by E. $\frac{1}{2}$ E.	1.780						
		Mag. N.S.	40 45.8	51	S.E. by E. $\frac{1}{2}$ E.	1.781						
		Mag. S.	21 11.2	51	S.E. by E. $\frac{1}{2}$ E.							
		wt. 1 gr.	12 23.7	51	S.E. by E. $\frac{1}{2}$ E.	1.790						
		wt. $1\frac{1}{2}$ gr.	18 37.4	51	S.E. by E. $\frac{1}{2}$ E.	1.804						
		wt. 2 grs.	25 50.1	51	S.E. by E. $\frac{1}{2}$ E.	1.778						
		wt. $2\frac{1}{2}$ grs.	32 30.9	51	S.E. by E. $\frac{1}{2}$ E.	1.777						
4. —49 24	187 23	wt. 3 grs.	40 32.8	51	S.E. by E. $\frac{1}{2}$ E.	1.760	+0.004	1.772	Swell from the northward, steady.			
		wt. $3\frac{1}{2}$ grs.	48 59.5	51	S.E. by E. $\frac{1}{2}$ E.	1.757						
		Def. N.	36 41.8	54	E.	1.779						
		Def. N.	36 44.7	54	E. by S.	1.776						
		Def. S.	34 22.0	54	E. by S.	1.762						
		Mag. N.	30 48.7	54	E. by S.	1.776						
		Mag. N.S.	40 56.3	54	E. by S.	1.768						
										—0.000		

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 4.	—49 24	187 23	Mag. S.	21 25.6	54	E. by S.		.000	1.772	Swell from the northward. Steady.
			wt. 1 gr.	12 24.3	54	E. by S.	1.789			
			wt. 1½ gr.	18 55.0	54	E. by S.	1.778			
			wt. 2 grs.	25 46.4	54	E. by S.	1.782			
			wt. 2½ grs.	32 36.7	54	E. by S.	1.774			
			wt. 3 grs.	40 48.6	54	E. by S.	1.753			
			wt. 3½ grs.	48 56.7	54	E. by S.	1.759			
5.	—49 23	188 54	Def. N.	36 18.3	55	E. by S.	1.803			
			Def. S.	34 29.5	55	E. by S.	1.754			
			Mag. N.	30 46.1	55	E. by S.	1.780			
			Mag. N.S.	40 54.9	55	E. by S.	1.770			Very steady.
			Mag. S.	21 34.1	55	E. by S.				
			wt. 1 gr.	12 35.7	55	E. by S.	1.762			
			wt. 1½ gr.	18 20.9	55	E. by S.	1.831			
			wt. 2 grs.	25 35.5	55	E. by S.	1.794			
			wt. 2½ grs.	32 51.2	55	E. by S.	1.762	.000	1.775	
			wt. 3 grs.	40 31.3	55	E. by S.	1.762			
			wt. 3½ grs.	48 46.6	55	E. by S.	1.764			
	—49 38	189 44	Def. N.	36 34.4	55	E. by S.	1.787			
			Def. S.	34 28.8	55	E. by S.	1.755			Very steady.
			Mag. N.	30 54.8	55	E. by S.	1.766			
			Mag. N.S.	41 01.8	55	E. by S.	1.759			
			Mag. S.	21 46.8	55	E. by S.				
6.	—49 50	190 46	Def. N.	36 37.1	51	E. by S.	1.784			
			Def. S.	34 02.5	51	E. by S.	1.781			
			Mag. N.	30 49.4	51	E. by S.	1.775			
			Mag. N.S.	41 04.2	51	E. by S.	1.756			
			Mag. S.	21 41.3	51	E. by S.				
			wt. 1 gr.	12 38.8	51	E. by S.	1.753	.000	1.766	
			wt. 1½ gr.	18 49.6	51	E. by S.	1.785			
			wt. 2 grs.	25 40.4	51	E. by S.	1.788			
			wt. 2½ grs.	33 28.2	51	E. by S.	1.725			Ship steady.
			wt. 3 grs.	40 37.3	51	E. by S.	1.758			
			wt. 3½ grs.	49 09.5	51	E. by S.	1.753			
	—50 08	191 39	Def. N.	36 40.0	51	E. by S.	1.781			
			Def. S.	34 16.4	51	E. by S.	1.768			
			Mag. N.	30 51.3	51	E. by S.	1.774			
			Mag. N.S.	41 02.2	51	E. by S.	1.759	.000	1.771	
			Mag. S.	21 42.4	51	E. by S.				
			wt. 1 gr.	12 35.7	51	E. by S.	1.761			
			wt. 1½ gr.	18 50.0	51	E. by S.	1.785			
7.	—50 32	191 52	Def. N.	35 51.7	51	S.E. by E.	1.828			Ship steady.
			Def. S.	33 46.7	51	S.E. by E.	1.796			
			Mag. N.	30 48.4	51	S.E. by E.	1.778	—007		
			Mag. N.S.	40 47.4	51	S.E. by E.	1.780			
			Mag. S.	21 27.7	51	S.E. by E.				
	—50 45	192 19	Def. N.	36 01.8	51	S.E. ½ E.	1.818			
			Def. S.	34 06.7	51	S.E. ½ E.	1.776			
			Mag. N.	30 40.7	51	S.E. ½ E.	1.785			
			Mag. N.S.	40 45.7	51	S.E. ½ E.	1.782		1.777	
			Mag. S.	21 32.3	51	S.E. ½ E.				
			wt. 1 gr.	12 43.0	51	S.E. ½ E.	1.743	—008		
			wt. 1½ gr.	18 56.2	51	S.E. ½ E.	1.776			
			wt. 2 grs.	25 58.6	51	S.E. ½ E.	1.769			
			wt. 2½ grs.	32 37.7	51	S.E. ½ E.	1.772			
			wt. 3 grs.	40 35.6	51	S.E. ½ E.	1.759			
			wt. 3½ grs.	48 00.8	51	S.E. ½ E.	1.784			

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.					
Dec. 8.	-51 37	194 00	Def. N.	35 49.9	49	E. by s.	1.830	-000	1.794	Ship steady.					
			Def. S.	33 50.1	49	E. by s.	1.793								
			Mag. N.	30 42.2	49	E. by s.	1.784								
			Mag. N.S.	40 31.4	49	E. by s.	1.796								
			Mag. S.	21 29.1	49	E. by s.									
			wt. 1 gr.	12 35.5	49	E. by s.	1.760								
			wt. 1½ gr.	18 34.6	49	E. by s.	1.806								
			wt. 2 grs.	25 16.9	49	E. by s.	1.813								
			wt. 2½ grs.	32 08.9	49	E. by s.	1.794								
			wt. 3 grs.	40 00.3	49	E. by s.	1.780								
			wt. 3½ grs.	48 01.8	49	E. by s.	1.782								
			-52 00	195 00	Def. N.	36 01.2	49				E. by s.	1.819	-000	1.799	Strong breeze, table steady, steering wildly.
	Def. S.	33 59.6			49	E. by s.	1.783								
	Mag. N.	30 36.5			49	E. by s.	1.792								
	Mag. N.S.	40 38.6			49	E. by s.	1.786								
	Mag. S.	20 59.5			49	E. by s.									
	Def. N.	35 53.6			45	E. by s.	1.826								
	Def. S.	33 44.6			45	E. by s.	1.798								
	Mag. N.	30 21.9			45	E. by s.	1.812								
	Mag. N.S.	40 47.0			45	E. by s.	1.781								
	Mag. S.	20 38.5			45	E. by s.									
	9. -52 14	197 49			Mag. N.S.	40 36.2	45	E. by s.	1.791	-000	1.799	Ship unsteady, steering wild.			
					Def. N.	36 14.8	46	E. ½ N.	1.805						
			Def. S.	33 54.6	46	E. ½ N.	1.788								
			Mag. N.	30 26.7	46	E. ½ N.	1.806								
			Mag. N.S.	40 30.9	46	E. ½ N.	1.798								
			Mag. S.	21 26.5	46	E. ½ N.									
			wt. 1 gr.	11 50.3	46	E. ½ N.	1.871								
			wt. 1½ gr.	17 43.9	46	E. ½ N.	1.891								
			wt. 2 grs.	24 29.7	46	E. ½ N.	1.867								
			wt. 2½ grs.	31 19.3	46	E. ½ N.	1.837								
			wt. 3 grs.	39 46.3	46	E. ½ N.	1.788								
			wt. 3½ grs.	47 43.1	46	E. ½ N.	1.791								
10. -53 01	202 16	Def. N.	36 41.3	45	E.S.E.	1.780	+008	1.820	Violent motion, steering well, head sea, table pretty steady.						
		Def. S.	33 40.8	45	E.S.E.	1.802									
		Mag. N.	30 30.2	45	E.S.E.	1.801									
		Mag. N.S.	40 20.2	45	E.S.E.	1.813									
		Mag. S.	21 23.0	45	E.S.E.										
		wt. 1 gr.	12 30.8	45	E.S.E.	1.771									
		wt. 1½ gr.	18 07.9	45	E.S.E.	1.851									
		wt. 2 grs.	24 38.0	45	E.S.E.	1.857									
		wt. 2½ grs.	31 44.7	45	E.S.E.	1.815									
		wt. 3 grs.	39 30.1	45	E.S.E.	1.798									
		wt. 3½ grs.	48 07.9	45	E.S.E.	1.779									
		11. -52 51	203 56	Def. N.	36 09.5	45				E.S.E.	1.811	-003	1.834	Head swell, little motion, steering well.	
Def. S.	33 22.8			45	E.S.E.	1.820									
Mag. N.	30 11.3			45	E.S.E.	1.828									
Mag. N.S.	39 57.5			45	E.S.E.	1.841									
Mag. S.	21 07.1			45	E.S.E.										
wt. 1 gr.	12 08.9			45	E.S.E.	1.823									
wt. 1½ gr.	18 00.7			45	E.S.E.	1.863									
wt. 2 grs.	24 39.1			45	E.S.E.	1.856									
wt. 2½ grs.	31 15.2			45	E.S.E.	1.840									
wt. 3 grs.	38 03.7			45	E.S.E.	1.855									
wt. 3½ grs.	47 41.3			45	E.S.E.	1.834									
12. -52 53	205 07														
		-53 31	206 14												

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.	
Dec. 13.	-54 19	208 24	Def. N.	36 02.0	51	E.S.E.	1.818	-003	1.814	Table steady, steering badly.	
			Def. S.	33 17.8	51	E.S.E.	1.825				
			Mag. N.	30 23.2	51	E.S.E.	1.811				
			Mag. N.S.	40 28.8	51	E.S.E.	1.801				
			Mag. S.	20 27.6	51	E.S.E.					
			Def. N.	36 03.0	51	E.S.E.	1.817				
	-54 53	209 24	Def. S.	33 14.6	51	E.S.E.	1.828	-003	1.814	Table steady, steering badly.	
			Mag. N.	30 10.5	51	E.S.E.	1.829				
			Mag. N.S.	39 59.5	51	E.S.E.	1.837				
			Mag. S.	20 52.6	51	E.S.E.					
			Def. N.	36 18.6	51	E.S.E.	1.802				
			Def. N.	36 11.8	48	S.E. by s.	1.808				
	-54 48	209 25	Def. S.	32 54.1	48	S.E. by s.	1.849	-015	1.836	Heavy sea, steering badly.	
			Mag. N.	30 18.1	48	S.E. by s.	1.818				
			Mag. N.S.	40 03.9	48	S.E. by s.	1.831				
			Mag. S.	20 54.4	48	S.E. by s.					
			Def. N.	35 54.6	52	S.E. by s.	1.825				
Def. S.			32 37.1	52	S.E. by s.	1.867					
14.	-56 14	211 43	Mag. N.	29 56.6	52	S.E. by s.	1.849	-015	1.836	Ship much more steady, steering better.	
			Mag. N.S.	39 36.9	52	S.E. by s.	1.867				
			Mag. S.	20 21.6	52	S.E. by s.					
			Def. N.	35 55.5	52	S.E. by s.	1.824				
			Def. S.	32 43.8	52	S.E. by s.	1.860				
			Mag. N.	29 59.3	52	S.E. by s.	1.845				
	-56 30	211 50	Mag. N.S.	39 31.8	52	S.E. by s.	1.874	-015	1.841	Table steady, steering well.	
			Mag. S.	20 24.4	52	S.E. by s.					
			Def. N.	35 36.6	52	S.E. by s.	1.841				
			Def. S.	32 43.4	52	S.E. by s.	1.861				
			Mag. N.	29 59.9	52	S.E. by s.	1.844				
			Mag. N.S.	40 01.6	52	S.E. by s.	1.834				
	15.	-56 53	212 06	Mag. S.	20 33.4	52	S.E. by s.		-015	1.843	Very steady.
				wt. 1 gr.	11 46.1	52	S.E. by s.	1.884			
				wt. 1½ gr.	18 10.6	52	S.E. by s.	1.848			
				wt. 2 grs.	24 02.0	52	S.E. by s.	1.902			
wt. 2½ grs.				31 08.6	52	S.E. by s.	1.848				
wt. 3 grs.				38 07.8	52	S.E. by s.	1.855				
-57 16		212 17	wt. 3½ grs.	46 00.9	52	S.E. by s.	1.846	-015	1.843	Very steady.	
			Def. N.	35 33.1	41	S.E. by s.	1.845				
			Def. S.	32 47.5	41	S.E. by s.	1.855				
			Mag. N.	29 57.1	41	S.E. by s.	1.848				
16.	-57 44	212 59	Mag. N.S.	40 06.1	41	S.E. by s.	1.828	-019	1.863	Very steady.	
			Mag. S.	20 33.2	41	S.E. by s.					
			Def. N.	35 28.4	41	S.E. by s.	1.850				
			Def. S.	32 21.9	41	S.E. by s.	1.882				
			Mag. N.	29 25.4	41	S.E. by s.	1.895				
			Mag. N.S.	39 39.1	41	S.E. by s.	1.865				
	-57 44	212 59	Mag. S.	20 14.7	41	S.E. by s.		-019	1.863	Very steady.	
			Def. N.	35 13.8	42	S.S.E.	1.863				
			Def. S.	32 22.3	42	S.S.E.	1.882				
			Mag. N.	29 51.2	42	S.S.E.	1.857				
			Mag. N.S.	39 30.9	42	S.S.E.	1.876				
			Mag. S.	20 15.2	42	S.S.E.					
-57 44	212 59	wt. 1 gr.	11 45.4	42	S.S.E.	1.882	-019	1.863	Very steady.		
		wt. 1½ gr.	18 00.2	42	S.S.E.	1.860					
		wt. 2 grs.	23 38.6	42	S.S.E.	1.929					
		wt. 2½ grs.	30 04.6	42	S.S.E.	1.904					

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.		
Dec. 16.	-58 28	213 08	Def. N.	34 42.2	42	S.S.E.	1.895	-017	1.878	Very steady.		
			Def. S.	32 09.3	42	S.S.E.	1.896					
			Mag. N.	29 32.0	42	S.S.E.	1.885					
			Mag. N.S.	39 29.4	42	S.S.E.	1.878					
			Mag. S.	20 16.5	42	S.S.E.						
			wt. 1 gr.	11 33.4	42	S.S.E.	1.915					
			wt. 1 1/2 gr.	17 36.2	42	S.S.E.	1.904					
			wt. 2 grs.	23 48.0	42	S.S.E.	1.917					
	-58 44	213 11	wt. 2 1/2 grs.	29 50.1	42	S.S.E.	1.918					
			wt. 3 grs.	36 40.9	42	S.S.E.	1.914					
			wt. 3 1/2 grs.	44 52.1	42	S.S.E.	1.877					
			Def. N.	35 11.8	42	S.S.E.	1.865					
			Def. S.	32 22.7	42	S.S.E.	1.882					
			Mag. N.	29 28.0	42	S.S.E.	1.891					
			Mag. N.S.	39 16.0	42	S.S.E.	1.896					
			Mag. S.	19 46.3	42	S.S.E.						
17.	-60 48	213 51	Def. N.	34 58.7	36	S.S.E.	1.878	-016	1.892	Very slight motion, steering well.		
			Def. S.	31 59.8	36	S.S.E.	1.905					
			Mag. N.	29 19.8	36	S.S.E.	1.903					
			Mag. N.S.	39 06.6	36	S.S.E.	1.907					
			Mag. S.	19 45.9	36	S.S.E.						
			wt. 1 gr.	11 51.7	36	S.S.E.	1.863					
			wt. 1 1/2 gr.	16 49.6	36	S.S.E.	1.987					
			wt. 2 grs.	23 56.7	36	S.S.E.	1.907					
	-61 37	213 54	wt. 2 1/2 grs.	29 43.5	36	S.S.E.	1.923		-016		1.916	Very steady, sailing amongst loose ice.
			wt. 3 grs.	36 48.8	36	S.S.E.	1.906					
			wt. 3 1/2 grs.	44 22.1	36	S.S.E.	1.893					
			Def. N.	34 28.6	34	S. 1/2 E.	1.908					
			Def. S.	31 43.6	34	S. 1/2 E.	1.922					
			Mag. N.	29 09.5	34	S. 1/2 E.	1.918					
			Mag. N.S.	39 10.2	34	S. 1/2 E.	1.903					
			Mag. S.	19 54.3	34	S. 1/2 E.						
18.	-62 34	212 34	Def. N.	34 27.6	32	S. by E.	1.909	-016	1.910	Very steady, running amongst loose ice.		
			Def. S.	31 38.4	32	S. by E.	1.928					
			Mag. N.	29 06.9	32	S. by E.	1.922					
			Mag. N.S.	38 39.3	32	S. by E.	1.945					
			Mag. S.	19 21.5	32	S. by E.						
			wt. 1 gr.	11 30.6	32	S. by E.	1.920					
			wt. 1 1/2 gr.	16 59.2	32	S. by E.	1.968					
			wt. 2 grs.	23 55.7	32	S. by E.	1.905					
	-63 06	210 55	wt. 2 1/2 grs.	29 07.6	32	S. by E.	1.958		-015		1.927	Very steady, running amongst loose ice.
			wt. 3 grs.	36 00.5	32	S. by E.	1.942					
			wt. 3 1/2 grs.	43 45.9	32	S. by E.	1.920					
			Def. N.	34 27.4	40	S.S.W.	1.910					
			Def. S.	31 50.7	40	S.S.W.	1.914					
			Mag. N.	29 08.0	40	S.S.W.	1.920					
			Mag. N.S.	38 52.6	40	S.S.W.	1.927					
			Mag. S.	19 37.4	40	S.S.W.						
20.	-63 36	208 20	Def. N.	34 20.3	34	S.S.W.	1.917	-014	1.927	Very steady, running amongst loose ice.		
			Def. S.	31 19.9	34	S.S.W.	1.946					
			Mag. N.	28 59.8	34	S.S.W.	1.932					
			Mag. N.S.	38 48.0	34	S.S.W.	1.933					
			Mag. S.	19 37.0	34	S.S.W.						
			Def. N.	34 21.3	34	S.	1.916					
			Def. S.	31 23.0	34	S.	1.943					
			Mag. N.	28 47.5	34	S.	1.950					
	-63 53	208 32	Mag. N.S.	38 39.1	34	S.	1.945		-014		1.927	Very steady, running amongst loose ice.
			Mag. S.	19 21.6	34	S.						

Observations of the Magnetic Force. (Continued.)

1841.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Dec. 21.	-64 11	206 35	Def. N.	34 01.3	34	s.s.w.	1.936	-013	1.927	Very steady, running amongst loose ice.
			Def. S.	31 15.8	34	s.s.w.	1.950			
			Mag. N.	28 54.2	34	s.s.w.	1.941			
			Mag. N.S.	38 44.7	34	s.s.w.	1.937			
			Mag. S.	19 15.2	34	s.s.w.	1.937			
	-64 51	206 19	wt. 1 gr.	11 10.3	35	s. $\frac{3}{4}$ w.	1.978	-013	1.943	Very steady, steering amongst loose ice.
			wt. 1 $\frac{1}{2}$ gr.	17 10.4	35	s. $\frac{3}{4}$ w.	1.948			
			wt. 2 grs.	23 07.5	35	s. $\frac{3}{4}$ w.	1.968			
			wt. 2 $\frac{1}{2}$ grs.	29 07.7	35	s. $\frac{3}{4}$ w.	1.959			
			wt. 3 grs.	35 52.4	35	s. $\frac{3}{4}$ w.	1.949			
			wt. 3 $\frac{1}{2}$ grs.	42 59.5	35	s. $\frac{3}{4}$ w.	1.947			
			Def. N.	34 05.5	35	s. $\frac{3}{4}$ w.	1.932			
			Def. S.	31 01.8	35	s. $\frac{3}{4}$ w.	1.965	-013	1.931	Very steady, steering amongst loose ice.
22.	-65 19	205 08	Def. N.	34 07.6	37	s. $\frac{1}{2}$ w.	1.930			
			Def. S.	31 17.5	37	s. $\frac{1}{2}$ w.	1.948			
			Mag. N.	28 50.9	37	s. $\frac{1}{2}$ w.	1.945			
			Mag. N.S.	38 42.3	37	s. $\frac{1}{2}$ w.	1.940			
	-65 34	205 00	Mag. S.	19 29.9	37	s. $\frac{1}{2}$ w.	1.940	-013	1.931	Very steady, steering amongst loose ice.
			Def. N.	33 59.5	37	s.	1.937			
			Def. S.	31 00.9	37	s.	1.966			
			Mag. N.	28 53.2	37	s.	1.942			
			Mag. N.S.	38 37.7	37	s.	1.946			
			Mag. S.	19 25.2	37	s.	1.946	+009	1.950	Very steady, sailing amongst loose ice.
23.	-65 47	204 19	Def. N.	34 02.2	36	N.E.	1.935			
			Def. S.	31 23.8	36	N.E.	1.942			
			Mag. N.	28 42.6	36	N.E.	1.958			
			Mag. N.S.	38 44.3	36	N.E.	1.938			
			Mag. S.	19 44.9	36	N.E.	1.938	+011	1.950	Fast to a piece of ice.
24.	-65 54	204 08	Def. N.	34 15.9	42	N. by w.	1.921			
			Def. S.	31 21.8	42	N. by w.	1.944			
			Mag. N.	28 51.3	42	N. by w.	1.945			
			Mag. N.S.	38 45.8	42	N. by w.	1.936			
			Mag. S.	19 29.0	42	N. by w.	1.936	-004	1.949	Working in a hole of water.
27.	-66 08	203 50	Def. N.	34 07.9	30	E.S.E.	1.929			
			Def. S.	30 57.8	30	E.S.E.	1.969			
			Mag. N.	28 46.1	30	N.W. by N.	1.953			
			Mag. N.S.	38 45.3	30	N.W. by N.	1.937			
			Mag. S.	19 24.3	30	N.W. by N.	1.937	+010	1.949	Working in a hole of water.
			Def. N.	33 56.0	30	w. by N.	1.941			
28.	-66 10	202 54	Def. N.	33 56.0	30	w. by N.	1.941	+003		
1842.										
Jan. 1.	-66 36	203 29	Def. N.	34 06.6	44	N.W. $\frac{1}{2}$ w.	1.931	+009	1.961	Fast to a piece of ice, Erebus fifty yards N.E. (This result is not employed in the map.)
			Def. S.	31 17.7	44	N.W. $\frac{1}{2}$ w.	1.948			
			Mag. N.	28 46.6	44	N.W. $\frac{1}{2}$ w.	1.951			
			Mag. N.S.	38 35.1	44	N.W. $\frac{1}{2}$ w.	1.950			
			Mag. S.	19 28.8	44	N.W. $\frac{1}{2}$ w.	1.950			
			wt. 1 gr.	11 20.8	44	N.W. $\frac{1}{2}$ w.	1.950			
			wt. 1 $\frac{1}{2}$ gr.	16 59.2	44	N.W. $\frac{1}{2}$ w.	1.967			
			wt. 2 grs.	22 44.6	44	N.W. $\frac{1}{2}$ w.	2.001			
			wt. 2 $\frac{1}{2}$ grs.	29 21.5	44	N.W. $\frac{1}{2}$ w.	1.947			
			wt. 3 grs.	35 50.3	44	N.W. $\frac{1}{2}$ w.	1.952			
			wt. 3 $\frac{1}{2}$ grs.	43 33.7	44	N.W. $\frac{1}{2}$ w.	1.922	+009	1.944	Working in a hole of water.
			Def. N.	34 13.5	33	N.W.	1.924			
			Def. S.	31 20.0	33	N.W.	1.946			
			Mag. N.	29 00.1	33	N.W.	1.932			
			Mag. N.S.	38 40.2	33	N.W.	1.943			
7.	-66 20	203 39	Mag. S.	19 29.8	33	N.W.	1.943			

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.		
Jan. 8.	-66 05	204 02	Def. N.	34 13.8	35	s. by w. $\frac{1}{2}$ w.	1.923	-011	1.944	Working in a hole of water.		
			Def. S.	31 22.2	35	s. by w. $\frac{1}{2}$ w.	1.944					
			Mag. N.	29 05.0	35	s. by w. $\frac{1}{2}$ w.	1.925					
			Mag. N.S.	38 47.0	35	s. by w. $\frac{1}{2}$ w.	1.935					
			Mag. S.	19 29.8	35	s. by w. $\frac{1}{2}$ w.		+012				
			wt. 1 gr.	11 14.4	35	N.	1.965					
			wt. $1\frac{1}{2}$ gr.	17 07.6	35	N.	1.951					
			wt. 2 grs.	23 02.1	35	N.	1.982					
			wt. $2\frac{1}{2}$ grs.	29 01.7	35	N.	1.963					
			wt. 3 grs.	35 44.9	35	N.	1.953					
			wt. $3\frac{1}{2}$ grs.	43 14.8	35	N.	1.930					
	9.	-66 01	204 04	Def. N.	33 45.1	35	s.w. $\frac{1}{2}$ w.	1.952	-007			
				Def. S.	31 12.7	35	s.w.	1.954				
				Mag. N.	28 59.9	35	s.w. by w.	1.932				
				Mag. N.S.	38 37.6	35	s.w. by w.	1.946				
	10.	-65 57	203 56	Mag. S.	19 16.0	35	s.w. by w.		-000			
				Def. N.	33 53.7	30	w. by s.	1.943				
				Def. S.	30 59.0	30	w. by s.	1.968				
				Mag. N.	28 46.5	30	w. by s.	1.952				
				Mag. N.S.	38 36.3	30	E.	1.948	+001			
				Mag. S.	19 16.3	30	E.					
				wt. 1 gr.	11 28.5	30	w. by s. $\frac{1}{2}$ s.	1.923				
				wt. $1\frac{1}{2}$ gr.	16 59.9	30	w. by s. $\frac{1}{2}$ s.	1.965				
				wt. 2 grs.	22 55.0	30	w. by s. $\frac{1}{2}$ s.	1.984	-003	Working in a hole of water.		
				wt. $2\frac{1}{2}$ grs.	29 09.5	30	w. by s. $\frac{1}{2}$ s.	1.955				
				wt. 3 grs.	35 46.6	30	w. by s. $\frac{1}{2}$ s.	1.950				
				wt. $3\frac{1}{2}$ grs.	42 54.2	30	w. by s. $\frac{1}{2}$ s.	1.942				
				Def. N.	33 54.5	30	s.w. by w.	1.942	-006			
				Def. S.	31 22.4	30	s.w. by w.	1.944				
				Mag. N.	28 46.7	30	s.w. by w.	1.952				
				Mag. N.S.	38 30.3	30	s.w. by w.	1.957				
	11.	-65 56	203 31	Mag. S.	19 19.4	30	s.w. by w.		-012			
				Def. N.	33 51.4	30	s.	1.946				
				Def. S.	31 05.2	30	s.	1.962				
				Mag. N.	28 45.2	30	s.	1.953				
	13.	-66 06	202 10	Mag. N.S.	38 40.3	30	s.	1.943	+012			
				Mag. S.	19 21.0	30	s.					
				Def. N.	34 14.7	33	N. $\frac{1}{2}$ E.	1.922				
				Def. S.	31 23.1	33	N. $\frac{1}{2}$ E.	1.943				
	14.	-66 08	201 46	Mag. N.	28 52.6	33	N. $\frac{1}{2}$ E.	1.942	+008			
				Mag. N.S.	38 49.4	33	N. $\frac{1}{2}$ E.	1.931				
				Mag. S.	19 36.1	33	N. $\frac{1}{2}$ E.					
				Def. N.	34 10.3	33	N.E. by E.	1.927				
	16.	-65 47	202 08	Def. S.	31 15.2	35	N.E. by E.	1.951	1.948			
				Mag. N.	28 49.5	35	N.E. by E.	1.947				
				Mag. N.S.	38 38.4	35	N.E. by E.	1.946				
				Mag. S.	19 27.1	35	N.E. by E.					
				Def. N.	33 47.6	50		1.949				
				Def. S.	31 16.1	50		1.951				
				Mag. N.	28 52.7	50		1.942				
				Mag. N.S.	38 45.7	50		1.936				
				Mag. S.	19 44.8	50						
				wt. 1 gr.	11 25.4	50	Observed on ice.	1.940				
				wt. $1\frac{1}{2}$ gr.	17 08.3	50		1.957				
				wt. 2 grs.	23 02.9	50		1.979				
				wt. $2\frac{1}{2}$ grs.	29 16.2	50		1.955				
				wt. 3 grs.	36 17.4	50		1.935				
				wt. $3\frac{1}{2}$ grs.	43 23.5	50		1.932				

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Jan. 26.	-67 12	203 12	Def. N.	33 14.0	35	E. by N.	1.984			
			Def. S.	31 00.0	35	E. by N.	1.967	+003		
			Mag. N.	28 30.9	35	E. by N.	1.977			
			Mag. N.S.	38 28.5	35	E. by N.	1.960			
			Mag. N.S.	38 22.2	35	S.E. by S.	1.966	-009		
			Mag. S.	19 15.7	35	S.E. by S.				
28.	-67 46	204 17	Def. N.	33 47.7	35	E. by N.	1.949	+003		
			Def. S.	31 00.7	35	N.	1.966	+012		
			Def. N.	33 47.5	35	N. by E.	1.949	+011		
			Def. N.	33 43.8	35	N.N.E.	1.954			
			Mag. N.	28 45.1	35	N.N.E.	1.955	+010		
			Mag. N.S.	38 29.8	35	N.N.E.	1.957			
			Mag. S.	19 21.1	35	N.N.E.				
			Def. N.	33 45.2	35	S. $\frac{3}{4}$ W.	1.952			
			Def. S.	30 52.2	35	S. $\frac{3}{4}$ W.	1.975	-012		
			Mag. N.	28 39.0	35	S. $\frac{3}{4}$ W.	1.965			
			Mag. N.S.	38 22.4	35	S. $\frac{3}{4}$ W.	1.968			
			Mag. S.	19 16.9	35	S. $\frac{3}{4}$ W.				
28.	-67 46	204 17	wt. 1 gr.	10 53.5	35	N.	2.028			
			wt. $1\frac{1}{2}$ gr.	16 57.2	35	N.	1.972	+012		
			wt. 2 grs.	23 09.2	35	N. by W. $\frac{3}{4}$ W.	1.966			
			wt. $2\frac{1}{2}$ grs.	29 14.4	35	N. by W. $\frac{3}{4}$ W.	1.951			
			wt. 3 grs.	35 37.6	35	N. by W. $\frac{3}{4}$ W.	1.959	+011		
			wt. $3\frac{1}{2}$ grs.	42 53.4	35	N. by W. $\frac{3}{4}$ W.	1.944			
29.	-67 24	204 05	Def. N.	33 42.1	31	S. by W.	1.956			
			Def. S.	30 58.3	31	S. by W.	1.969	-012		
			Mag. N.	28 49.8	31	S. by W.	1.947			
			Mag. N.S.	38 41.5	31	S. by W.	1.941			
31.	-67 12	202 24	Def. N.	33 51.2	32	S.S.W.	1.946			
			Def. S.	30 50.5	32	S.S.W.	1.976	-011		
			Mag. N.	28 38.1	32	S.S.W.	1.966			
			Mag. N.S.	38 30.3	32	S.S.W.	1.957			
			Mag. S.	19 21.8	32	S.S.W.				
			Def. N.	33 52.1	32	S.W.	1.945	-007		
			Def. N.	33 52.3	32	S.W. by S.	1.945	-008		
Feb. 1.	-67 12	201 34	Def. N.	34 30.6	32	W. by S.	1.906	-001		
			Def. N.	34 04.4	32	E.	1.933	+001		
	-67 16		Def. N.	33 56.0	32	S.S.W.	1.941			
			Def. S.	31 03.0	32	S.S.W.	1.964	-011		
			Mag. N.	28 46.3	32	S.S.W.	1.951			
			Mag. N.S.	38 31.8	32	S.S.W.	1.954			
			Mag. S.	19 21.1	32	S.S.W.				
			Def. N.	34 07.1	32	N. $\frac{3}{4}$ W.	1.930	+011		
			Def. N.	33 51.1	32	S.W.	1.946	-007		
2.	-67 56	199 48	Def. N.	33 33.9	31	S. by W.	1.964			
			Def. S.	31 00.5	31	S. by W.	1.966	-011		
			Mag. N.	28 51.5	31	S. by W.	1.944			
			Mag. N.S.	38 23.3	31	S. by W.	1.967			
			Mag. S.	19 15.5	31	S. by W.				
3.	-68 21	200 06	Def. N.	33 45.4	31	S.S.W.	1.952			
			Def. S.	30 51.4	31	S.S.W.	1.976	-011		
			Mag. N.	28 22.2	31	S.S.W.	1.990			
			Mag. N.S.	38 21.2	31	S.S.W.	1.970			
			Mag. S.	19 13.8	31	S.S.W.				

* This result has not been employed in the map.

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 4.	—68 45	199 41	Def. N.	33 38.7	30	s.	1.959	—011	1.961	Table steady.
			Def. S.	30 43.2	30	s.	1.984			
			Mag. N.	28 32.2	30	s.	1.975			
			Mag. N.S.	38 15.0	30	s.	1.977	—011		
			Mag. S.	19 15.9	30	s.	1.984			
			wt. 1 gr.	11 08.5	30	s.	1.974			
			wt. 1½ gr.	16 55.4	30	s. ½ E.	2.015	—011		
			wt. 2 grs.	22 31.5	30	s.	1.963			
			wt. 2½ grs.	29 00.9	30	s.	1.983			
			wt. 3 grs.	35 06.1	30	s.	1.952	—011		
			wt. 3½ grs.	42 35.6	30	s. by E.	1.959			
			Def. N.	33 38.8	30	s. by E.	1.963			
	—68 49	199 26	Def. S.	31 04.3	30	s. by E.	1.938	+010		
			Def. N.	33 59.1	30	N.N.W.	1.952			
			Def. N.	33 46.1	32	s.W.	1.981			
			5. —68 52	198 24	Def. S.	30 46.1	32	s.W.	1.970	—006
					Mag. N.	28 35.2	32	s.W.	1.965	
					Mag. N.S.	38 24.0	32	s.W.	1.984	
					Mag. S.	19 18.6	32	s.W.	1.966	—005
					wt. 1 gr.	11 08.8	32	s.W. ½ w.	2.016	
					wt. 1½ gr.	16 59.2	32	s.W. ½ w.	1.974	
					wt. 2 grs.	22 30.9	32	s.W. ½ w.	1.961	—005
					wt. 2½ grs.	28 49.9	32	s.W. ½ w.	1.949	
					wt. 3 grs.	35 33.8	32	s.W. ½ w.	1.952	
	wt. 3½ grs.	42 40.2			32	s.W. ½ w.	1.982			
	6. —69 55	192 17			Def. N.	33 46.5	34	s. by w.	1.990	—010
					Def. S.	30 44.6	34	s. by w.	1.987	
			Mag. N.	28 21.7	34	s. by w.	1.953			
			Mag. N.S.	38 08.0	34	s. by w.	1.943	—010		
			Mag. S.	18 54.1	34	s.	1.980			
			Def. N.	33 44.5	34	s.	1.965			
			7. —70 05	191 03	Def. N.	33 53.9	30	s.s.w.	2.021	—009
					Def. S.	30 47.4	30	s.s.w.	1.948	
					Mag. N.	28 38.8	30	s.s.w.	1.947	
					Mag. N.S.	37 43.3	30	s.s.w.	1.989	—009
					Mag. S.	17 52.3	30	s.s.w.	1.977	
Def. N.					33 48.7	31	s.w.	2.020		
8. —70 08	186 39	Def. N.			33 49.3	31	s.w. by w.	1.961	—004	
		Def. S.			30 38.2	31	s.w. by w.	1.979		
		Mag. N.			28 30.9	31	s.w. by w.	2.007		
		Mag. N.S.			37 43.8	31	s.w. by w.	1.989	—004	
		Mag. S.			17 38.4	31	s.w. by w.	1.988		
		wt. 1 gr.			11 15.2	31	s.	1.980		
		—70 17	186 04	wt. 1½ gr.	16 52.1	31	s.	1.960	—009	
				wt. 2 grs.	22 37.0	31	s.	1.995		
				wt. 2½ grs.	28 35.7	31	s.	1.983		
				wt. 3 grs.	34 59.8	31	s.	2.034	—009	
				wt. 3½ grs.	41 52.3	31	s.			
				Def. N.	33 38.4	31	s.			
Def. S.	30 34.2			31	s.					
Mag. N.	28 26.8			31	s.					
Mag. N.S.	37 33.2			31	s.					
Mag. S.	17 17.7			31	s.					

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.	
Feb. 9.	-70 32	185 38	Def. N.	33 37.4	30	s.	1.961	-009	1.983	Head swell, very unsteady.	
			Def. S.	30 50.6	30	s.	1.976				
			Mag. N.S.	37 30.0	30	s.	2.039				
			Def. N.	33 43.4	30	S.E. by S.	1.955	-006			
			Def. S.	30 29.7	30	S. 1/2 E.	1.997				
			Mag. N.S.	37 29.7	30	S. 1/2 E.	2.039				
10.	-69 56	184 43	Def. N.	33 37.7	32	w. by S.	1.960	-000		Head swell, not steady.	
			Def. S.	30 47.2	32	w. by S.	1.980				
			Mag. N.	28 34.0	32	w. by S.	1.972				
			Mag. N.S.	37 56.0	32	w. by S.	2.004				
			Mag. S.	17 58.6	32	w. by S.					
11.	-69 51	183 02	Def. N.	33 37.5	32	W.S.W.	1.960	-001	1.988	Strong breeze, swell from the west, table not steady.	
			Def. S.	30 30.3	32	W.S.W.	1.997				
			Mag. N.	28 18.6	32	W.S.W.	1.994				
			Mag. N.S.	37 44.4	32	W.S.W.	2.029				
			Mag. S.	18 08.6	32	W.S.W.					
12.	-71 03	180 56	Def. N.	33 38.3	33	S.E. by S.	1.960	-006	1.988	Cross sea, table very unsteady.	
			Def. S.	30 37.8	33	S.E. by S.	1.989				
			Mag. N.	28 18.2	33	S.E. by S.	1.995				
			Mag. N.S.	37 51.2	33	S.E. by S.	2.011				
			Mag. S.	18 05.3	33	S.E. by S.					
13.	-72 07	181 50	Def. N.	33 22.3	31	S.E. by S.	1.976	-006	2.001	Swell from N.W., steering wildly, table unsteady.	
			Def. S.	30 42.3	31	S.E. by S.	1.985				
			Mag. N.	28 04.6	31	S.E. by S.	2.017				
			Mag. N.S.	37 27.2	31	S.E. by S.	2.044				
			Mag. S.	17 43.3	31	S.E. by S.					
14.	-72 55	181 33	Def. N.	33 14.6	30	S.E. by E.	1.983	-004	2.001	N.W. swell, ship unsteady.	
			Def. S.	30 22.9	30	S.E. by E.	2.004				
			Mag. N.	28 12.1	30	S.E. by E.	2.006				
			Mag. N.S.	37 31.9	30	S.E. by E.	2.036				
			Mag. S.	17 56.7	30	S.E. by E.					
16.	-74 51	174 02	Def. N.	33 12.5	28	S.S.E.	1.986	-006	2.008	Table steady.	
			Def. S.	30 26.1	28	S.S.E.	2.001				
			Mag. N.	27 52.3	28	S.S.E.	2.036				
			Mag. N.S.	37 19.9	28	S.S.E.	2.052				
			Mag. S.	17 45.9	28	S.S.E.					
	-75 09	173 16	wt. 1 gr.	11 09.7	28	E. 1/2 S.	1.976	-000	2.008	N.W. swell, motion slight.	
			wt. 1 1/2 gr.	16 40.5	28	E. 1/2 S.	2.001				
			wt. 2 grs.	21 41.0	28	E. 1/2 S.	2.090				
			wt. 2 1/2 grs.	28 13.7	28	E. 1/2 S.	2.013				
			wt. 3 grs.	34 53.1	28	E. 1/2 S.	1.995	-000			
			wt. 3 1/2 grs.	42 16.6	28	E. 1/2 S.	1.964				
			Def. N.	33 04.9	28	E. by S.	1.990				
			Def. S.	30 23.8	28	E. by S.	2.003				
			Mag. N.S.	37 27.9	28	E. by S.	2.042	-000	2.006	Steering wildly, table unsteady.	
17.	-76 06	174 57	Def. N.	33 25.4	32	E. by N. 1/2 N.	1.973				
			Def. S.	30 37.3	32	E. by N. 1/2 N.	1.990				
			Mag. N.	28 16.2	32	E. by N. 1/2 N.	1.999				
			Mag. N.S.	37 28.6	32	E. by N. 1/2 N.	2.041	+002			
			Mag. S.	17 38.4	32	E. by N. 1/2 N.					
18.	-77 02	181 37	Def. N.	33 12.4	27	E.N.E.	1.987		+004	2.007	Cross sea, table unsteady.
			Def. S.	30 36.1	27	E.N.E.	1.991				
			Mag. N.	28 17.4	27	E.N.E.	1.998				
			Mag. N.S.	37 31.7	27	E.N.E.	2.036				
			Mag. S.	17 49.0	27	E.N.E.					

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 19.	-76 48	184 46	Def. N.	33 16.1	25	N. by E.	1.983	+006	2.009	Head sea, ship unsteady.
			Def. S.	30 30.3	25	N. by E.	1.997			
			Mag. N.	28 14.8	25	N. by E.	2.002			
			Mag. N.S.	37 34.7	25	N. by E.	2.031			
			Mag. S.	17 30.6	25	N. by E.				
20.	-76 20	191 26	Def. N.	33 10.8	28	N.E.	1.988	+005	2.024	Head sea, ship unsteady.
			Def. S.	30 30.9	28	N.E.	1.996			
			Mag. N.	27 55.8	28	N.E.	2.030			
			Mag. N.S.	37 12.8	28	N.E.	2.062			
			Mag. S.	17 14.3	28	N.E.				
22.	-76 24	184 54	Def. N.	33 09.1	30	S.E. by S.	1.990	-005	2.004	Strong wind, head sea, unsteady.
			Def. S.	30 25.3	30	S.E. by S.	2.002			
			Mag. N.	28 11.1	30	S.E. by S.	2.007			
			Mag. N.S.	37 30.2	30	S.E. by S.	2.039			
			Mag. S.	17 41.0	30	S.E. by S.				
	-77 13	193 52	Def. N.	33 12.9	30	E. by S.	1.986	-000	2.011	Light swell, motion gentle.
			Def. S.	30 39.5	30	E. by S.	1.987			
			Mag. N.	28 21.0	30	E. by S.	1.991			
			Mag. N.S.	37 31.9	30	E. by S.	2.036			
			Mag. S.	17 13.0	30	E. by S.				
			wt. 1 gr.	10 55.0	30	E. by S.	2.021	+005	2.001	Table steady.
			wt. 1½ gr.	16 28.5	30	E. by S.	2.026			
			wt. 2 grs.	22 23.3	30	E. by S.	2.028			
			wt. 2½ grs.	28 07.5	30	E. by S.	2.020			
			wt. 3 grs.	34 16.6	30	E. by S.	2.025	+004	2.001	Table steady.
			wt. 3½ grs.	41 32.7	30	E. by S.	1.992			
23.	-77 47	197 25	Def. N.	33 28.8	29	N.E. by E.	1.969			
			Def. S.	30 36.2	29	N.E. by E.	1.991			
			Mag. N.	28 08.2	29	E.N.E.	2.011	+004	2.001	Table steady.
			Mag. N.S.	37 45.3	29	E.N.E.	2.018			
			Mag. S.	17 17.8	29	E.N.E.				
			Def. N.	33 10.3	30	S.W. by S.	1.989			
24.	-77 14	199 29	Def. S.	30 41.2	30	S.W. by S.	1.980	-005	1.992	Fresh breeze, swell from N.E., table steady.
			Mag. N.	28 22.9	30	S.W. by S.	1.989			
			Mag. N.S.	37 30.5	30	S.W. by S.	2.038			
			Mag. S.	17 25.3	30	S.W. by S.				
			wt. 1 gr.	11 02.2	30	S.W. by S.	2.000	-005	1.992	Fresh breeze, swell from N.E., table steady.
			wt. 1½ gr.	16 31.1	30	S.W. by S.	2.020			
			wt. 2 grs.	22 33.5	30	S.W. by S.	2.010			
			wt. 2½ grs.	28 40.4	30	S.W. by S.	1.983			
			wt. 3 grs.	34 58.0	30	S.W. by S.	1.989	-005	1.992	Fresh breeze, swell from N.E., table steady.
			wt. 3½ grs.	42 08.1	30	S.W. by S.	1.970			
25.	-75 20	194 36	Def. N.	33 05.2	29	W.	1.994			
			Def. S.	30 34.4	29	W.	1.993			
			Mag. N.	28 14.8	29	W.	2.000	+001	2.003	Fresh breeze, swell from N.E., table steady.
			Mag. N.S.	37 43.8	29	W.	2.020			
			Mag. S.	17 38.2	29	W.				
			Def. N.	33 17.7	29	N.W. by W.	1.980			
26.	-73 10	189 21	Def. S.	30 34.9	29	N.W. by W.	1.992	+005	2.000	Strong breeze, motion great.
			Mag. N.	28 06.6	29	N.W. by W.	2.012			
			Mag. N.S.	38 01.7	29	N.W. by W.	1.995			
			Mag. S.	17 13.8	29	N.W. by W.				
			Def. N.	33 22.8	26	S.W.	1.976	-005	1.999	Easterly swell, slight motion.
27.	-72 03	187 40	Def. S.	30 36.3	26	S.W.	1.991			
			Mag. N.	28 11.4	26	S.W.	2.007			
			Mag. N.S.	37 39.4	26	W. by N. ½ N.	2.025			
			Mag. S.	17 28.8	26	W. by N. ½ N.		+002	1.999	Easterly swell, slight motion.

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Feb. 27.	-72° 03'	187° 40'	wt. 1 gr.	11° 01' 0	26	s.w. $\frac{1}{2}$ w.	2.002	-005	1.999	Easterly swell, slight motion.
			wt. 1½ gr.	16 26.3	26	s.w. $\frac{1}{2}$ w.	2.029			
			wt. 2 grs.	22 13.8	26	s.w. $\frac{1}{2}$ w.	2.040			
			wt. 2½ grs.	28 25.7	26	s.w. $\frac{1}{2}$ w.	1.998			
			wt. 3 grs.	34 35.3	26	s.w. $\frac{1}{2}$ w.	2.009			
			wt. 3½ grs.	42 33.7	26	s.w. $\frac{1}{2}$ w.	1.953			
			wt. 1 gr.	11 04.8	26	w. by n. $\frac{1}{2}$ n.	1.990			
	-71 43	187 15	wt. 1½ gr.	16 01.3	26	w. by n. $\frac{1}{2}$ n.	2.081	+002	1.999	Easterly swell, slight motion.
			wt. 2 grs.	22 29.5	26	w. by n. $\frac{1}{2}$ n.	2.016			
			wt. 2½ grs.	28 37.6	26	w. by n. $\frac{1}{2}$ n.	1.986			
			wt. 3 grs.	34 56.6	26	w. by n. $\frac{1}{2}$ n.	1.990			
			wt. 3½ grs.	42 04.9	26	w. by n. $\frac{1}{2}$ n.	1.971			
			Def. N.	33 44.8	25	w. by s.	1.952			
			Def. S.	30 47.1	25	w. by s.	1.980			
28.	-71 20	184 30	Mag. N.	28 22.8	25	w. by s.	1.988	-000	1.999	Easterly swell, slight motion.
			Mag. N.S.	37 39.1	25	w. by s.	2.025			
			Mag. S.	17 44.3	25	w. by s.				
			Def. N.	33 24.5	32	w.n.w.	1.974			
			Def. S.	30 38.5	32	w.n.w.	1.989			
			Mag. N.	28 17.3	32	w.n.w.	1.998			
			Mag. N.S.	37 47.1	32	w.n.w.	2.015			
	-68 09	183 10	Mag. S.	17 43.2	32	w.n.w.		+005	1.999	Easterly swell, slight motion.
			Def. N.	33 34.6	32	n.n.e.	1.963			
			Def. S.	31 01.2	32	n.n.e.	1.966			
			Mag. N.	28 30.9	32	n.n.e.	1.977			
			Mag. N.S.	38 05.3	32	n.n.e.	1.990			
			Mag. S.	18 05.9	32	n.n.e.				
			Def. N.	33 30.0	31	n.e. by e.	1.968			
3.	-67 35	185 18	Def. S.	31 15.6	31	n.e. by e.	1.951	+006	1.978	Cross sea, ship unsteady.
			Mag. N.	28 29.3	31	n.e. by e.	1.979			
			Mag. N.S.	37 54.8	31	n.e. by e.	2.005			
			Mag. S.	18 00.1	31	n.e. by e.				
			wt. 1 gr.	11 07.4	31	n.e. by e.	1.986			
			wt. 1½ gr.	17 00.0	31	n.e. $\frac{1}{2}$ e.	1.965			
			wt. 2 grs.	22 48.2	31	n.e. $\frac{1}{2}$ e.	1.993			
	-67 40	187 40	wt. 2½ grs.	28 54.6	31	n.e. $\frac{1}{2}$ e.	1.970	+006	1.981	Strong gale, heavy sea, ship unsteady.
			wt. 3 grs.	35 30.5	31	n.e. $\frac{1}{2}$ e.	1.965			
			wt. 3½ grs.	42 54.1	31	n.e. $\frac{1}{2}$ e.	1.942			
			Def. N.	33 43.9	33	n. by w.	1.954			
			Def. S.	31 04.0	33	n. by w.	1.963			
			Mag. N.	28 23.5	33	n. by w.	1.988			
			Mag. N.S.	37 47.2	33	n. by w.	2.015			
4.	-67 09	188 02	Mag. S.	17 59.9	33	n. by w.		+011	1.981	Heavy sea from W.S.W., ship very unsteady.
			Def. N.	33 43.6	35	n.	1.954			
			Def. S.	31 47.7	35	n.	1.917			
			Mag. N.	28 36.4	35	n.	1.968			
			Mag. N.S.	37 57.1	35	n.	2.003			
			Mag. S.	17 50.3	35	n.				
			Def. N.	33 56.8	33	n. by e.	1.940			
5.	-65 28	191 24	Def. S.	31 20.9	33	n. by e.	1.945	+012	1.955	Swell from the S.S.W., table steady.
			Mag. N.	28 44.3	33	n. by e.	1.956			
			Mag. N.S.	38 07.4	33	n. by e.	1.988			
			Mag. S.	18 29.3	33	n. by e.				
			wt. 1 gr.	11 29.7	33	n. by e. $\frac{1}{2}$ e.	1.920			
			wt. 1½ gr.	17 20.6	33	n. by e. $\frac{1}{2}$ e.	1.928			
			wt. 2 grs.	23 10.9	33	n. by e. $\frac{1}{2}$ e.	1.963			
	-64 49	192 21						+012		

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 6.	—64 49	192 21	wt. 2½ grs.	29 34.9	33	N. by E. ½ E.	1.930	+012	1.955	Swell from the S.S.W., table steady.
			wt. 3 grs.	36 02.8	33	N. by E. ½ E.	1.940			
			wt. 3½ grs.	43 37.5	33	N. by E. ½ E.	1.917			
7.	—63 30	194 15	Def. N.	34 42.3	33	N. by E.	1.895	+012	1.942	Table steady.
			Def. S.	31 50.8	33	N. by E.	1.914			
			Mag. N.	29 04.3	33	N. by E.	1.926			
			Mag. N.S.	38 11.2	33	N. by E.	1.983			
			Mag. S.	18 24.5	33	N. by E.				
8.	—62 17	195 55	Def. N.	34 47.8	35	N. by E.	1.889	+014	1.916	Table steady.
			Def. S.	32 05.4	35	N. by E.	1.900			
			Mag. N.	29 00.5	35	N. by E.	1.931			
			Mag. N.S.	38 35.2	35	N. by E.	1.950			
			Mag. S.	18 46.6	35	N. by E.				
			wt. 1 gr.	11 47.0	35	N. by E.	1.875			
			wt. 1½ gr.	18 01.9	35	N. by E.	1.857			
			wt. 2 grs.	23 47.3	35	N. by E.	1.916			
			wt. 2½ grs.	30 03.9	35	N. by E.	1.902			
			wt. 3 grs.	37 04.3	35	N. by E.	1.894			
			wt. 3½ grs.	45 00.2	35	N. by E.	1.870			
9.	—61 06	198 08	Def. N.	34 50.2	35	N.E. ½ N.	1.887	+013		Sea getting up, unsteady.
			Def. S.	32 03.8	35	N.E. ½ N.	1.901			
			Mag. N.	29 15.0	35	N.E. ½ N.	1.910			
			Mag. N.S.	38 35.4	35	N.E. ½ N.	1.950			
			Mag. S.	18 55.7	35	N.E. ½ N.				
10.	—60 19	203 42	Def. N.	34 45.6	34	E.N.E.	1.891	+010	1.920	Ship unsteady.
			Def. S.	32 05.7	34	E.N.E.	1.899			
			Mag. N.	29 15.1	34	E.N.E.	1.910			
			Mag. N.S.	38 40.9	34	E.N.E.	1.942			
			Mag. S.	19 00.8	34	E.N.E.				
11.	—60 15	208 06	Def. N.	35 04.8	35	E. by N.	1.872	+007	1.907	Strong gale, heavy sea, ship very unsteady.
			Def. S.	31 58.7	35	E. by N.	1.906			
			Mag. N.	29 04.3	35	E. by N.	1.926			
			Mag. N.S.	38 46.5	35	E. by N.	1.935			
			Mag. S.	18 53.1	35	E. by N.				
12.	—60 16	211 45	Def. N.	35 04.2	35	E. by N.	1.873	+007		Heavy swell from S.W., unsteady.
			Def. S.	32 08.0	35	E. by N.	1.897			
			Mag. N.	29 25.5	35	E. by N.	1.894			
			Mag. N.S.	39 14.9	35	E. by N.	1.897			
			Mag. S.	18 53.3	35	E. by N.				
13.	—59 53	216 28	Def. N.	35 00.2	36	N.E. ½ E.	1.877	+015	1.910	Heavy swell, steering badly.
			Def. S.	32 11.9	36	N.E. ½ E.	1.893			
			Mag. N.	29 23.2	36	N.E. ½ E.	1.898			
			Mag. N.S.	39 02.3	36	N.E. ½ E.	1.914			
			Mag. S.	18 59.1	36	N.E. ½ E.				
14.	—59 22	218 14	Def. N.	35 07.5	37	N.E. ½ E.	1.870	+015	1.900	Heavy swell, very unsteady, steering badly.
			Def. S.	32 32.6	37	N.E. ½ E.	1.871			
			Mag. N.	29 36.2	37	N.E. ½ E.	1.879			
			Mag. N.S.	38 56.5	37	N.E. ½ E.	1.922			
			Mag. S.	19 00.9	37	N.E. ½ E.				
15.	—58 49	221 25	Def. N.	35 14.8	37	E.N.E.	1.862	+011	1.913	Heavy swell, steering badly.
			Def. S.	31 38.8	37	E.N.E.	1.927			
			Mag. N.	29 10.9	37	E.N.E.	1.917			
			Mag. N.S.	39 11.3	37	E.N.E.	1.902			
			Mag. S.	19 05.6	37	E.N.E.				

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 16.	—59 01	227 43	Def. N.	34 39.9	39	E.	1.897	+003	1.897	Heavyswell, steering badly.
			Def. S.	32 14.2	39	E.	1.891			
			Mag. N.	29 30.9	39	E.	1.887			
			Mag. N.S.	39 10.7	39	E.	1.903			
			Mag. S.	18 51.8	39	E.				
18.	—60 05	235 56	Def. N.	35 07.2	38	E. by S.	1.870	000	1.884	Heavy sea from S.W. by W., ship unsteady.
			Def. S.	32 36.0	38	E. by S.	1.868			
			Mag. N.	29 27.6	38	E. by S.	1.892			
			Mag. N.S.	39 08.7	38	E. by S.	1.904			
			Mag. S.	18 50.6	38	E. by S.				
	—60 17	236 38	Def. N.	35 02.5	38	E.	1.875	+003	1.892	The ship more steady.
			Def. S.	32 29.4	38	E.	1.875			
			Mag. N.	29 25.4	38	E.	1.896			
			Mag. N.S.	39 04.2	38	E.	1.911			
			Mag. S.	18 45.3	38	E.				
	—60 24	237 29	Def. N.	35 05.5	38	E. by N.	1.872	+007	1.907	Ship steady.
			Def. S.	32 07.2	38	E. by N.	1.898			
			Mag. N.	29 06.3	38	E. by N.	1.923			
			Mag. N.S.	39 05.9	38	E. by N.	1.909			
			Mag. S.	18 23.6	38	E. by N.				
21.	—59 05	247 27	Def. N.	35 50.2	38	E. by N.	1.830	+007	1.875	Cross sea, motion gentle.
			Def. S.	32 49.7	38	E. by N.	1.853			
			Mag. N.	29 27.6	38	E. by N.	1.892			
			Mag. N.S.	39 13.5	38	E. by N.	1.898			
			Mag. S.	19 10.0	38	E. by N.				
22.	—58 26	251 42	Def. N.	35 29.5	38	E. by N.	1.848	+007	1.885	Cross sea, ship unsteady.
			Def. S.	32 41.7	38	E. by N.	1.862			
			Mag. N.	29 27.9	38	E. by N.	1.891			
			Mag. N.S.	39 05.7	38	E. by N.	1.909			
			Mag. S.	19 23.5	38	E. by N.				
23.	—58 33	254 45	wt. 1 gr.	12 12.4	33	E. $\frac{1}{2}$ N.	1.812	+006	1.824	Little motion.
			wt. $1\frac{1}{2}$ gr.	18 20.0	33	E. $\frac{1}{2}$ N.	1.828			
			wt. 2 grs.	25 22.7	33	E. $\frac{1}{2}$ N.	1.803			
			wt. $2\frac{1}{2}$ grs.	31 29.0	33	E. $\frac{1}{2}$ N.	1.825			
			wt. 3 grs.	39 04.8	33	E. $\frac{1}{2}$ N.	1.812			
			wt. $3\frac{1}{2}$ grs.	47 40.6	33	E. $\frac{1}{2}$ N.	1.780			
			Def. N.	36 13.8	33	E. $\frac{1}{2}$ N.	1.806			
			Def. S.	33 24.9	33	E. $\frac{1}{2}$ N.	1.818			
			Mag. N.	29 55.5	33	E. $\frac{1}{2}$ N.	1.850			
			Mag. N.S.	39 49.9	33	E. $\frac{1}{2}$ N.	1.851			
			Mag. S.	19 52.7	33	E. $\frac{1}{2}$ N.				
24.	—58 40	257 32	Def. N.	36 09.9	35	E. by N.	1.810	+010	1.832	Little motion.
			Def. S.	33 27.9	35	E. by N.	1.815			
			Mag. N.	29 47.9	35	E. by N.	1.862			
			Mag. N.S.	39 36.0	35	E. by N.	1.869			
			Mag. S.	19 56.5	35	E. by N.				Little motion; overcast and damp.
	—58 53	258 55	wt. 1 gr.	12 30.1	35	E. by N.	1.770			
			wt. $1\frac{1}{2}$ gr.	18 17.1	35	E. by N.	1.837			
			wt. 2 grs.	25 22.4	35	E. by N.	1.803			
			wt. $2\frac{1}{2}$ grs.	31 46.5	35	E. by N.	1.810			
26.	—58 59	267 50	Def. N.	36 48.2	45	E. by N. $\frac{1}{2}$ N.	1.773	+012	1.783	Motion gentle.
			Def. S.	34 31.2	45	E. by N. $\frac{1}{2}$ N.	1.753			
			Mag. N.	30 53.2	45	E. by N. $\frac{1}{2}$ N.	1.771			
			Mag. N.S.	40 39.9	45	E. by N. $\frac{1}{2}$ N.	1.786			
			Mag. S.	20 37.6	45	E. by N. $\frac{1}{2}$ N.				

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Mar. 27.	-59 01	272 06	Def. N.	37 29.4	36	E.N.E.	1.734	+013	1.747	Ship unsteady.
			Def. S.	35 37.2	36	E.N.E.	1.687			
			Mag. N.	31 21.2	36	E.N.E.	1.734			
			Mag. N.S.	40 47.4	36	E.N.E.	1.780			
			Mag. S.	20 48.3	36	E.N.E.		+016	1.722	Swell from S.W., slight motion.
28.	-58 24	276 18	Def. N.	38 14.0	39	N.E. by E.	1.690			
			Def. S.	35 38.0	39	N.E. by E.	1.686			
			Mag. N.	31 57.2	39	N.E. by E.	1.684			
			Mag. N.S.	40 59.0	39	N.E. by E.	1.763	+017	1.672	Slight motion. Needle very unsteady (omitted in the mean).
			Mag. S.	20 51.8	39	N.E. by E.				
29.	-58 25	279 44	wt. 1 gr.	13 14.6	45	N.E. by E.	1.676			
			wt. 1½ grs.	20 00.5	45	N.E. by E.	1.684			
			wt. 2 grs.	28 08.5	45	N.E. by E.	1.642	+015	1.648	Slight motion.
			wt. 2½ grs.	36 37.1	45	N.E. by E.	1.601			
			Def. N.	38 49.8	45	N.E. by E.	1.656			
			Def. S.	36 09.1	45	N.E. by E.	1.658			
			Mag. N.	32 21.1	45	N.E. by E.	1.651	+021	1.648	Slight motion.
			Mag. N.S.	41 45.0	45	N.E. by E.	1.705			
			Mag. S.	21 53.0	45	N.E. by E.				
			Def. N.	38 25.5	40	E.N.E.	1.680			
30.	-58 31	281 33	Def. S.	36 04.1	40	E.N.E.	1.661	+021	1.648	Slight motion.
			Mag. N.	32 15.8	40	E.N.E.	1.658			
			Mag. N.S.	41 37.5	40	E.N.E.	1.714			
			Mag. S.	21 26.3	40	E.N.E.				
31.	-58 36	285 33	Def. N.	39 35.3	44	N.E.	1.611	+024	1.592	Strong breeze, ship unsteady, steering wild.
			Def. S.	36 46.6	44	N.E.	1.619			
			Mag. N.	32 48.3	44	N.E.	1.613			
			Mag. N.S.	42 15.6	44	N.E.	1.664			
			Mag. S.	22 13.4	44	N.E.		-017	1.495	Heavy sea, ship unsteady.
Apr. 1.	-57 21	289 36	Def. N.	40 12.8	47	N.E. by N.	1.573			
			Def. S.	36 33.8	47	N.E. by N.	1.632			
			Mag. N.	33 28.9	47	N.E. by N.	1.554			
			Mag. N.S.	42 50.4	47	N.E. by N.	1.622	+022	1.495	Heavy sea, ship unsteady.
			Mag. S.	22 29.8	47	N.E. by N.				
2.	-57 26	291 32	Def. N.	40 13.1	44	S.E.	1.573			
			Def. S.	37 44.6	44	S.E.	1.561			
			Mag. N.	33 23.9	44	S.E.	1.562	+025	1.355	Ship steady.
			Mag. N.S.	42 47.3	44	S.E.	1.627			
			Mag. S.	23 07.7	44	S.E.				
			Def. N.	41 28.4	44	N.E.	1.505			
3.	-56 37	294 34	Def. S.	38 40.8	44	N.E.	1.506	+025	1.355	Ship steady.
			Mag. N.	33 47.9	44	N.E.	1.527			
			Mag. N.S.	44 02.5	44	N.E.	1.523			
			Mag. S.	24 06.6	44	N.E.				
			Def. N.	42 33.1	44	N.E.	1.443	+025	1.355	Ship steady.
4.	-54 48	297 21	Def. S.	40 06.6	44	N.E.	1.428			
			Mag. N.	35 00.8	44	N.E.	1.420			
			Mag. N.S.	45 01.4	44	N.E.	1.440			
			Mag. S.	25 06.5	44	N.E.		+025	1.355	Ship steady.
			Def. N.	44 47.8	44	N.N.E.	1.325			
			Def. S.	42 29.0	44	N.N.E.	1.307			
			Mag. N.	36 03.2	44	N.N.E.	1.326			
			Mag. N.S.	46 17.6	44	N.N.E.	1.326	+025	1.355	Ship steady.
			Mag. S.	25 40.2	44	N.N.E.				
			wt. 1 gr.	17 23.4	44	N.N.E.	1.284			
			wt. 1½ gr.	26 11.2	44	N.N.E.	1.304			

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.	
Apr. 5.	-52° 40'	299° 52'	wt. 2 grs.	34° 54.7	44	N.N.E.	1.351	+0.025	1.355	Ship steady.	
			wt. 2½ grs.	45 13.0	44	N.N.E.	1.344				
			wt. 3 grs.	54 16.9	44	N.N.E.	1.408	+0.025	1.340	Ship steady.	
			Def. N.	44 40.6	44	N.N.E.	1.327				
			Def. S.	42 04.5	44	N.N.E.	1.326				
	Mag. N.	36 12.5	44	N.N.E.	1.313						
	Mag. N.S.	46 43.3	44	N.N.E.	1.290						
	-52° 28'	301° 42'	Mag. S.	25 58.0	44	N.N.E.	+0.024	1.346	Slight motion.		
			Def. N.	44 52.9	44	N.N.W. ½ W.				1.319	
			Def. S.	42 26.1	44	N.N.W. ½ W.				1.308	
			Mag. N.	36 14.5	44	N.N.W. ½ W.				1.309	
			Mag. N.S.	46 16.5	44	N.N.W. ½ W.				1.332	
	6.	-51° 42'	301° 36'	Mag. S.	26 08.0	44	N.N.W. ½ W.	+0.009	1.346	Single anchor in Port Louis, Berkeley Sound.	
				Def. N.	44 21.2	44	W. ½ N.				1.346
				Def. S.	42 02.4	44	W. ½ N.				1.328
				Def. N.	44 58.5	43					1.314
				Def. S.	41 52.8	43					1.335
	9.	Falkland Islands.		Mag. N.	35 57.0	43		1.336	Mean of all the results obtained with weights at Port Louis 1.336.		
				Mag. N.S.	46 13.9	43		1.335			
Mag. S.				25 37.0*	43						
wt. 1 gr.				16 56.5	43		1.316				
wt. 1½ gr.				25 36.6	43		1.331				
wt. 2 grs.				34 47.2	43		1.356				
wt. 2½ grs.				45 34.1	43		1.336				
wt. 3 grs.				57 39.1	43		1.353				
Def. N.				44 27.0	43		1.340				
Def. S.				42 00.4	43	Observed on shore.	1.330				
10.	-51° 32'	301° 53'	Mag. N.	36 00.0	43		1.331				
			Mag. N.S.	46 13.2	43		1.336				
			Mag. S.	25 42.8	43						
			wt. 1 gr.	16 51.2	43		1.323				
			wt. 1½ gr.	25 34.3	43		1.333				
			wt. 2 grs.	34 47.8	43		1.355				
			wt. 2½ grs.	45 29.7	43		1.338				
			wt. 3 grs.	57 48.7†	43		1.350				
			Def. N.	44 29.0	38		1.339				
			July 25.			Def. S.	41 58.0			38	
Mag. N.	36 00.9	38					1.330				
Mag. N.S.	46 14.8	38					1.333				
Aug. 15.										At the Magnetic Station.	

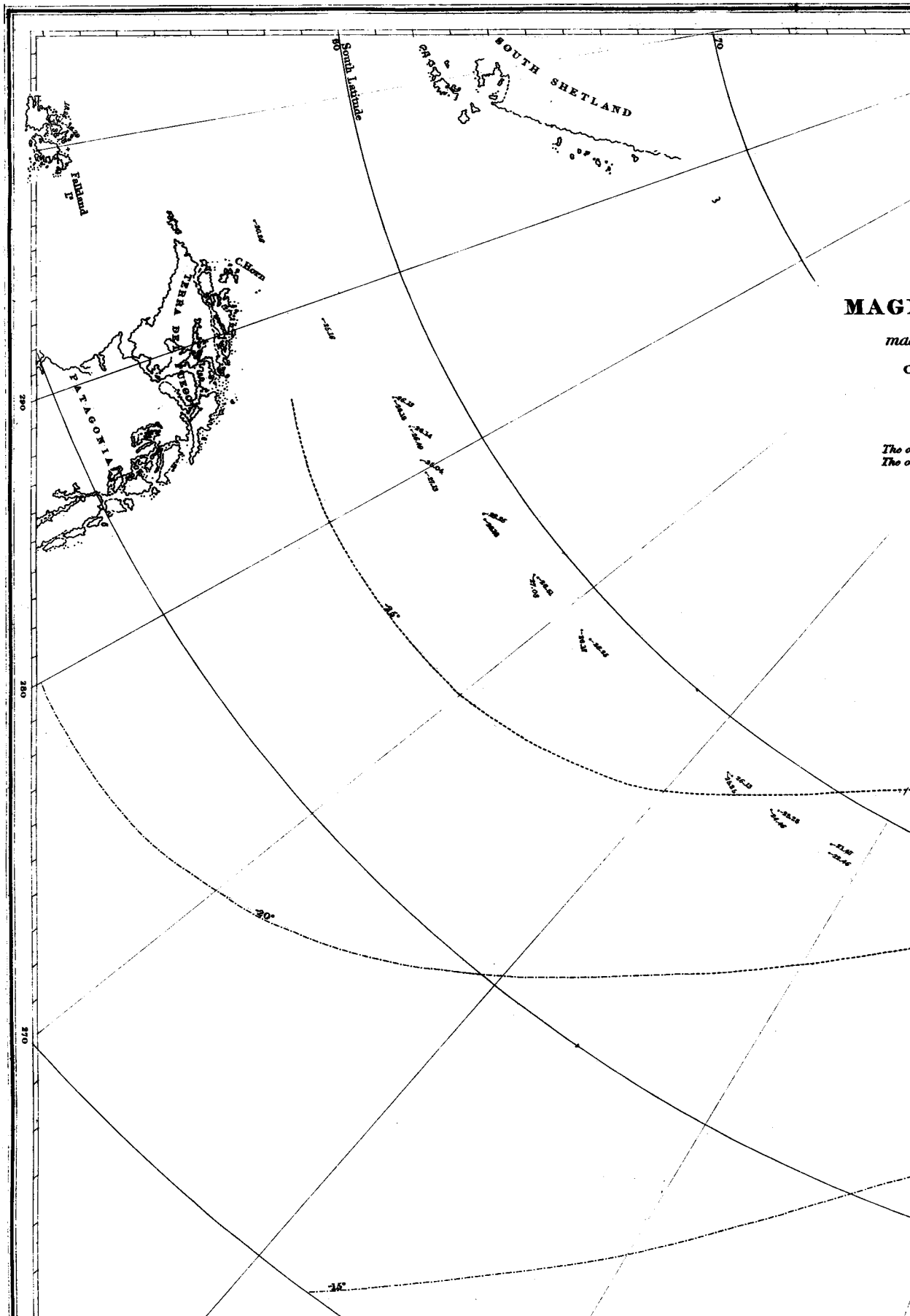
* Observed on shore; face west.	wt. 1 gr.	16° 14.1	Intensity.
	wt. 1½ gr.	24 36.9	1.316
	wt. 2 grs.	33 44.9	1.338
	wt. 2½ grs.	44 31.3	1.342
	wt. 3 grs.	58 17.8	1.334
† Observed on shore; face west.	wt. 1 gr.	16 26.1	1.333
	wt. 1½ gr.	24 27.9	1.301
	wt. 2 grs.	33 49.5	1.345
	wt. 2½ grs.	44 17.1	1.339
	wt. 3 grs.	58 19.5	1.339

Observations of the Magnetic Force. (Continued.)

1842.	Lat.	Long.	Method employed.	Angle of deflection. Face east.	Temperature.	Ship's head.	Intensity.	Correction for ship's attraction.	Corrected Intensity.	Remarks.
Aug. 15.	°	°	Mag. S.	25 52.1*	38	Observed on shore.			Mean of all the results obtained with weights at Port Louis 1.336.	At the Magnetic Station.
			wt. 1 gr.	17 00.4	38		1.311			
			wt. 1½ gr.	25 37.3	38		1.331			
			wt. 2 grs.	34 24.4	38		1.369			
			wt. 2½ grs.	45 20.1	38		1.341			
			wt. 3 grs.	57 43.6	38		1.352			
18.			Def. N.	44 27.0	38		1.340			
			Def. S.	41 59.6	38		1.330			
			Mag. N.	35 59.3	38		1.332			
			Mag. N.S.	46 12.2	38		1.338			
Aug. 15.	At anchor in Berkeley Sound.	To obtain corrections for the ship's attraction.	Mag. S.	25 43.8	38				1.342	
			Def. N.	44 59.4	40	E. ½ S.	1.313	+007		
			Def. N.	44 32.3	40	E.	1.336	+009		
			Def. N.	44 10.0	40	E.S.E.	1.355	-003		
			Def. N.	43 52.8	40	S.E.	1.370	-014		
			Def. N.	43 55.3	40	S.S.E.	1.368	-023		
			Def. N.	43 52.3	40	S.	1.370	-024		
			Def. N.	43 57.8	40	S.S.W.	1.366	-023		
			Def. N.	44 05.9	40	S.W.	1.359	-014		
			Def. N.	44 22.3	40	W.S.W.	1.345	-003		
			Def. N.	44 47.5	40	W.	1.324	+009		
			Def. N.	45 06.1	40	W.N.W.	1.308	+017		
			Def. N.	45 01.7	40	N.W.	1.312	+023		
			Def. N.	44 59.7	40	N.N.W.	1.313	+025		
			Def. N.	44 52.2	40	N.	1.320	+026		
			Def. N.	44 57.2	40	N.N.E.	1.315	+025		
			Def. N.	44 59.0	40	N.E.	1.314	+023		
			Def. N.	44 32.5	40	E.N.E.	1.336	+017		

* Observed on shore;
face west.

wt. 1 gr.	16 15.4	Intensity.	1.315
wt. 1½ gr.	24 30.1		1.344
wt. 2 grs.	33 57.8		1.335
wt. 2½ grs.	44 32.3		1.333
wt. 3 grs.	57 35.7		1.344



MAGNETIC DECLINATION

made in the Expedition commanded by

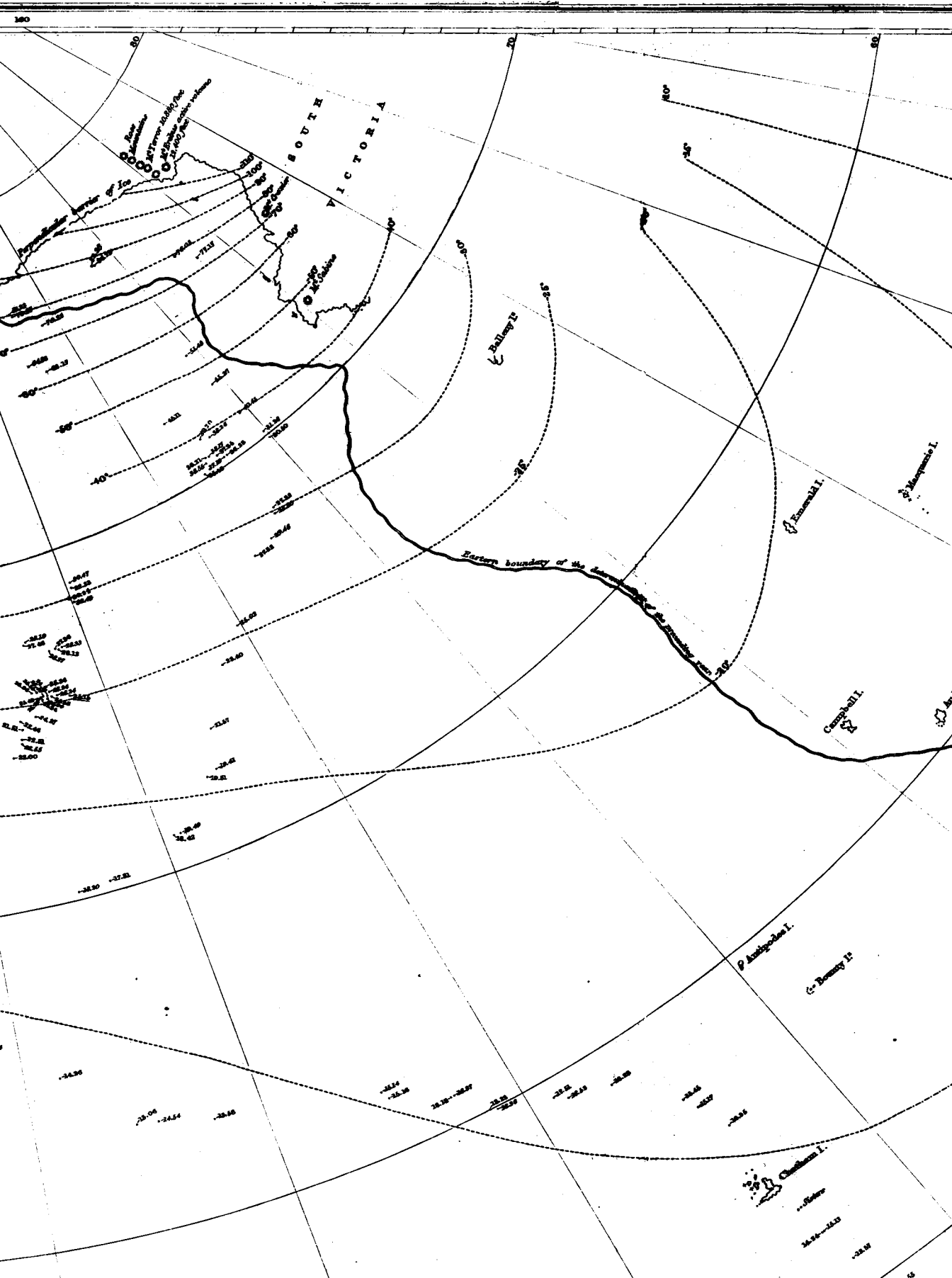
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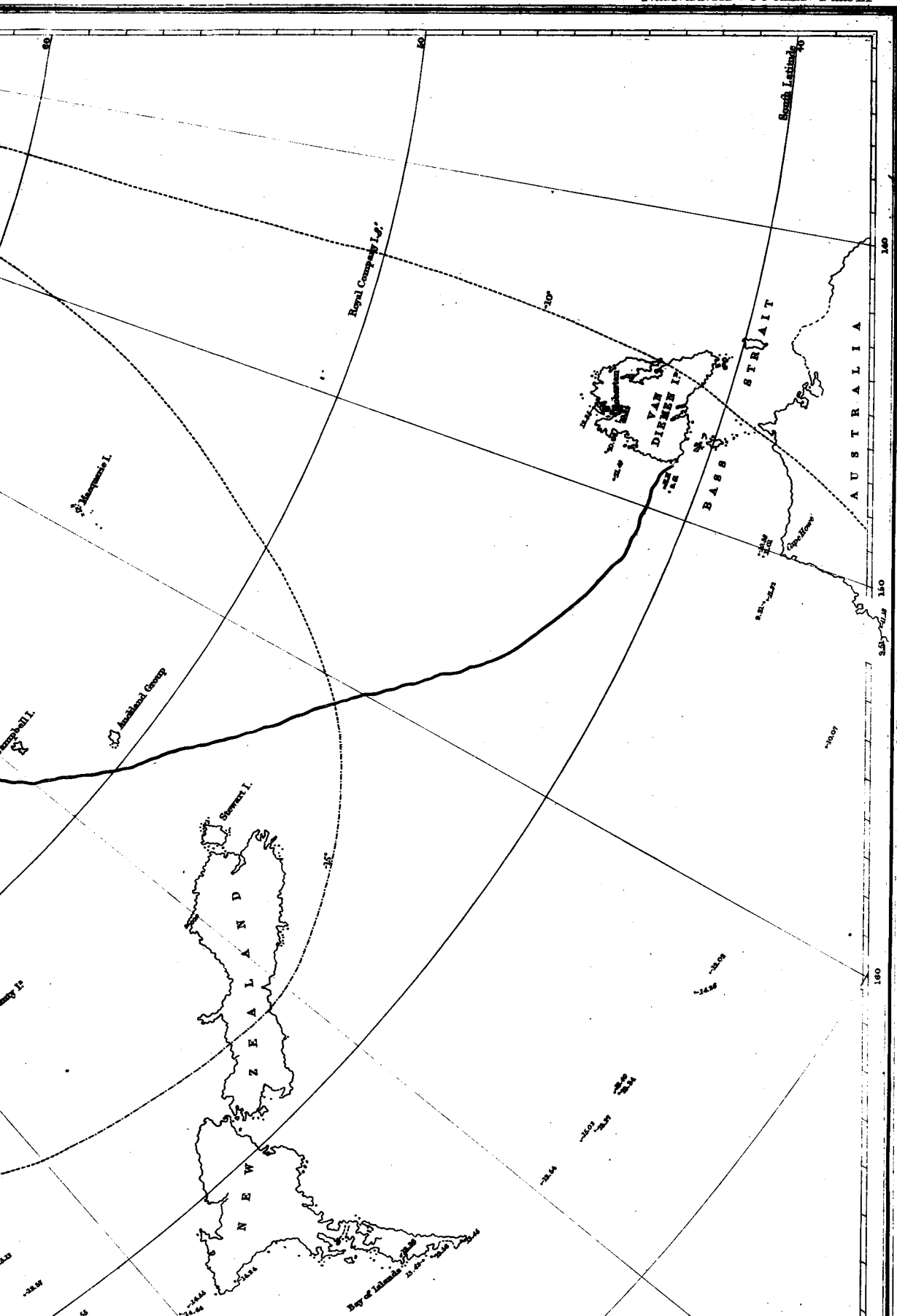
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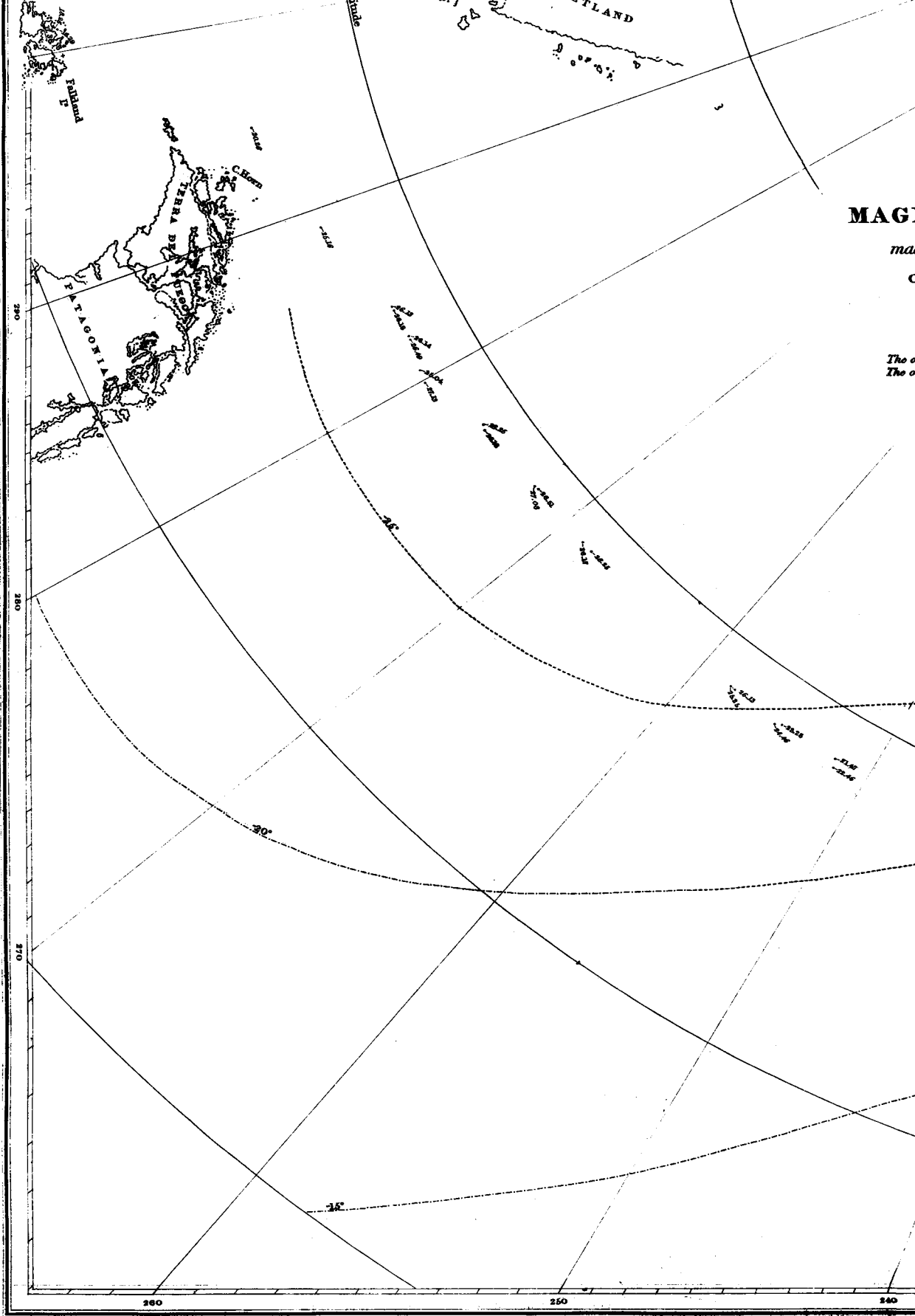
May 1841. and August 1842.

The observations of the Erebus are in Roman and-ss.10
The observations of the Terror are in Italics. that-ss.10

The observations of the Terror are in *Italics*. ~~that is so~~







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MAGNETIC DECLINATION

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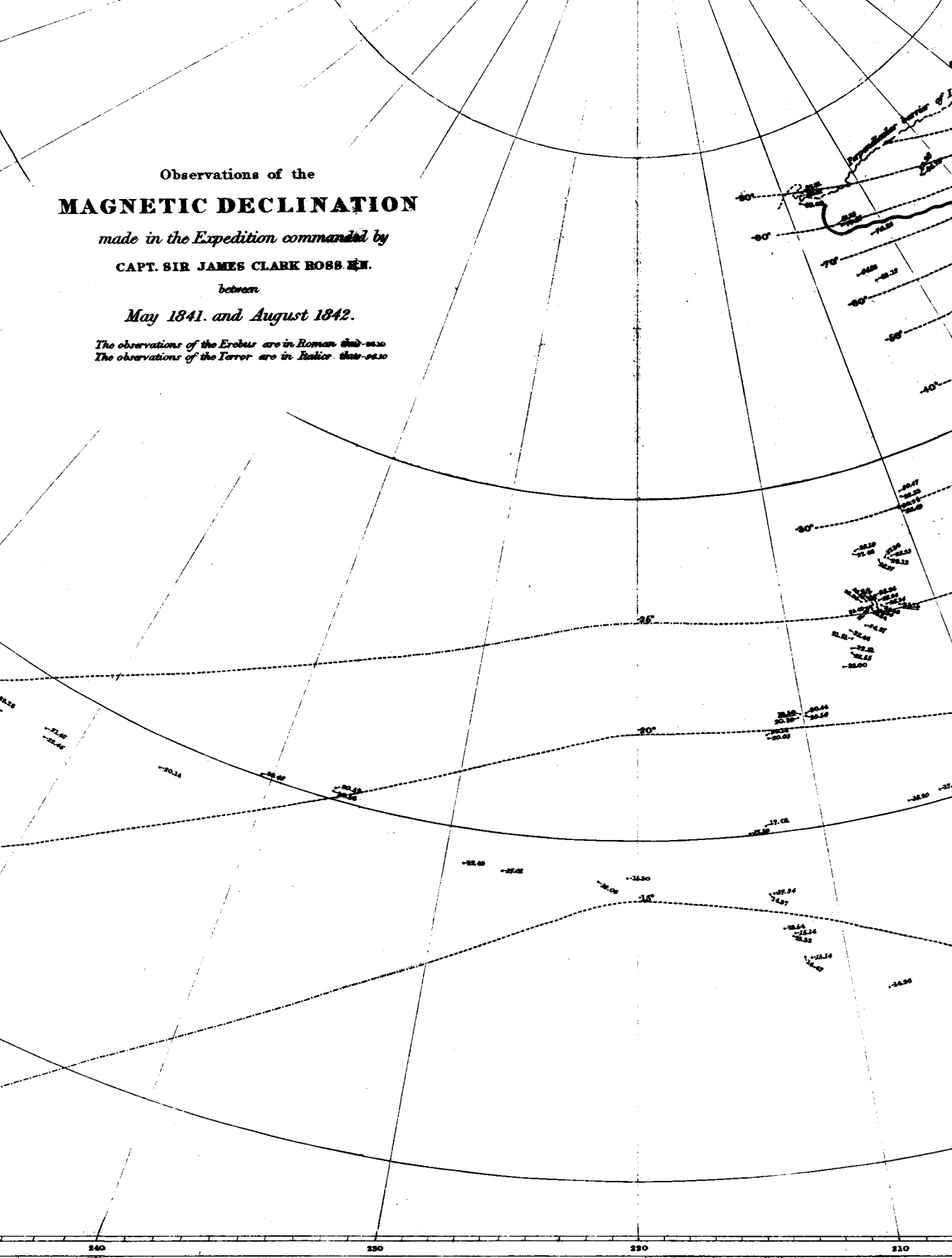
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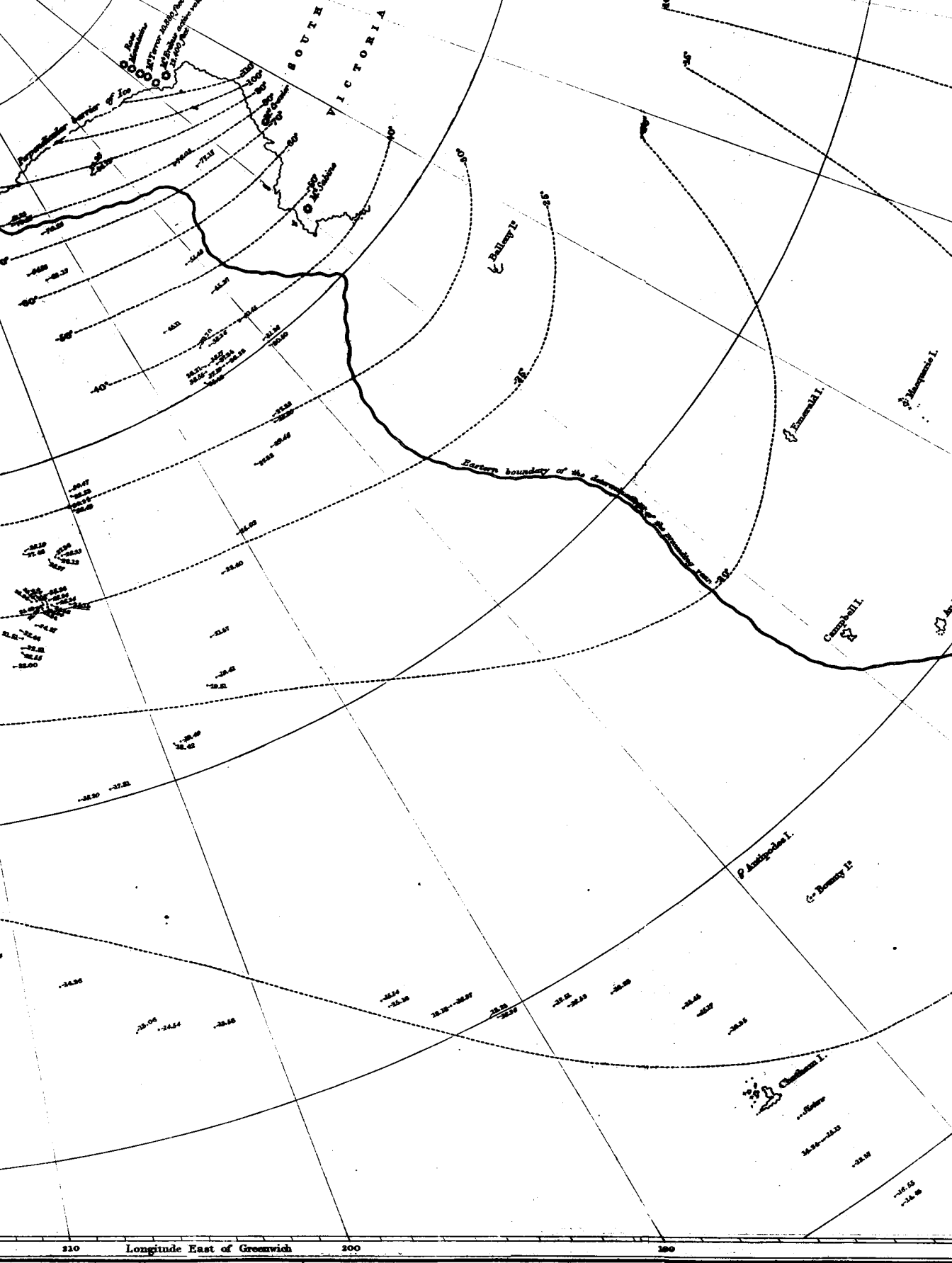
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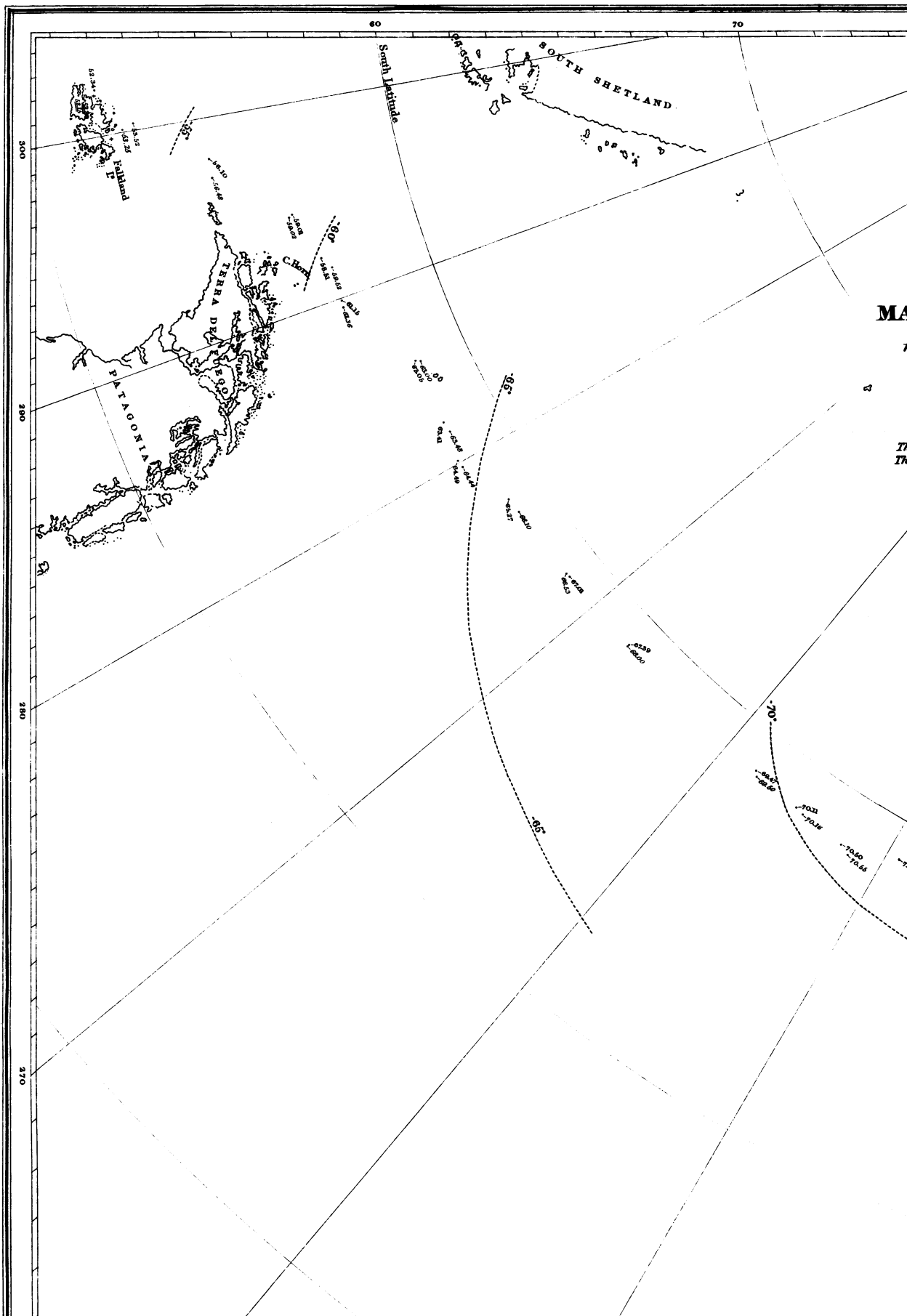
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The observations of the Erebus are in Roman. this-ss.10
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The observations of the Terror are in *Italics*. that-06.10







Observations of the
MAGNETIC INCLINATION

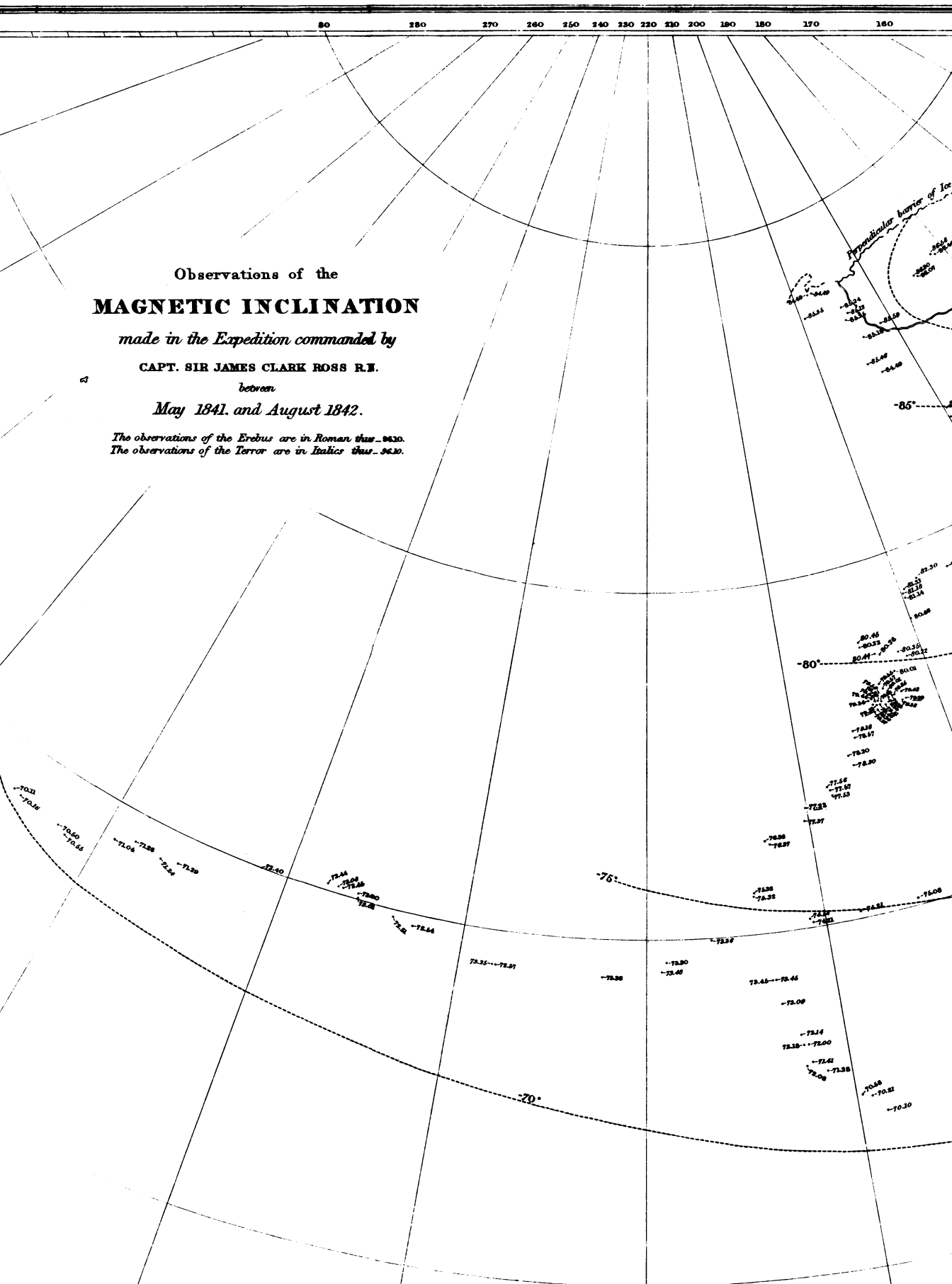
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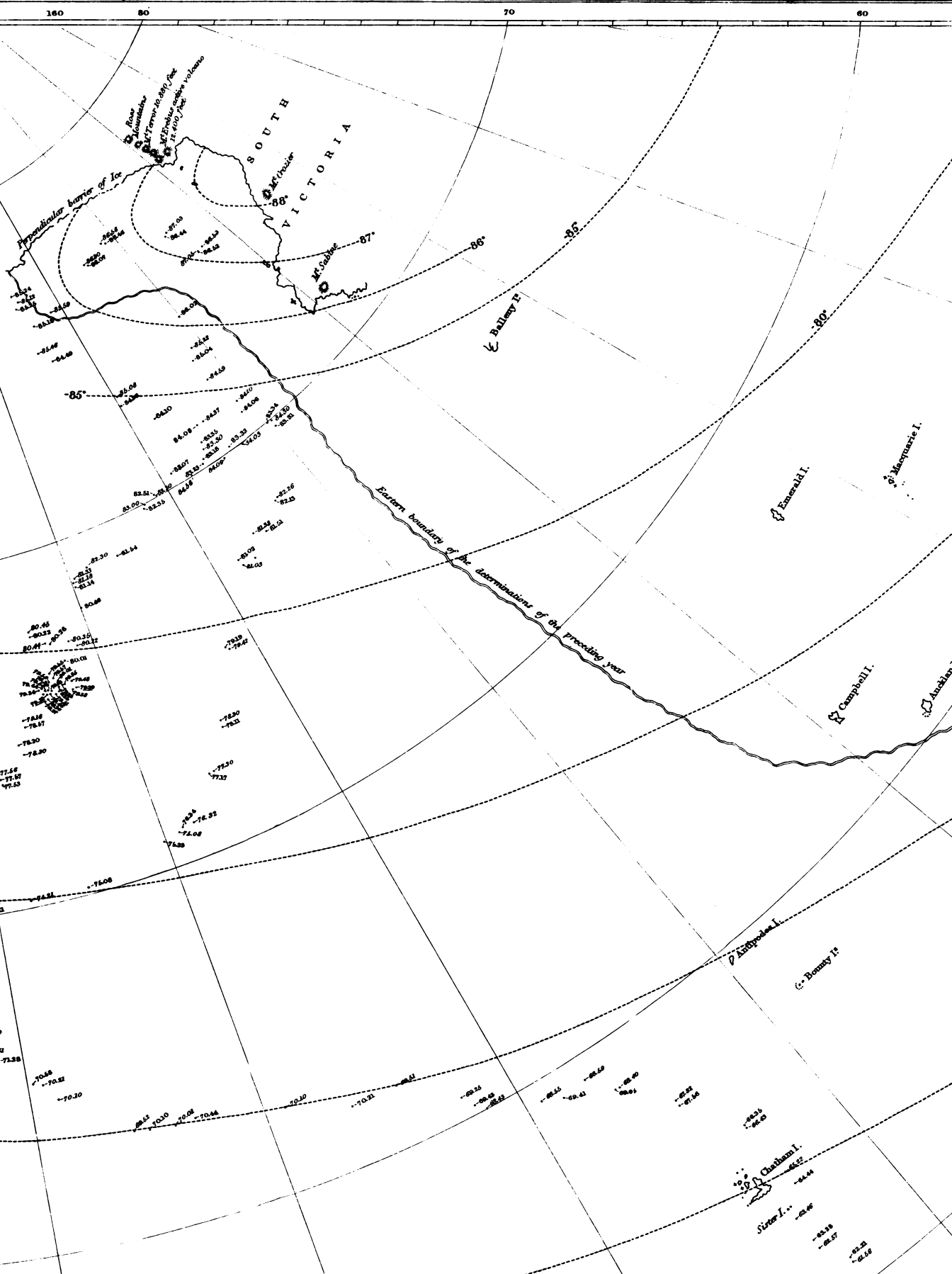
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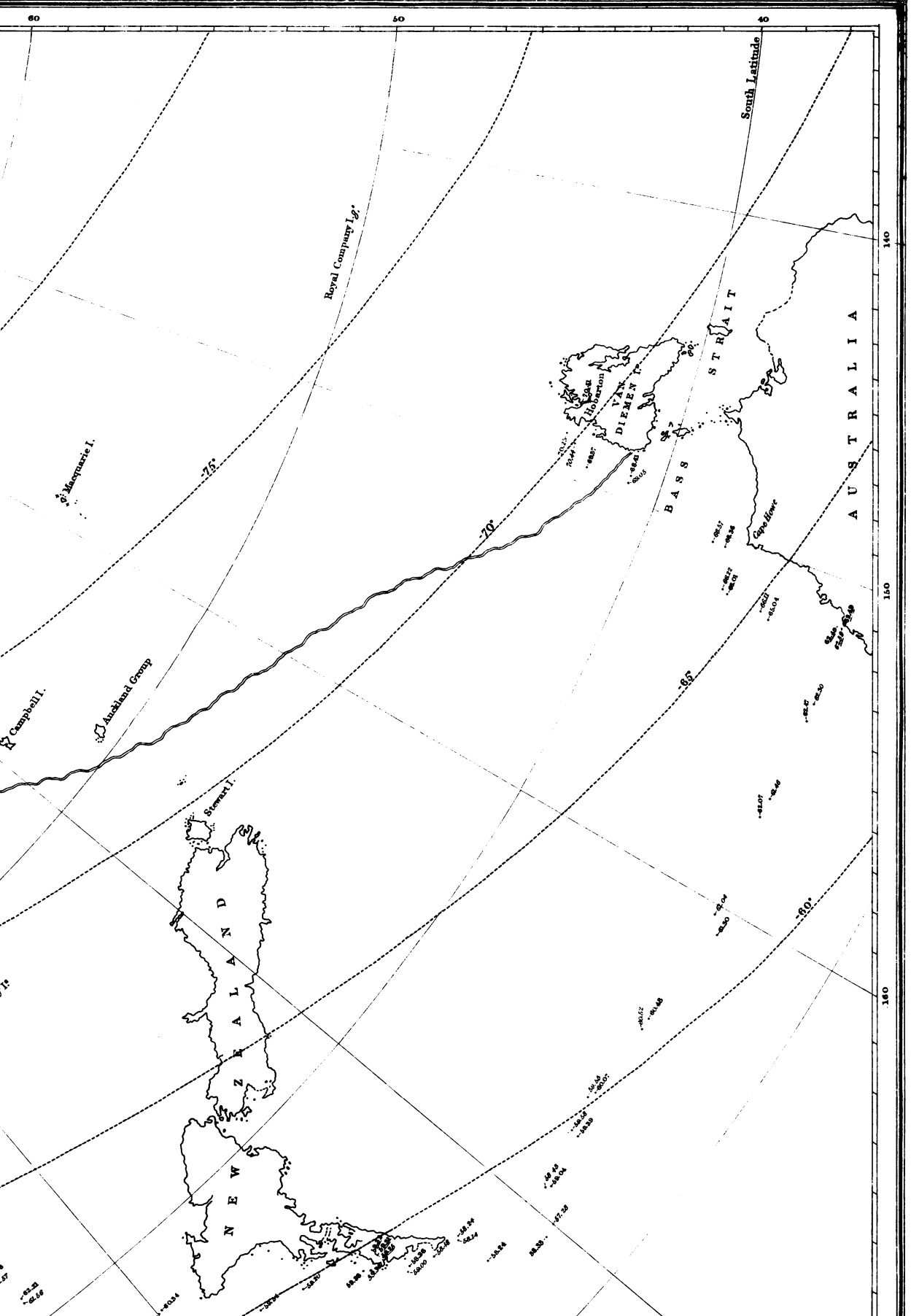
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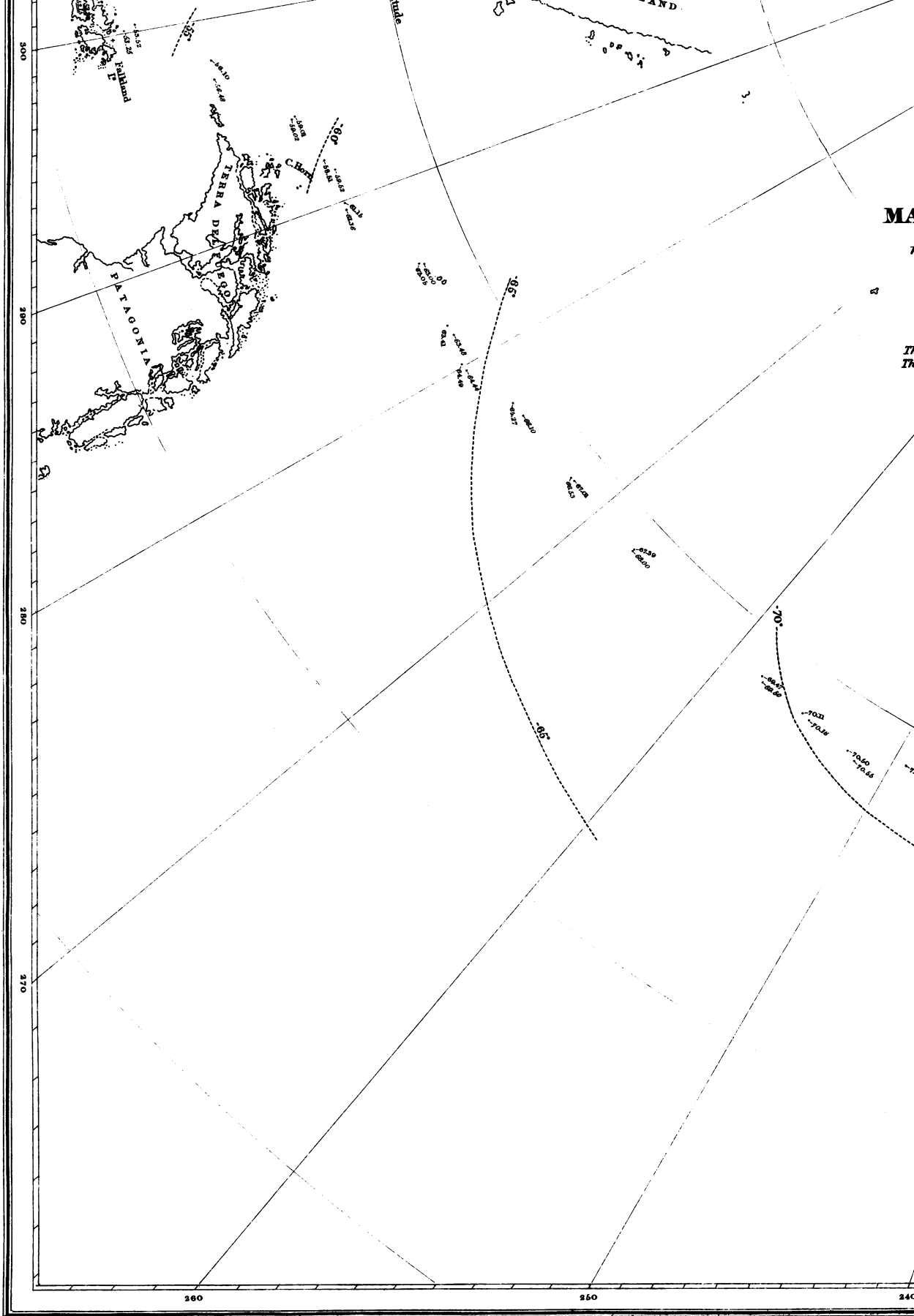
May 1841. and August 1842.

*The observations of the Erebus are in Roman thus. 86.30.
The observations of the Terror are in Italic thus. 86.30.*

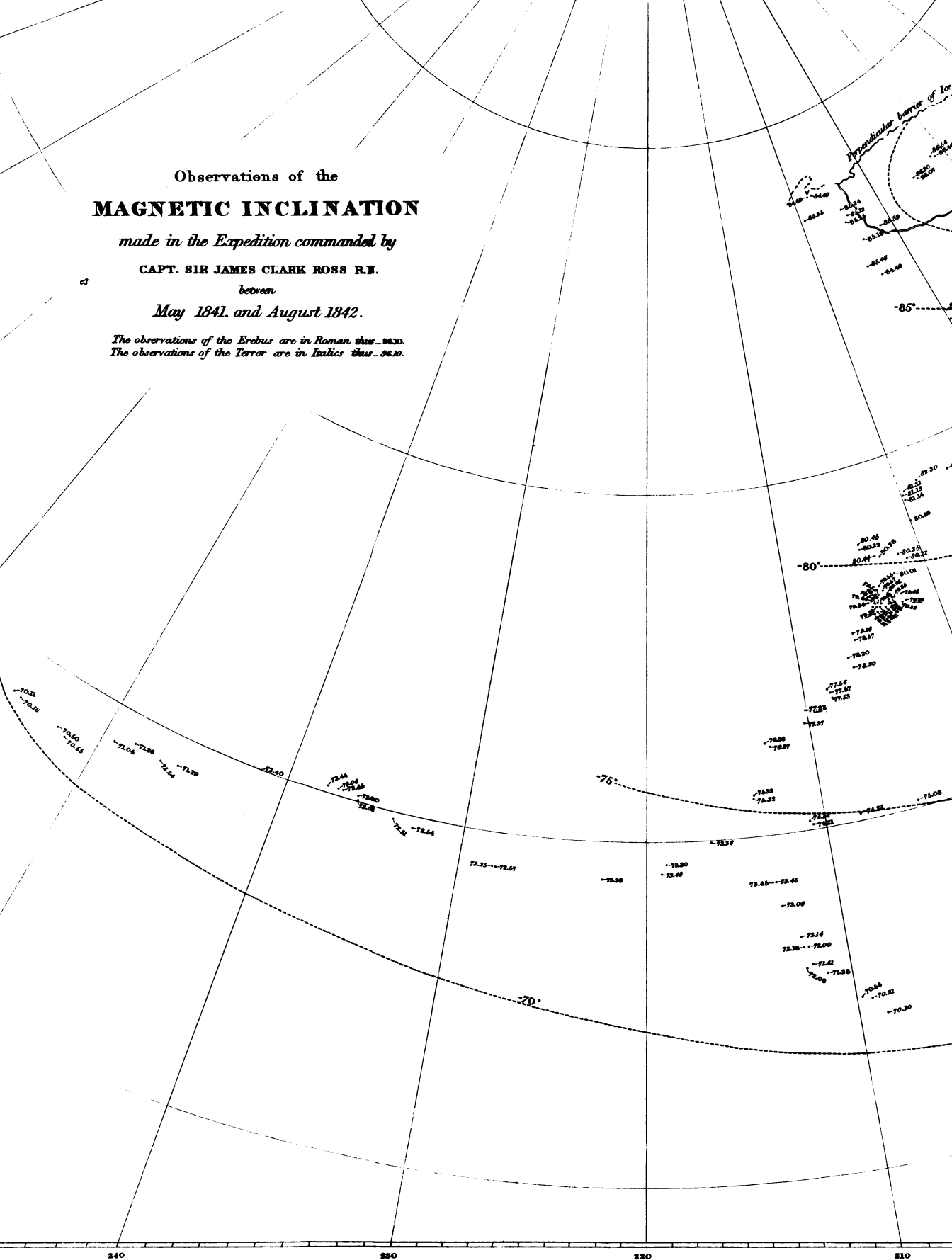


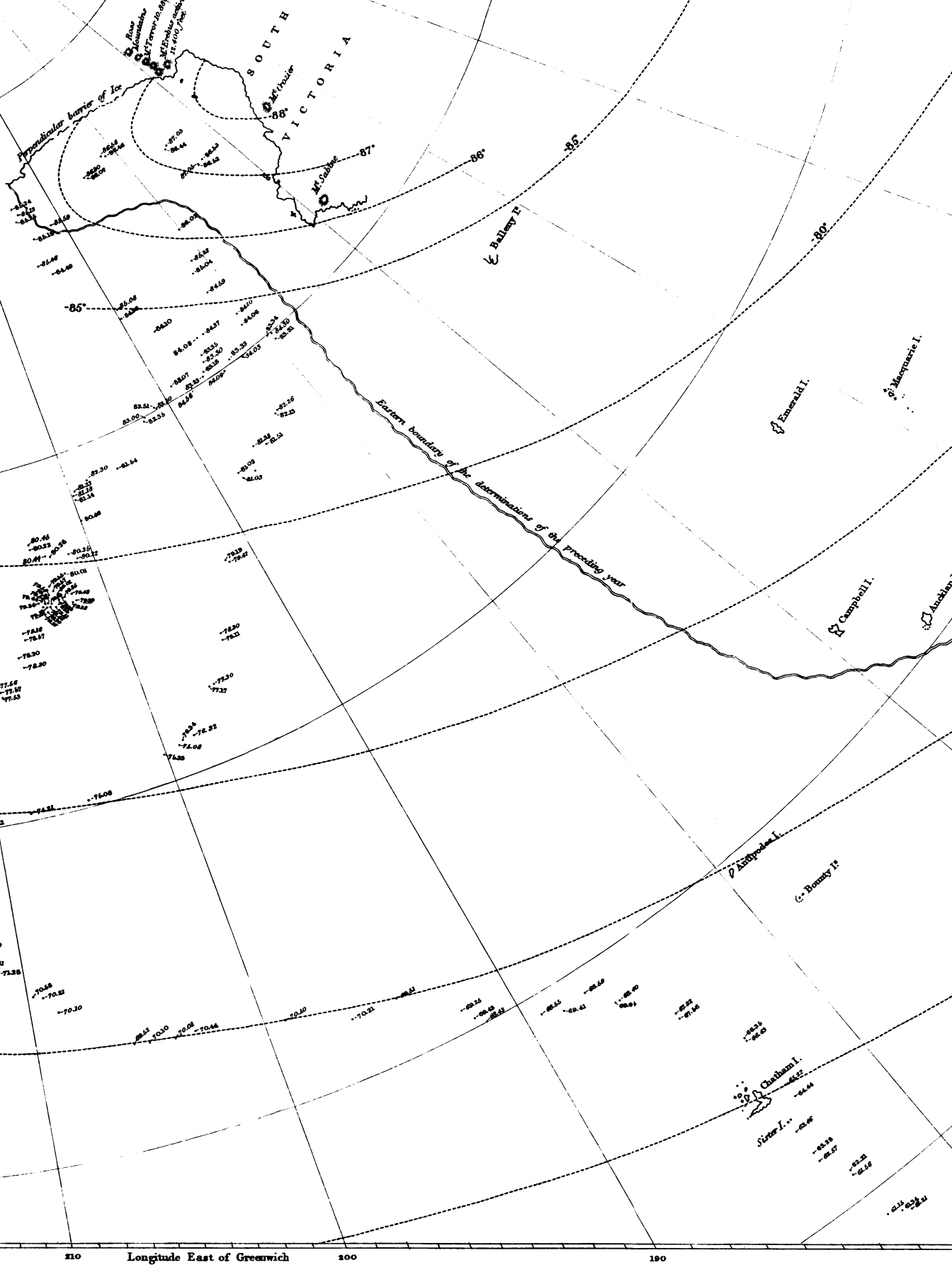






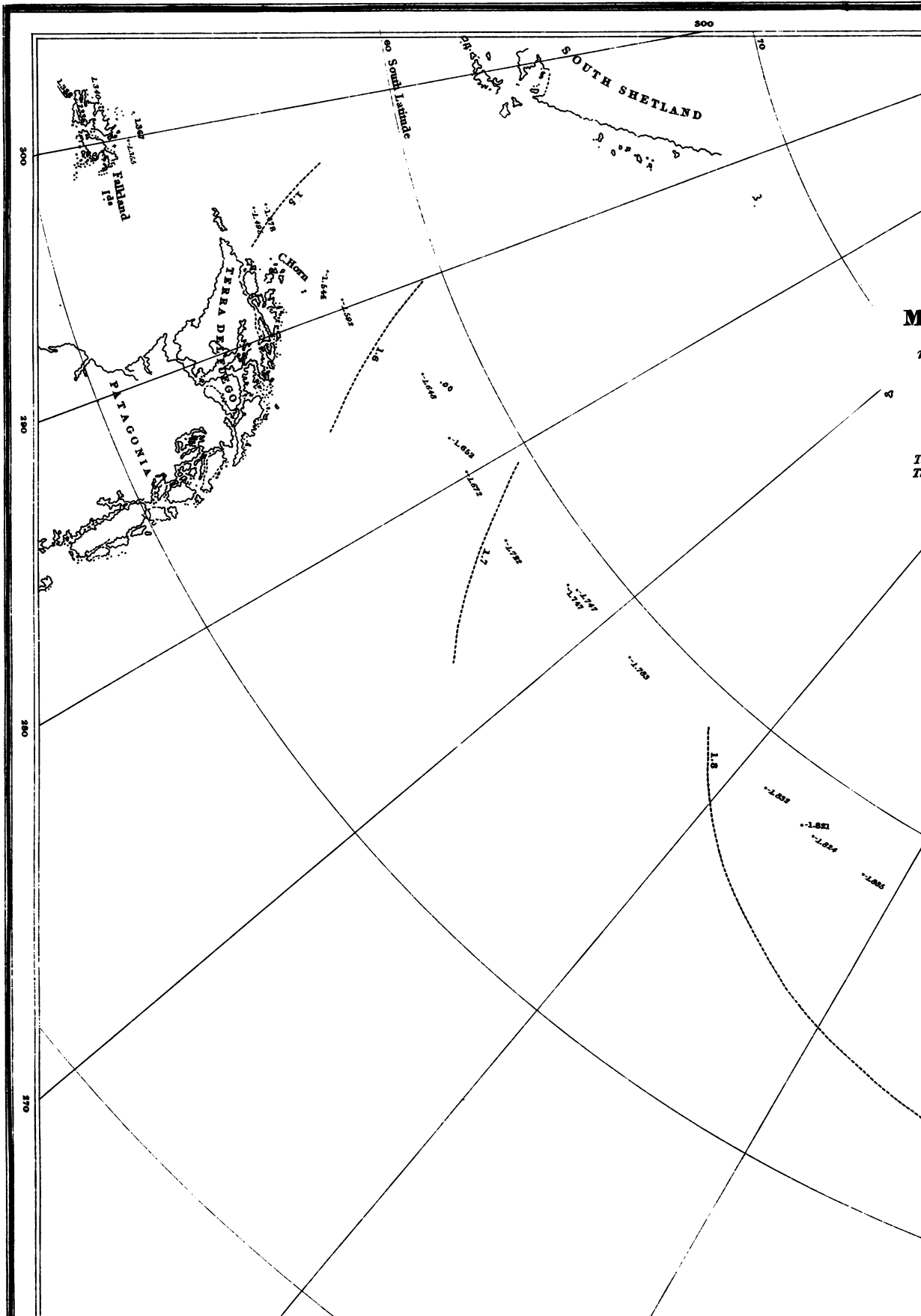
The observations of the Erebus are in Roman thus—0630.
The observations of the Terror are in Italics thus—0630.





Longitude East of Greenwich

190



Observations of the
MAGNETIC INTENSITY

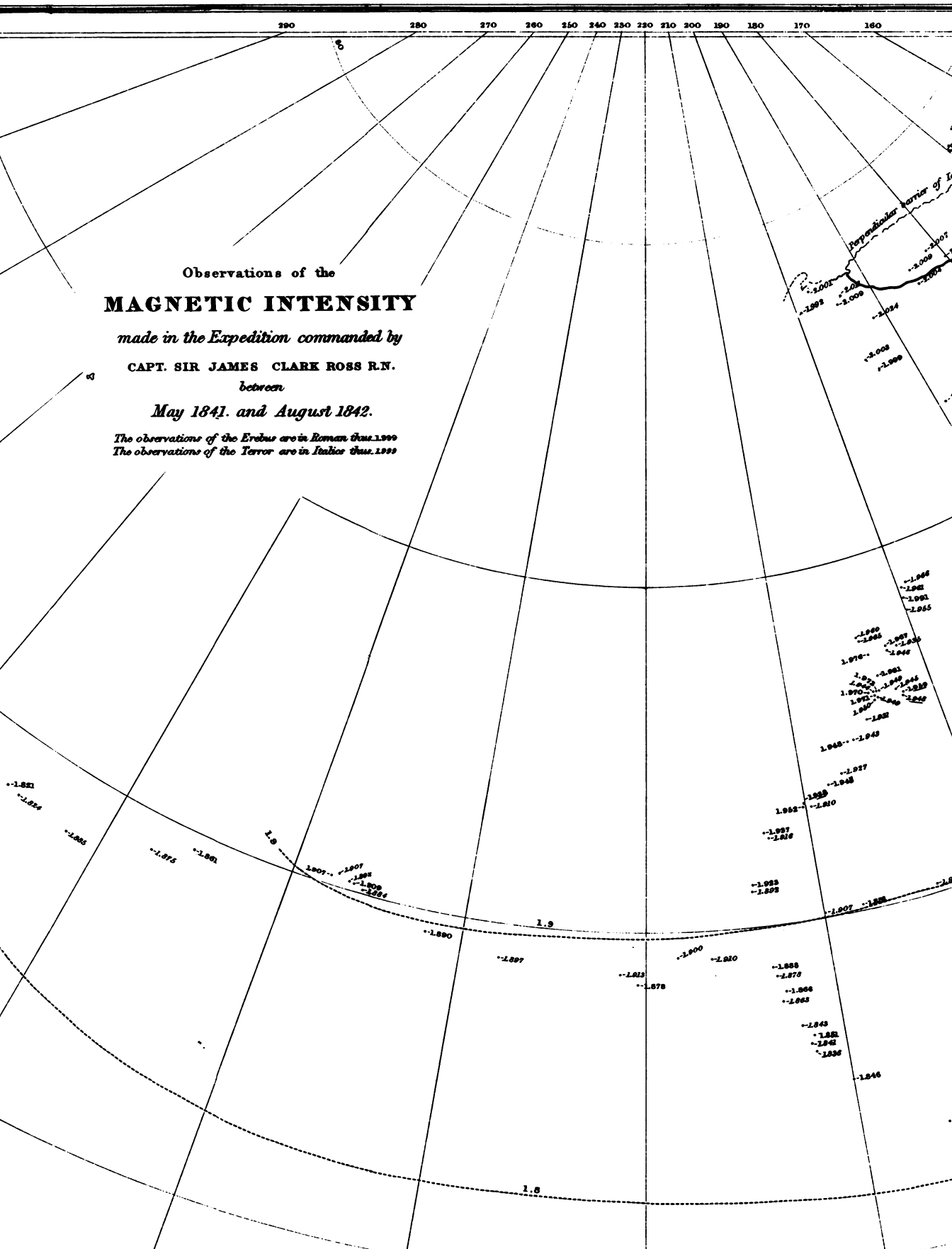
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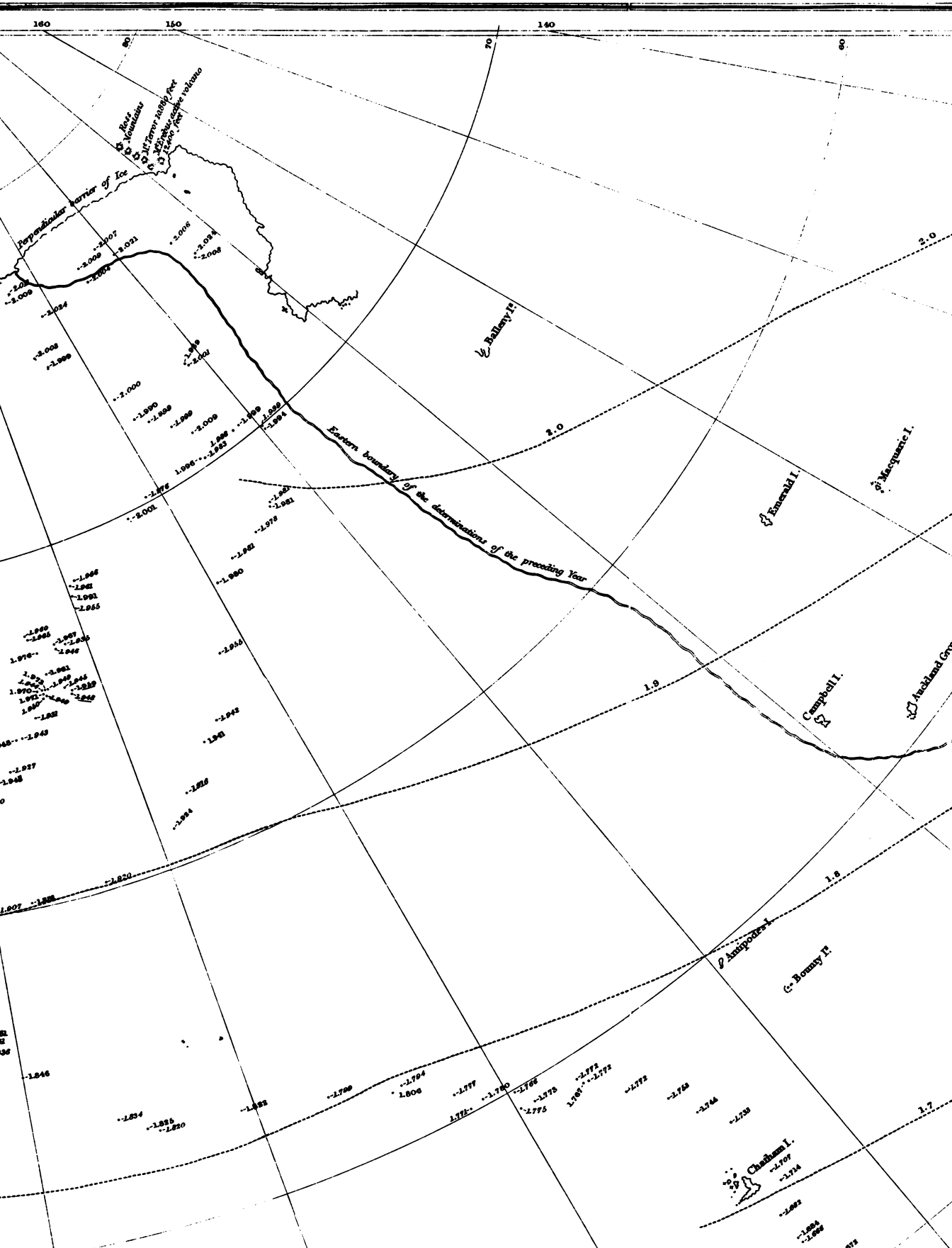
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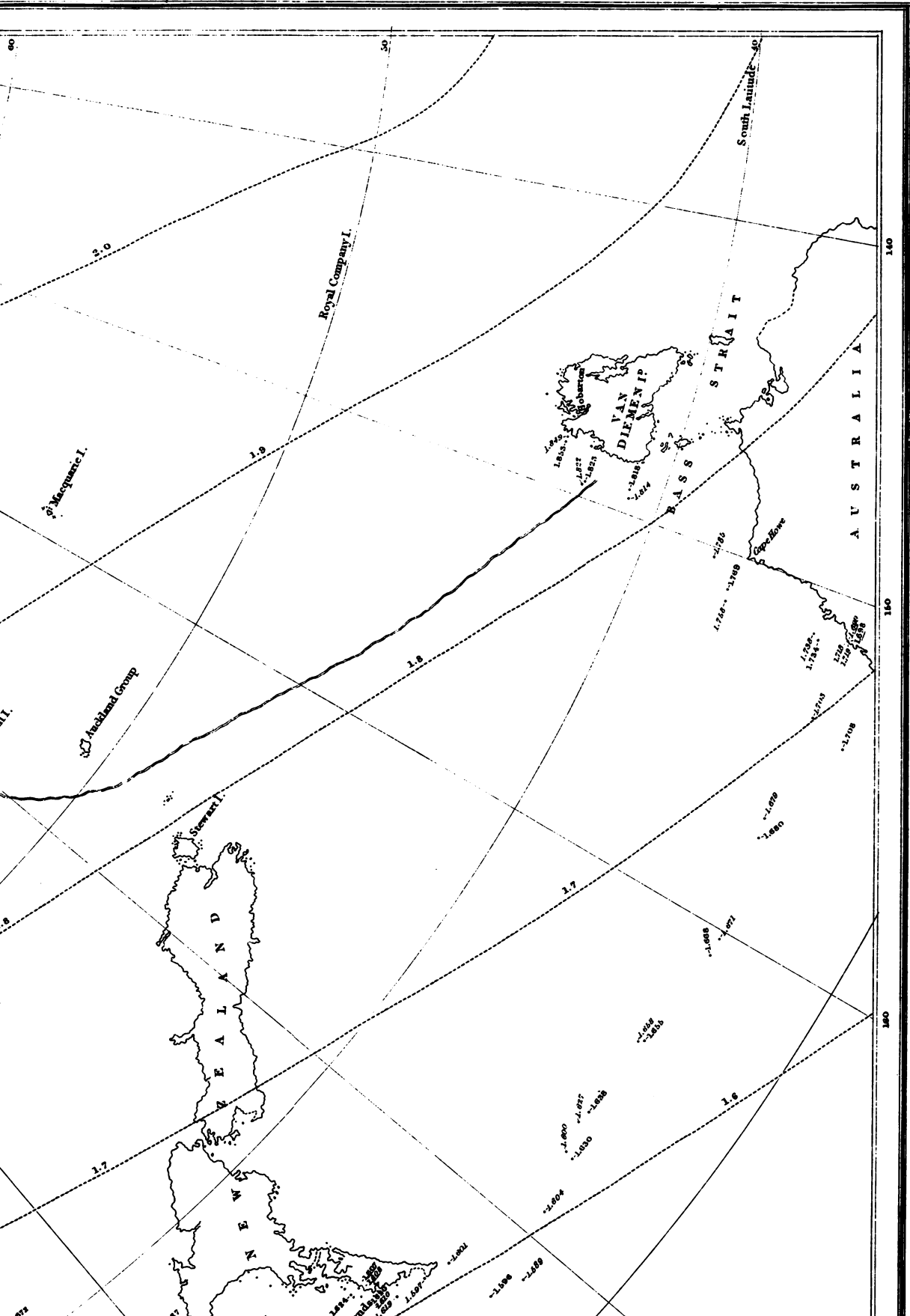
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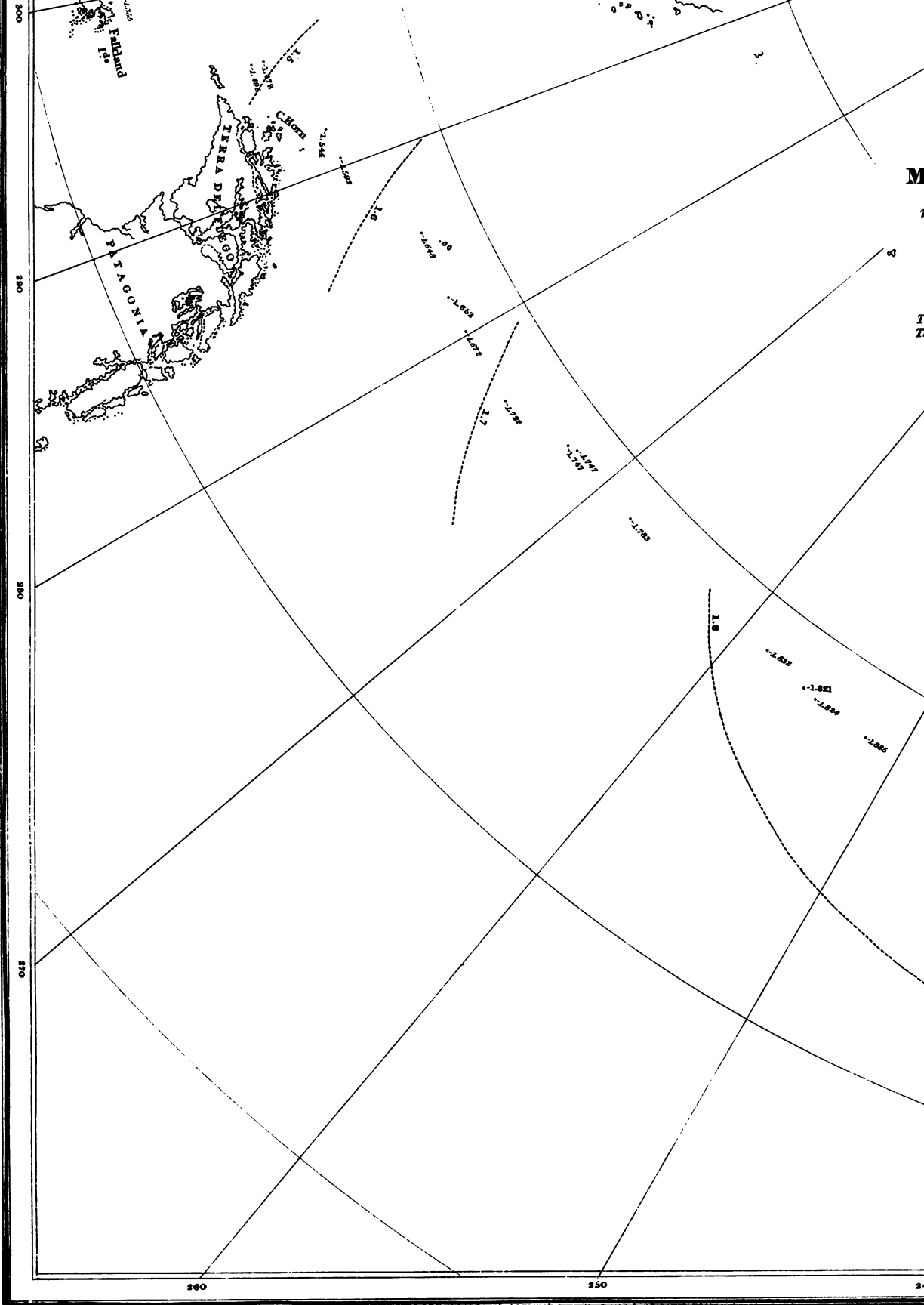
May 1841. and August 1842.

The observations of the Erebus are in Roman thus 1900
The observations of the Terror are in Italic thus 1900









Observations of the
MAGNETIC INTENSITY

made in the Expedition commanded by

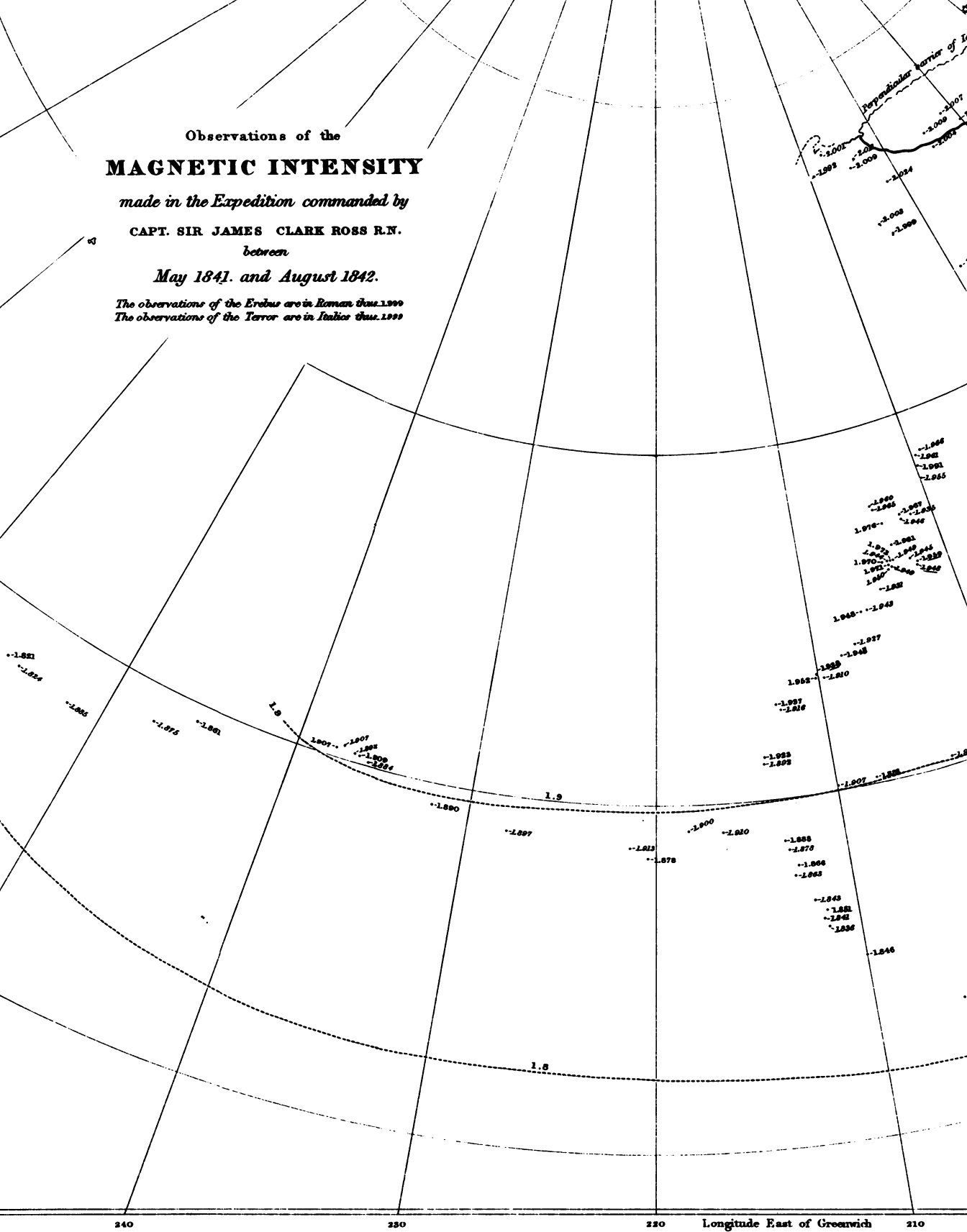
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between

May 1841. and August 1842.

The observations of the Erebus are in Roman thus. 1900

The observations of the Terror are in Italic thus. 1900



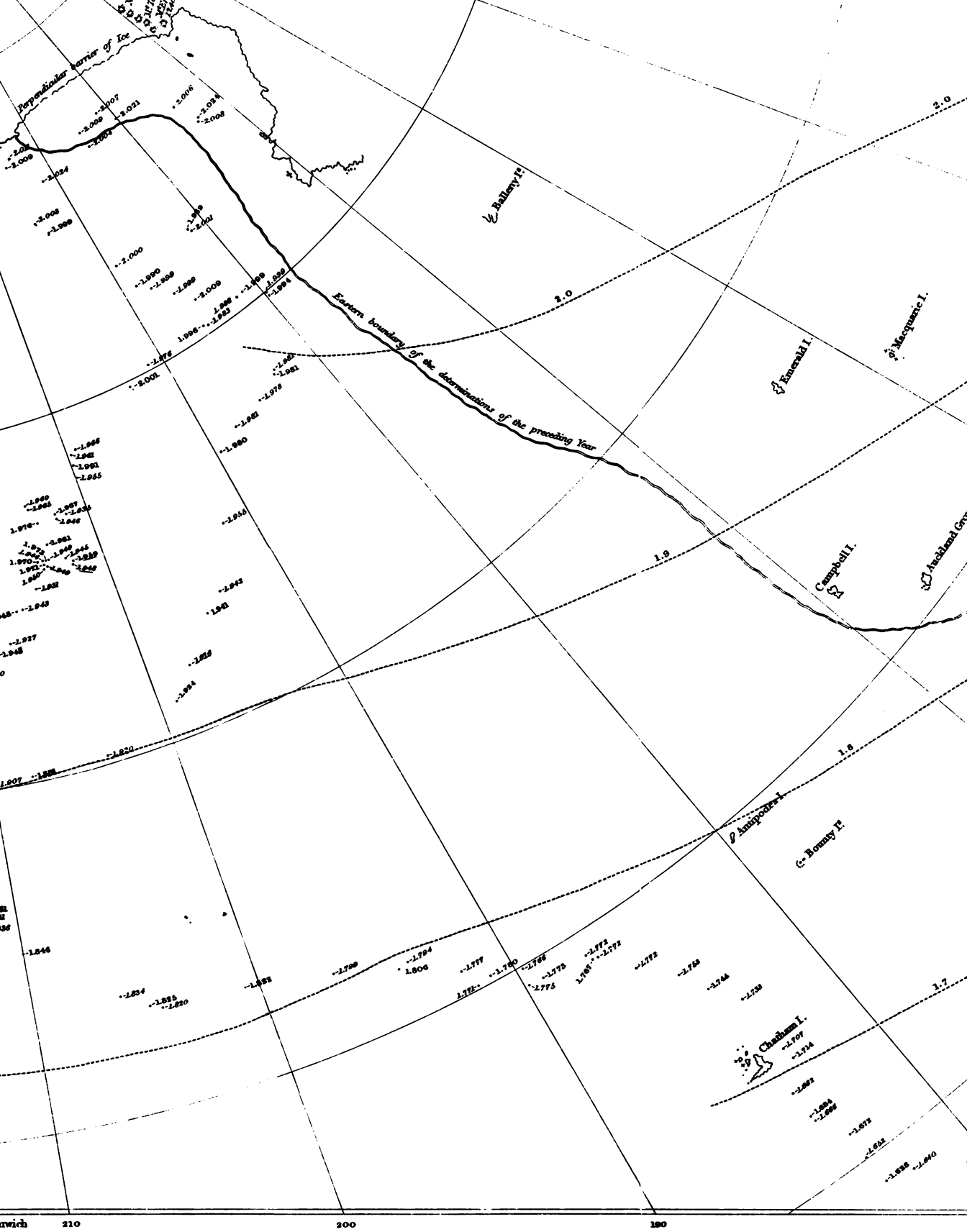
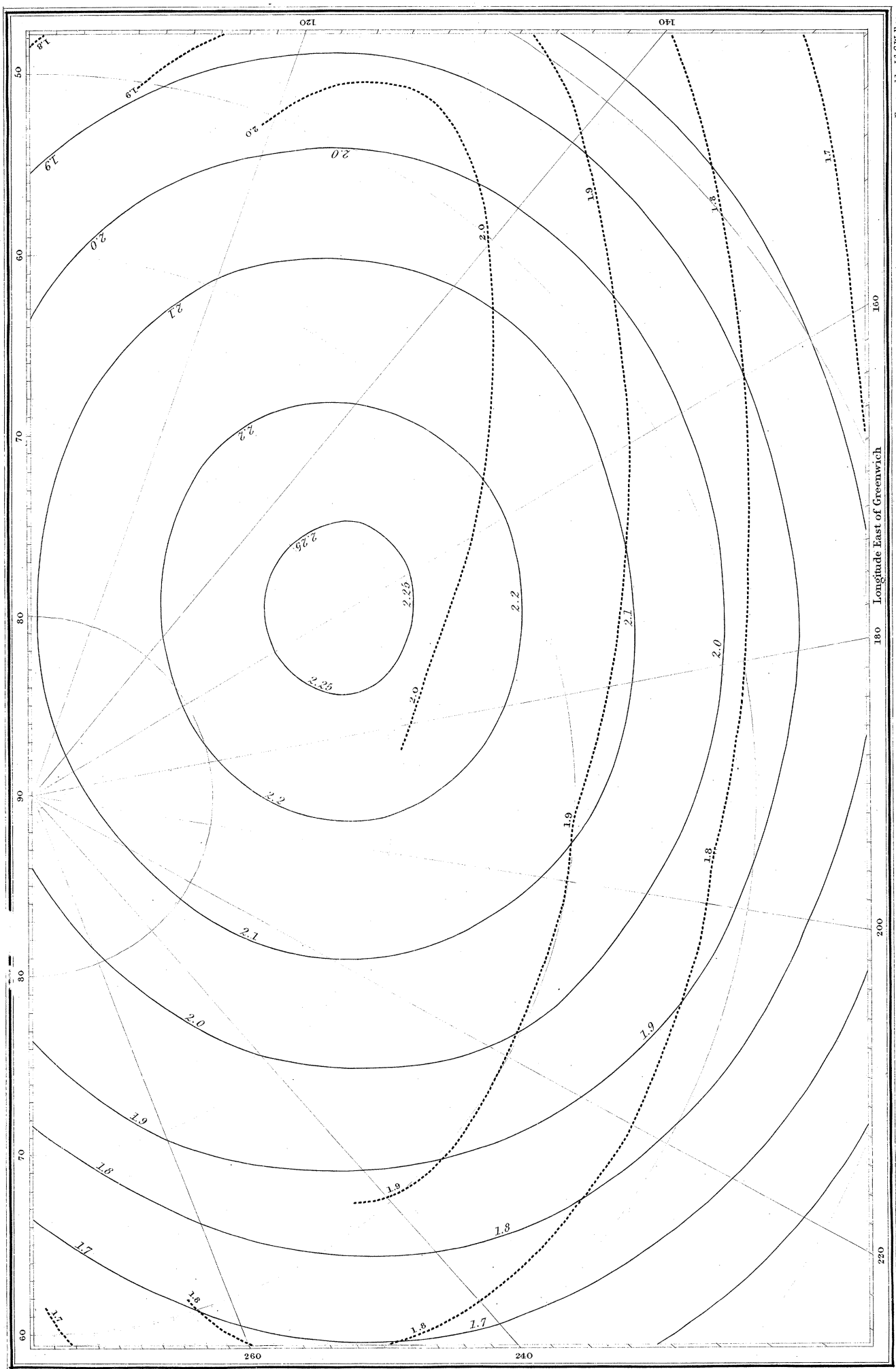


PLATE SHOWING THE LINES OF EQUAL INTENSITY DEDUCED FROM THE OBSERVATIONS OF
THE ANTARCTIC EXPEDITION IN COMPARISON WITH M. GAUSS'S THEORETICAL LINES.

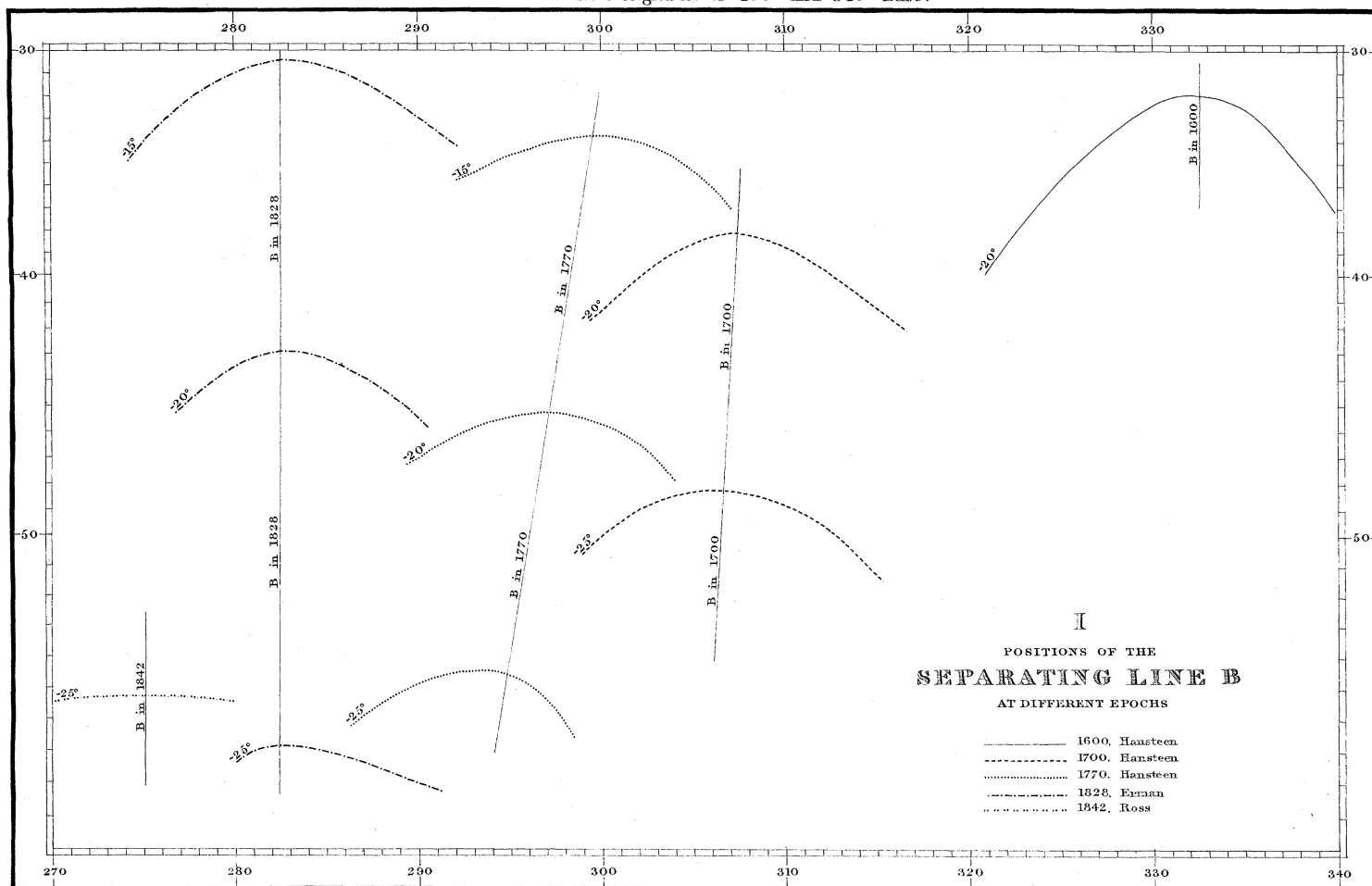
Phil. Trans. MDCCCLIV. Plate XVII.

——— Gauss's theoretical Lines
- - - - - Lines deduced from the Observations of the Antarctic Expedition



Plate, shewing the progressive westerly movement of the Magnetic Phenomena in the Southern Pacific Ocean.

1. Between the Longitudes of 270° and 340° East.



2. Between the Longitudes of 200° and 270° East.

